



Calhoun: The NPS Institutional Archive
DSpace Repository

Theses and Dissertations

1. Thesis and Dissertation Collection, all items

1989-06

The design and implementation of a position measuring system for a remotely controlled video camera

Lloyd, Peter D.

Monterey, California. Naval Postgraduate School

<http://hdl.handle.net/10945/25823>

This publication is a work of the U.S. Government as defined in Title 17, United States Code, Section 101. Copyright protection is not available for this work in the United States.

Downloaded from NPS Archive: Calhoun



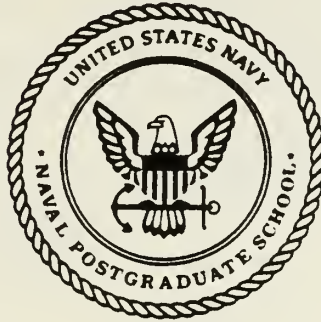
Calhoun is the Naval Postgraduate School's public access digital repository for research materials and institutional publications created by the NPS community. Calhoun is named for Professor of Mathematics Guy K. Calhoun, NPS's first appointed -- and published -- scholarly author.

Dudley Knox Library / Naval Postgraduate School
411 Dyer Road / 1 University Circle
Monterey, California USA 93943

<http://www.nps.edu/library>

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

L767

THE DESIGN AND IMPLEMENTATION
OF A POSITION MEASURING SYSTEM FOR
A REMOTELY CONTROLLED VIDEO CAMERA

by

Peter D. Lloyd

June 1989

Thesis Advisor:

Alfred W. Cooper

Co-Advisor:

Hal A. Titus

Approved for public release; distribution is unlimited

T245986

Unclassified

Security classification of this page

REPORT DOCUMENTATION PAGE

1a Report Security Classification Unclassified			1b Restrictive Markings		
2a Security Classification Authority			3 Distribution Availability of Report Approved for public release; distribution is unlimited.		
2b Declassification Downgrading Schedule					
Performing Organization Report Number(s)			5 Monitoring Organization Report Number(s)		
4a Name of Performing Organization Naval Postgraduate School		6b Office Symbol (if applicable) 62	7a Name of Monitoring Organization Naval Postgraduate School		
4c Address (city, state, and ZIP code) Monterey, CA 93943-5000			7b Address (city, state, and ZIP code) Monterey, CA 93943-5000		
4a Name of Funding Sponsoring Organization		8b Office Symbol (if applicable)	9 Procurement Instrument Identification Number		
4c Address (city, state, and ZIP code)			10 Source of Funding Numbers		
			Program Element No	Project No	Task No
1 Title (include security classification) THE DESIGN AND IMPLEMENTATION OF A POSITION MEASURING SYSTEM FOR A REMOTELY CONTROLLED VIDEO CAMERA					
2 Personal Author(s) Peter D. Lloyd					
3a Type of Report Master's Thesis		13b Time Covered From To		14 Date of Report (year, month, day) June 1989	
				15 Page Count 133	
5 Supplementary Notation The views expressed in this thesis are those of the author and do not reflect the official policy or position of the Department of Defense or the U.S. Government.					
7 Cosati Codes			18 Subject Terms (continue on reverse if necessary and identify by block number)		
Field	Group	Subgroup	Position measurement, microprocessor, MC68705U3, M68705EVM, optical shaft encoder, HEDS-6000,IRSTD.		
9 Abstract (continue on reverse if necessary and identify by block number)					
<p>A position measuring system for a remotely controlled video camera was designed and built. The camera is intended to be used with the modified Advance Development Model of the AN/SAR-8 Infrared Search and Target Designation System (IRSTD) in use at the Naval Postgraduate School. The video data collected by the camera will be correlated with the infrared data from the IRSTD to develop a background data base that will be used in the development of signal processing algorithms.</p> <p>The measurement system uses two Hewlett Packard HEDS-6000 incremental optical encoders, two Motorola MC68705U3 microprocessors and two digital display devices to measure and present the camera's azimuth and elevation angles to an operator at a remote location. The azimuth can be measured over a range of 360° with a resolution of ± 0.0213° and the elevation can be measured over 24° with a resolution of ± 0.138°. The resolution is limited primarily by hysteresis, which is due to the backlash in the gears between the transducers and the axes of interest.</p>					
10 Distribution Availability of Abstract <input checked="" type="checkbox"/> Unclassified unlimited <input type="checkbox"/> same as report <input type="checkbox"/> DTIC users			21 Abstract Security Classification Unclassified		
4a Name of Responsible Individual Alfred W. Cooper			22b Telephone (include Area code) (408) 646-2452		22c Office Symbol 61Cr

FORM 1473,84 MAR

83 APR edition may be used until exhausted
All other editions are obsolete

Security classification of this page

Unclassified

Approved for public release; distribution is unlimited.

The Design and Implementation
of a Position Measuring System
for a Remotely Controlled
Video Camera

by

Peter D. Lloyd
Captain, United States Marine Corps
B.S., United States Naval Academy, 1979

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL
June 1989

ABSTRACT

A position measuring system for a remotely controlled video camera was designed and built. The camera is intended to be used with the modified Advance Development Model of the AN/SAR-8 Infrared Search and Target Designation System (IRSTD) in use at the Naval Postgraduate School. The video data collected by the camera will be correlated with the infrared data from the IRSTD to develop a background data base that will be used in the developement of signal processing algorithms.

The measurement system uses two Hewlett Packard HEDS-6000 incremental optical encoders, two Motorola MC68705U3 microprocessors and two digital display devices to measure and present the camera's azimuth and elevation angles to an operator at a remote location. The azimuth can be measured over a range of 360° with a resolution of $\pm 0.0213^\circ$ and the elevation can be measured over 24° with a resolution of $\pm 0.138^\circ$. The resolution is limited primarily by hysteresis, which is due to the backlash in the gears between the transducers and the axes of interest.

17238
2 767
C. 1

THESIS DISCLAIMER

The reader is cautioned that computer programs developed in this research may not have been exercised for all cases of interest. While every effort has been made, within the time available, to ensure that the programs are free of computational and logic errors, they cannot be considered validated. Any application of these programs without additional verification is at the risk of the user.

TABLE OF CONTENTS

I. INTRODUCTION	1
A. BACKGROUND	1
B. DESIGN SPECIFICATIONS	2
II. DESIGN STRATEGY	4
A. GENERAL	4
B. TRANSDUCERS	7
1. General	7
2. Transducer technologies	8
a. Reluctive Displacement Transducers	8
b. Capacitive Displacement Transducers	9
c. Potentiometric Displacement Transducers	11
d. Encoders	15
C. MOUNTING THE TRANSDUCER	17
D. SELECTING AN OPTICAL SHAFT ENCODER	19
E. THE DISPLAY	22
F. THE SIGNAL CONDITIONER	22
1. Up/down (U/D) counter with table look-up	23
2. Up/down counter and multiplication	24
3. Add,subtract	24
4. Microcomputer	25
5. Microprocessor	25
III. DESIGN	28
A. GENERAL	28
B. SHAFT ENCODER AND LINE DRIVER	28
C. ENCODER-MICROPROCESSOR INTERFACE	30
D. SWITCHES	31
E. MC68705U3	34
1. General	34
2. Memory Map	35

a. Input Output (I/O)	35
b. Timer	37
3. RAM	42
4. ROM	42
5. Central Processing Unit (CPU)	43
6. Input	44
7. Output	44
F. DISPLAY	46
G. POWER SUPPLIES	46
 IV. CALIBRATION , TESTING AND IMPLEMENTATION	48
A. GENERAL	48
B. CALIBRATION	48
1. Scale Factor	53
2. Hysteresis	56
C. IMPLEMENTATION OF THE CALIBRATION DATA	60
1. Background	60
2. Implementing the Hysteresis Buffer	62
3. Implementing the Scale Factor	63
D. FINAL TESTING	65
1. General	65
2. Pan Axis	66
a. Hysteresis	66
b. Scale Factor	67
c. Combined Error	68
3. Tilt Axis	68
a. Hysteresis	68
b. Scale Factor	68
c. Combined Error	69
E. FINAL IMPLEMENTATION	70
 V. CONCLUSIONS AND RECOMMENDATIONS	71
A. SYSTEM PERFORMANCE	71
B. RECOMMENDATIONS FOR FURTHER WORK	71

APPENDIX A. SCHEMATIC DIAGRAMS	72
APPENDIX B. PRINTED CIRCUIT BOARD PLANS	80
APPENDIX C. MICROPROCESSOR PROGRAMS	87
A. GENERAL	87
B. PAN	88
C. TILT	105
LIST OF REFERENCES	120
INITIAL DISTRIBUTION LIST	122

LIST OF TABLES

Table	1. ANGULAR DISPLACEMENT TRANSDUCERS	18
Table	2. SIGNAL PROCESSOR AND DISPLAY SWITCHES	36
Table	3. MPU CONNECTIONS	39
Table	4. MPU CONNECTIONS (CONT'D.)	40
Table	5. COUNT ROUTINE LOGIC	62

LIST OF FIGURES

Figure 1.	Basic Electronic Position Measuring System	5
Figure 2.	Camera Position Measuring System	6
Figure 3.	RVDT Schematic	9
Figure 4.	RVDT Output Characteristics	10
Figure 5.	Capacitive Displacement Transducer	10
Figure 6.	Geometry of an Angular Potentiometric Transducer	12
Figure 7.	Multiturn Potentiometer	13
Figure 8.	Potentiometric Transducer	14
Figure 9.	Absolute Photoelectric Angular Encoder	16
Figure 10.	Camera Servo	20
Figure 11.	HEDS-6000 Series Encoder Kit	29
Figure 12.	Modified Camera Servo	30
Figure 13.	Encoder Connector Specifications	31
Figure 14.	Encoder-Microprocessor Connector Specifications	32
Figure 15.	Interrupt Interface	33
Figure 16.	Control Panel	34
Figure 17.	Debouncing circuit	35
Figure 18.	MC68705U3 Pin assignments	37
Figure 19.	MC68705U3 Memory Configuration	38
Figure 20.	MC68705U3 Timer Functional Block Diagram.	41
Figure 21.	Reverse Over-voltage Protection Circuit	47
Figure 22.	Prototype/Development Model	49
Figure 23.	Host Computer - Evaluation Module Connections	50
Figure 24.	Monitor - Evaluation Module Connections	51
Figure 25.	Evaluation Module - Signal Processor Connections	52
Figure 26.	Geometry Used to Determine the Scale Factor	54
Figure 27.	Alternate Geometry Used to Determine the Scale Factor	55
Figure 28.	Typical Hysteresis Curve	57
Figure 29.	Operation of the Hysteresis Buffer	58
Figure 30.	Hysteresis Curve	59
Figure 31.	Program Flow Diagram	61

ACKNOWLEDGEMENTS

This thesis is prepared in conjunction with research sponsored in part by the Naval Sea Systems Command, PMS-421, and by the Naval Postgraduate School.

I would like to take a moment to thank the following people who have offered so much and so generously as I have undertaken this project:

My parents who have always helped me through the hard times.

Professor A. W. Cooper for his confidence and insight.

Professor Hal Titus for his constant encouragement, guidance and tremendous sense of humor which made even the difficult times enjoyable.

John Glenn, Jerry Lentz and Eric Moore for their continued technical assistance.

ET2 Akerson for his dedicated work in designing and building the printed circuit boards.

George Jaksha for his expert advice and work in modifying the camera servo mechanism.

I offer my sincere thanks to my fellow officers and students, especially my good friends Capt Steve Spehn and CPT Ken Cockerham for their friendship and thoughtful suggestions.

Finally, I offer my thanks and love to my dear wife, Ellen, who has given so very much in the past two years.

I. INTRODUCTION

A. BACKGROUND

The old saying that "every solution breeds new problems", while somewhat pessimistic, quite often rings true in today's increasingly technical world. One such example is the use of infrared (IR) sensors for the detection, tracking and/or identification of targets in a combat environment. IR sensors are ideally suited for use on today's battlefield. They are passive, i.e., they do not need to emit energy in order to detect the presence of potential targets. This allows them to operate during times of emission control when many other target detection systems are useless. They have the ability to "see through" many forms of camouflage and concealment, dust, clouds, smoke, etc., that might otherwise afford an enemy target a safe haven. Additionally, because almost everything on today's battlefield generates some degree of infrared energy, IR sensors can be used to locate and identify a wide variety of targets.

The extent to which a particular IR sensor is useful depends primarily on its ability to detect and identify targets reliably and accurately. Detection of the target is primarily a function of the IR sensor's sensitivity. The classification of a received IR signal as a potential target or as background noise, while still dependant on the sensitivity of the sensors, is primarily a function of the quality of the signal processing algorithms being used to process the received signals. In addition to being reliable these algorithms must be able to process the received signals in "real time" if the system is to be an effective weapons system.

Creation of a background data base that can be used to test some of these algorithms has been one of the tasks being performed by the Naval Academic Center for Infrared Technology (NACIT) located at the Naval Postgraduate School (NPS). The Advanced Development Model (ADM) of the AN/SAR-8 was sent to the NACIT in January of 1984 from the Naval Surface Weapons Center (NSWC) at Dahlgren, Virginia. The ADM was modified, calibrated and placed in service at NPS in December, 1987. The modified version of the ADM, the Infrared Search and Target Designation (IRSTD) System, is currently operational at NPS. [Ref. 1: pp. 8-12]

One way to enhance the usefulness of the IR data being collected at NPS would be to collect video data concurrently with the IR data. A video image of a portion of the horizon would permit visual identification of IR sources in that region. This additional

tional information could be an aid in the development of the signal processing algorithms for the IRSTD. Accordingly, a decision to proceed with video data collection was made by NACIT, and a camera system was purchased. Components of the system include;

- RCA (TC1005/01), Closed circuit video camera.
- PELCO (AI700), Automatic iris servo.
- PELCO (F1.5X), 1.5 times range extender.
- PELCO (MLZ6DT), Desk top lens remote control module.
- PELCO (PT1250DC), Heavy duty Pan/Tilt servo.
- PELCO (MPTV1510DT), Pan/Tilt remote control unit.
- Panasonic (WV-5410), Video Monitor.

In Ref. 1 Ayers describes the IRSTD's detectors:

The IR detectors consist of two vertical arrays of sensing elements in the focal plane of the Schmidt telescope. The telescope is rotated so as to sweep the image across the detector arrays. Each array incorporates a column of 90 indium antimonide photovoltaic linear detector elements. These two arrays are independent of each other and are covered by filters which pass selected wavebands of IR radiation in the 3 to 5 micrometer range. Each element has the angular dimensions of $2 \times .3$ milliradians with the larger being its height. Designated as the lead and the lag, these two arrays are separated by about one-half degree in azimuth. [Ref. 1: p. 17]

Thus, as the IRSTD scans the horizon the resulting IR image has a resolution of approximately 10^{-4} radians (0.00573°) in the horizontal plane and 0.23° in the vertical plane. The video system's smaller field of view can be remotely controlled using the control units listed above. Thus, for the video data to be of any use in the development of the signal processing algorithms, the camera's orientation must first be known, and, in order to determine the pixel-to-pixel correlation between the IR image and the video image, the position of the video camera needs to be known with the same kind of accuracy as the IR image. The design and implementation of a position measuring system for this remotely controlled video camera is the subject of this thesis.

B. DESIGN SPECIFICATIONS

The design specifications for this problem were relatively straight forward. The position measuring system needed to meet the following criteria.

- The system should be able to measure the elevation angle (tilt), above and below the horizontal reference plane of the camera over a range of $\pm 12^\circ$.
- The measured elevation angle should be accurate to within $\pm 0.23^\circ$.

- The system should be able to measure the bearing (pan), left or right of some arbitrary reference, of the camera over a range of 360° .
- The measured bearing should be accurate to within $\pm 10^{-4}$ radians.
- The output should be displayed in a convenient form. The display should be collocated with the camera servo remote controls, an indoor site approximately 200 meters away from the camera.
- Portions of the measuring system required to be collocated with the camera should be weatherproofed.
- The system must be reliable and should be simple to operate.

II. DESIGN STRATEGY

A. GENERAL

A position measuring system, like any system, is a combination of devices interconnected to perform a certain function. The most basic position measuring system (see Figure 1) consists of only four such devices: a transducer, a signal conditioner, a display device and a power supply. More complicated position measuring systems include those designed to take a number of different measurements either simultaneously or consecutively. Still more complex systems multiplex these various measurements over a single channel to some distant location where they can be processed and displayed. [Ref. 2: pp. 2-14]

The design specifications for the camera position measurement system (subsequently referred to as the "measurement system") required that two measurements, pan and tilt, be taken simultaneously and transmitted some distance to a remote display. Two separate transducers, capable of independent operation, were therefore required. In order for both the azimuth and the elevation to be displayed simultaneously two display devices were also required.

Several pairs of RG-178 coaxial cable were available to transmit signals between the camera servo and the remote control site. Since the cable was available and it was desirable to reduce the system complexity, a decision was made not to multiplex the data over a single channel. Instead, each measurand would have a separate transducer, a dedicated signal processor and a unique display device. Position information for each axis would be transmitted over a dedicated channel.

The physical locations of the transducers and the display devices were dictated by the design specifications; however, there was some flexibility in deciding where to locate the signal conditioner. Site selection was based on an attempt to maximize total system performance and simplicity while ensuring the maintainability and environmental integrity of the signal conditioner. The only advantage to locating the signal conditioner with the camera servo and the transducer would have been to limit the distance that the transducer's output signal would have to be transmitted to the processor. On the other hand, separating the signal conditioner and the transducers would limit the distance over which the conditioned signal would have to be transmitted to the display device. The trade-off here was not clear cut and would probably depend on the specific hardware

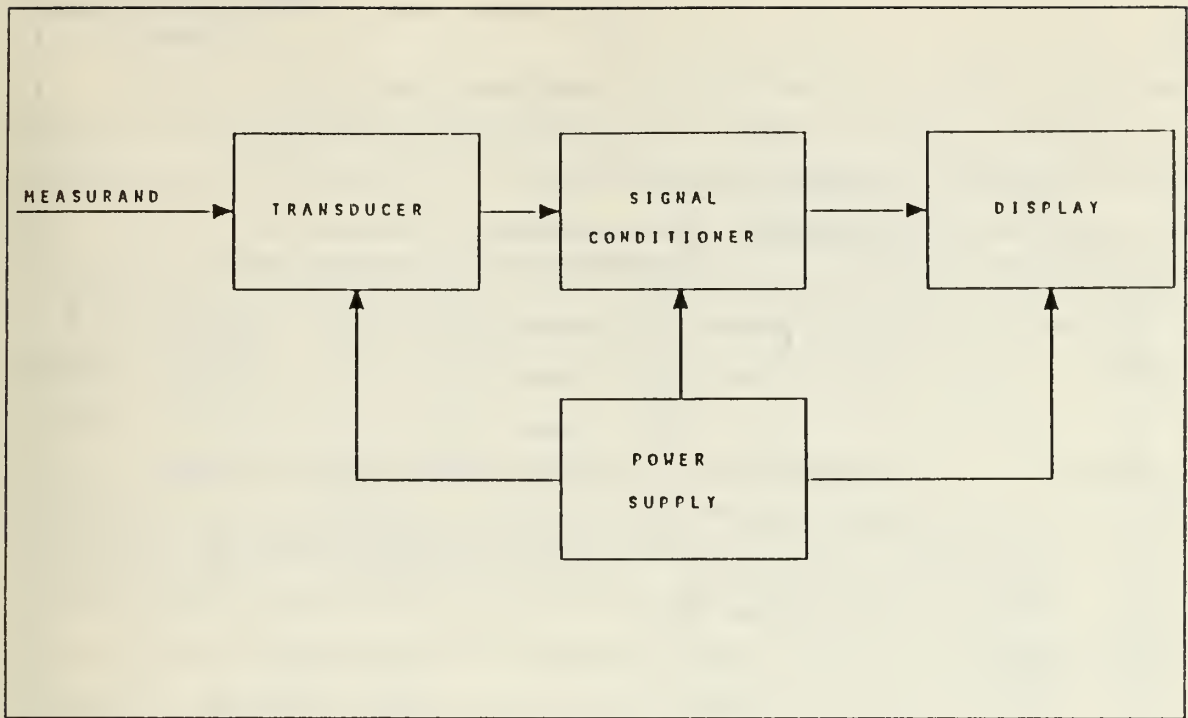


Figure 1. Basic Electronic Position Measuring System: From Ref. 2: p. 2

used and the speed of rotation of the camera servo. There was one significant advantage, however, to collocating the display and the signal processor; since they would both be indoors, the need for weatherproofing the signal processor would be eliminated.

Power was available at both ends of the system, there was therefore no requirement to have a common power supply for the entire system. One supply could be used to provide power to the two transducers, collocated with the camera servo, and a second supply could power the signal conditioner and the displays.

A block diagram of the prototype measurement system is shown interconnected with the camera positioning system in Figure 2. Once this basic system layout had been determined, proper selection of the actual hardware was necessary. The design criteria were the primary consideration in the initial stages of the hardware selection. Final selection of the specific components, however, involved balancing additional factors, such as availability and cost against the system requirements.

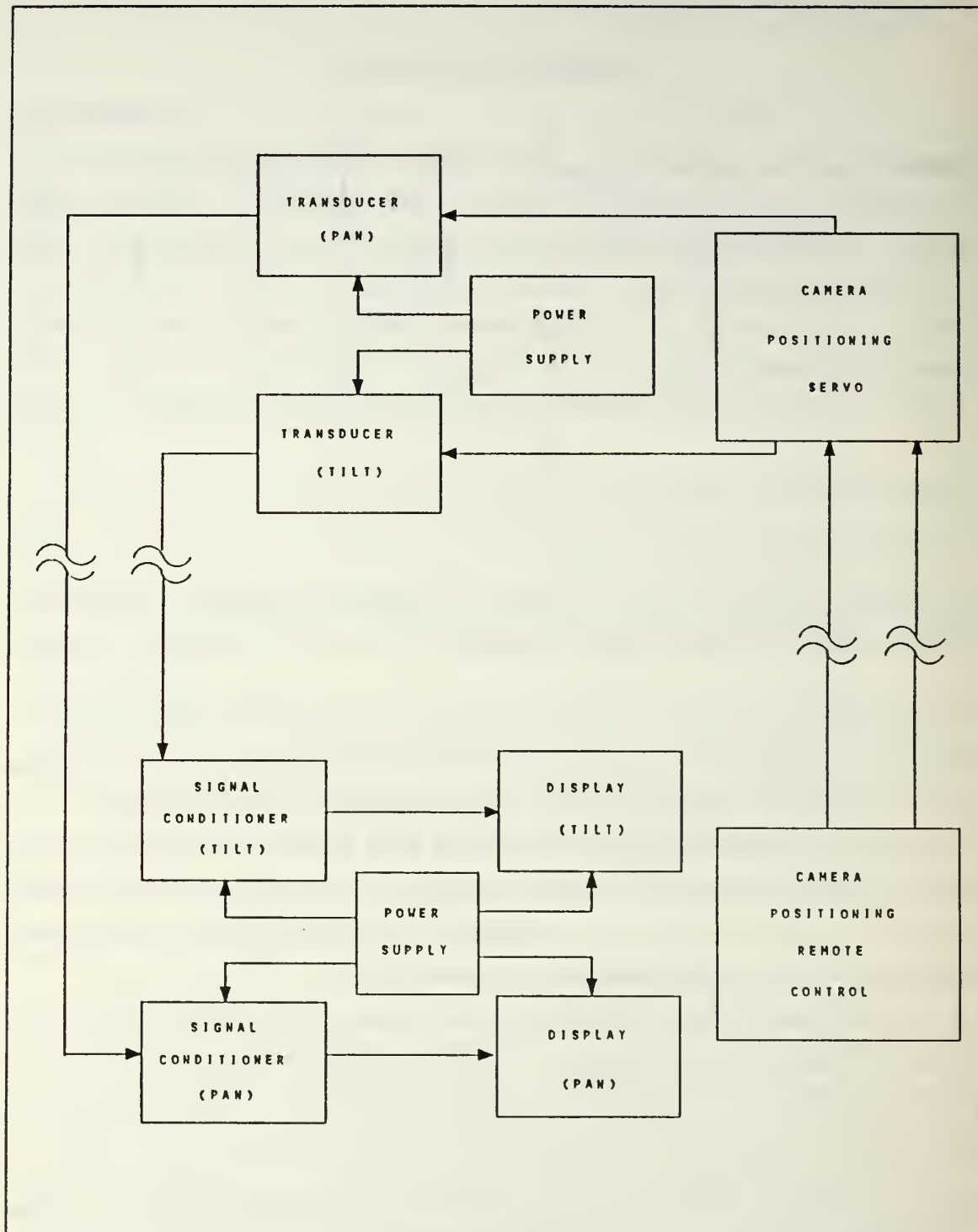


Figure 2. Camera Position Measuring System

B. TRANSDUCERS

1. General

Since in practice most measurement systems do not have the ability to respond directly to the measurand, transducers are used to convert one physical quantity (e.g., angular position) into another, more usable quantity or signal (e.g., an electrical signal) [Ref. 3: p. 1-4]. The transducer is therefore a vital part of any measurement system, and although none of the components of this system could have been chosen independently of the other elements, proper transducer selection appeared to be the key to meeting the design specifications. Thus, selection of a transducer was the next step in the design process.

Using the selection guidelines given by Norton on pages 51-53 of Ref. 2 and the design criteria stated previously, several observations and decisions were made which significantly reduced the number of transducers considered feasible for use in the measurement system. The fact that the servo was capable of rotating the camera left or right, and up or down suggested that the transducer should be capable of detecting both increasing and decreasing angles on both axes. Additionally, since the servo was anticipated to rotate the camera through one 360° arc in the horizontal plane, the transducer used to measure this angle (subsequently referred to as the "pan transducer") needed to have a comparable range capability. The range requirement for the "tilt transducer" (used to measure the elevation angle) was much less restrictive. These factors, angular bidirectional capability and full scale range, eliminated a great number of transducers from the list of candidates.

The list was further narrowed by the accuracy requirements previously specified. Again the accuracy in the horizontal plane placed a much more severe limitation on the selection of a transducer than the accuracy requirements for the vertical plane. The following paragraphs in this section outline the logic used in the selection of the transducers. The factors considered in the selection process included the following;

- The accuracy requirements given in the specifications.
- The ease with which a specific transducer could be installed on the servo.
- The ability to weatherproof the servo and the transducer once the transducer was installed.
- The rotation speed of the camera about the servo axes.
- The extent to which a particular transducer/mounting configuration would modify the measurand.
- Cost effectiveness.

- Availability.
- Signal conditioning requirements.
- The extent to which the selection of a particular transducer would simplify or complicate the modification or expansion of the measurement system.

2. Transducer technologies

Displacement transducer technologies fall into three very broad categories depending on whether they are capable of measuring linear or angular displacement, or both. Some technologies could be eliminated immediately since they were clearly not suited for measuring angular position. Strain gauge displacement transducers, inductive displacement transducers and vibrating-wire displacement transducers are examples of such devices. The following paragraphs briefly describe the different transducer technologies which were investigated. Table 1 on page 18 summarizes the salient points of the discussion. [Ref. 2: pp. 90-117].

a. *Reluctive Displacement Transducers*

The rotary variable differential transformer (RVDT), which operates by detecting a change in the reluctance between coils, offers excellent resolution, dynamic characteristics, linearity and life expectancy [Ref.3: p. (2-14)]. Figure 3 shows a schematic diagram and a simplified cross-section of an RVDT. The ferromagnetic, cardioid-shaped core is attached to a shaft as shown. As the shaft rotates, the inductive coupling between the primary and each of the secondary coils changes. When the cam is symmetric with respect to the two secondary coils, their output voltages are equal but opposite in phase which results in a differential output voltage of zero. As the shaft rotates away from this "null" the differential output voltage varies as shown in Figure 4. The linear region of the curve is limited to the angles between $\pm 40^\circ$ of the reference. Thus, the RVDT could not be used on the Pan axis. It was however, initially considered as a candidate for the Tilt transducer. [Refs. 2: pp. 93-99, 3: pp. (9-10)-(9-13) and 4: p. 19]

Another type of reductive displacement transducer is manufactured by Farrand Controls. Their INDUCTOSYN rotary position transducers have accuracies to ± 1.5 arc sec ($\approx (4 \times 10^{-4})^\circ$). Unfortunately, these devices are 11.89 inches in diameter, and mounting them on the camera servo would have been extremely difficult, if not impossible. [Refs. 2: pp. 89-111, 5]

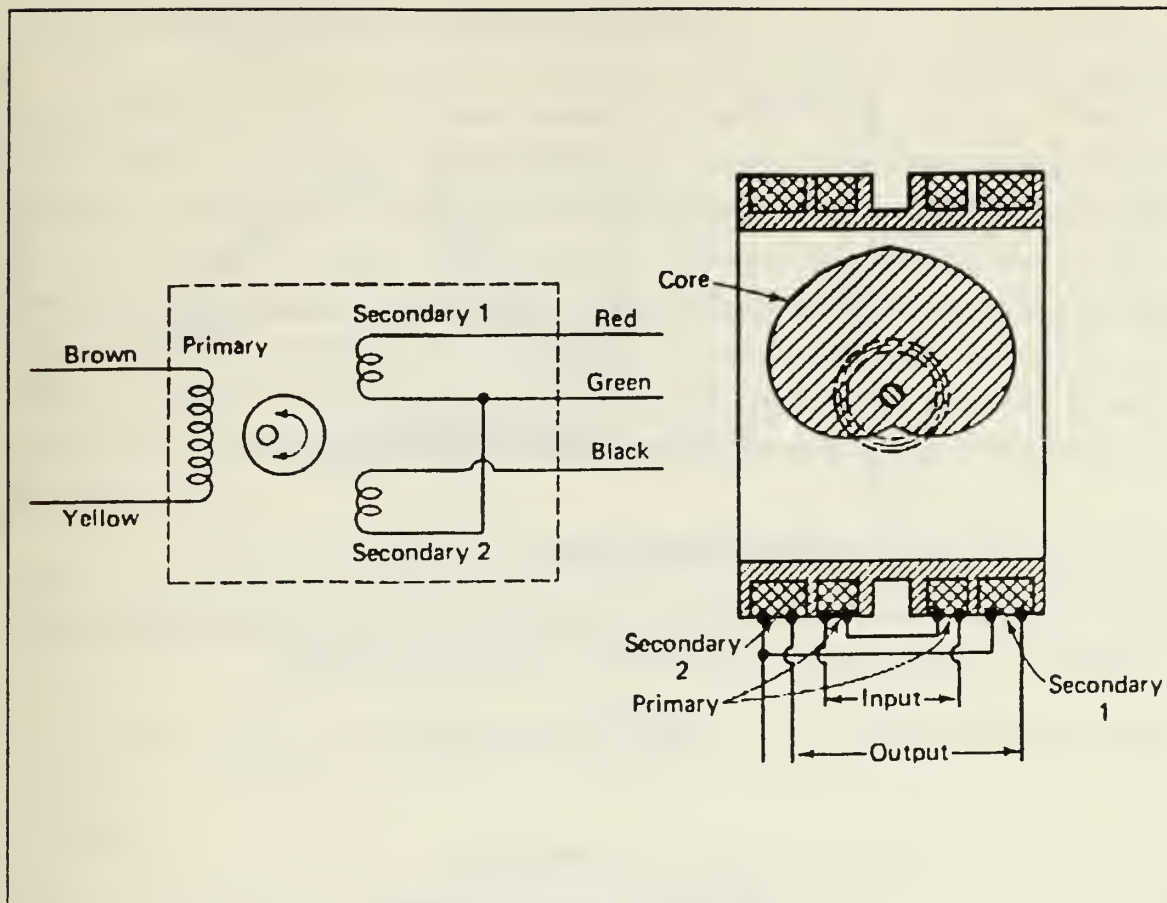


Figure 3. RVDT Schematic: From Ref. 2: p. 98.

b. Capacitive Displacement Transducers

Angular displacement can also be measured by coupling the rotating component to the shaft of a variable capacitor in the manner shown in Figure 5. Lenk describes the operation of the capacitive displacement transducer quite succinctly.

The capacitor ... consists of a metal plate that moves between two fixed metal plates as a shaft is rotated. The three plates, and the air between them, form a capacitor with a capacitance that varies in proportion to the degree to which the plates are meshed. When the plates are completely meshed, the capacitance is at its maximum. When the plates are completely unmeshed, the capacitance is at minimum. [Ref. 4: p. 18]

Capacitive displacement transducers offer many of the advantages of reluctance displacement transducers. They have an effective range of about 300° which, while better than the RVDT's range, is still not adequate for the pan axis [Ref. 4: p. 18]. Additionally they are more sensitive to changes in the ambient temperature. Since the

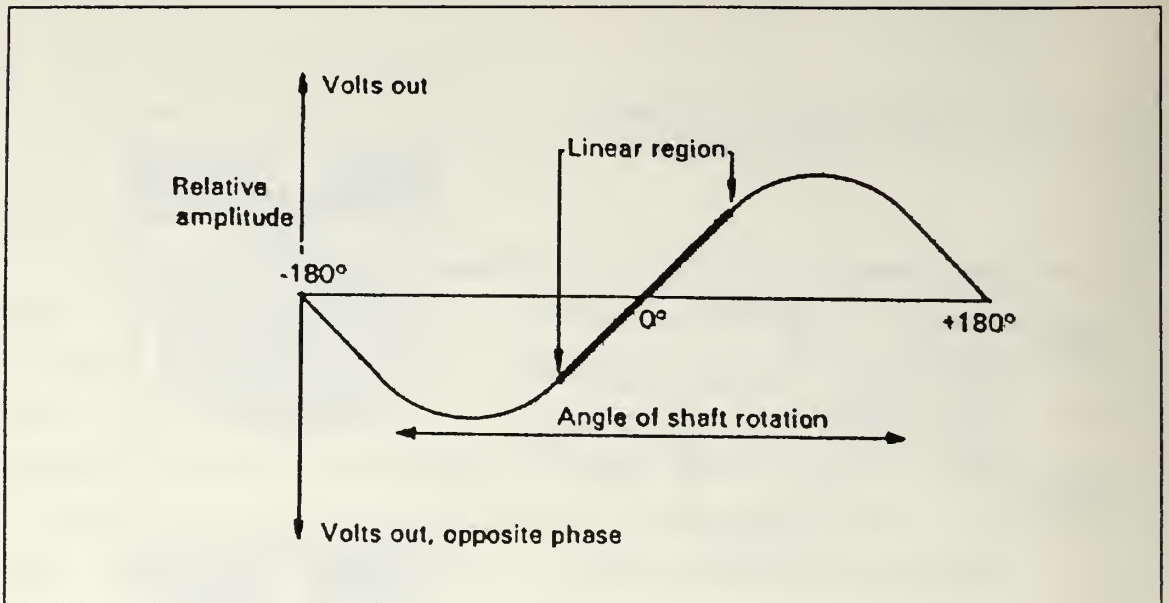


Figure 4. RVDT Output Characteristics: From Ref. 2: p. 95.

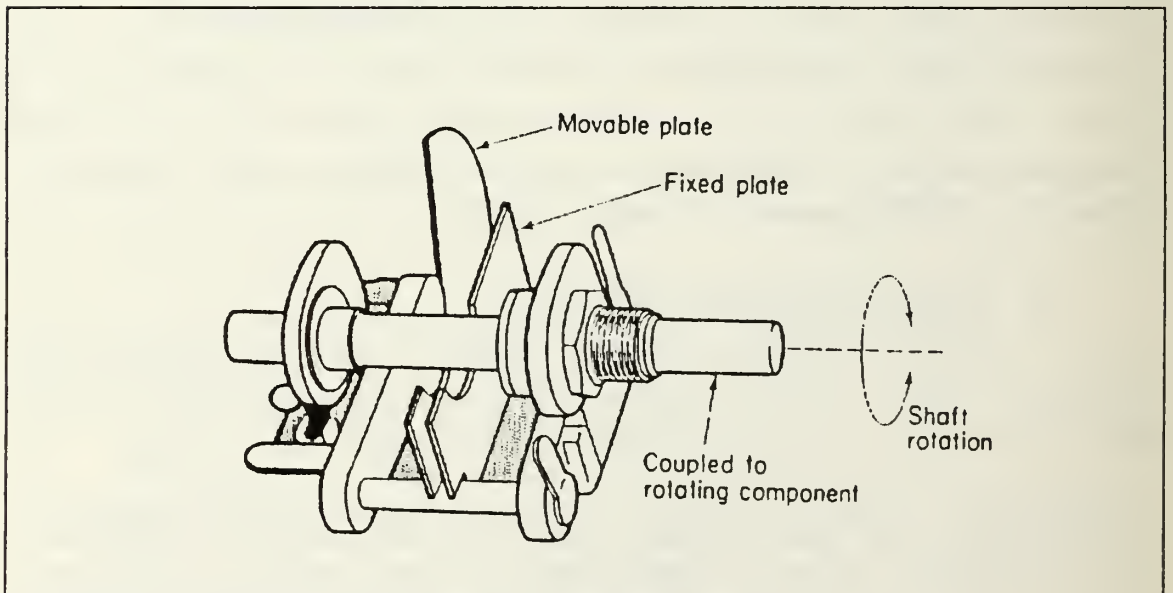


Figure 5. Capacitive Displacement Transducer: Ref. 4: p. 18.

measurement system was being designed to be used outdoors, the use of a capacitive displacement transducer would have required the addition of a temperature compensator in the design. While possible, this would have increased the system complexity considerably. [Ref. 2: pp. 90-91]

c. *Potentiometric Displacement Transducers*

Another very common and relatively simple family of transducers operate by measuring the change in resistance caused by a change in the measurand. There are a wide variety of such devices available. The basic form of potentiometric angular displacement transducers uses a resistance element, formed into an arc, and a movable electrical contact that rotates about the axis of interest. By measuring the change in resistance that results from a change in position, one is able to determine the angular displacement. The resistive element is typically a wirewound element, the resolution of which is determined by the number of turns per unit length of the resistance element. The angular resolution can be increased by increasing the turn density (wires/degree) of the potentiometer.

The practical limit for wire spacing on wirewound elements according to Ref. 6 is between 500 and 1000 turns per inch. From Figure 6 one can see that this limits the angular resolution for a single-turn device to

$$\Delta\theta(\text{rad}) \simeq \tan\left(\frac{\Delta x(\text{in})}{R(\text{in})}\right) \quad (1)$$

Therefore,

$$\Delta\theta(\text{rad}) \simeq \frac{2\Delta x}{D} = \frac{0.002(\text{in})}{D(\text{in})} \quad (2)$$

To achieve the 10^{-4} rad resolution, specified for the Pan axis, with a single turn potentiometer would therefore require a 20 in diameter potentiometer. Mounting a device this large on the camera servo was simply not feasible. Potentiometers are, however, available with multiple turns. Shaped in a helix fashion similar to that shown in Figure 7, the total length of the potentiometer can be increased, which in turn increases its resolution, without increasing the diameter of the device.

Increasing the resolution of the potentiometer by increasing the turn density in any of the manners described above, however, increases the output impedance of the device, which leads to increasing nonlinearity between the measurand and the transducer

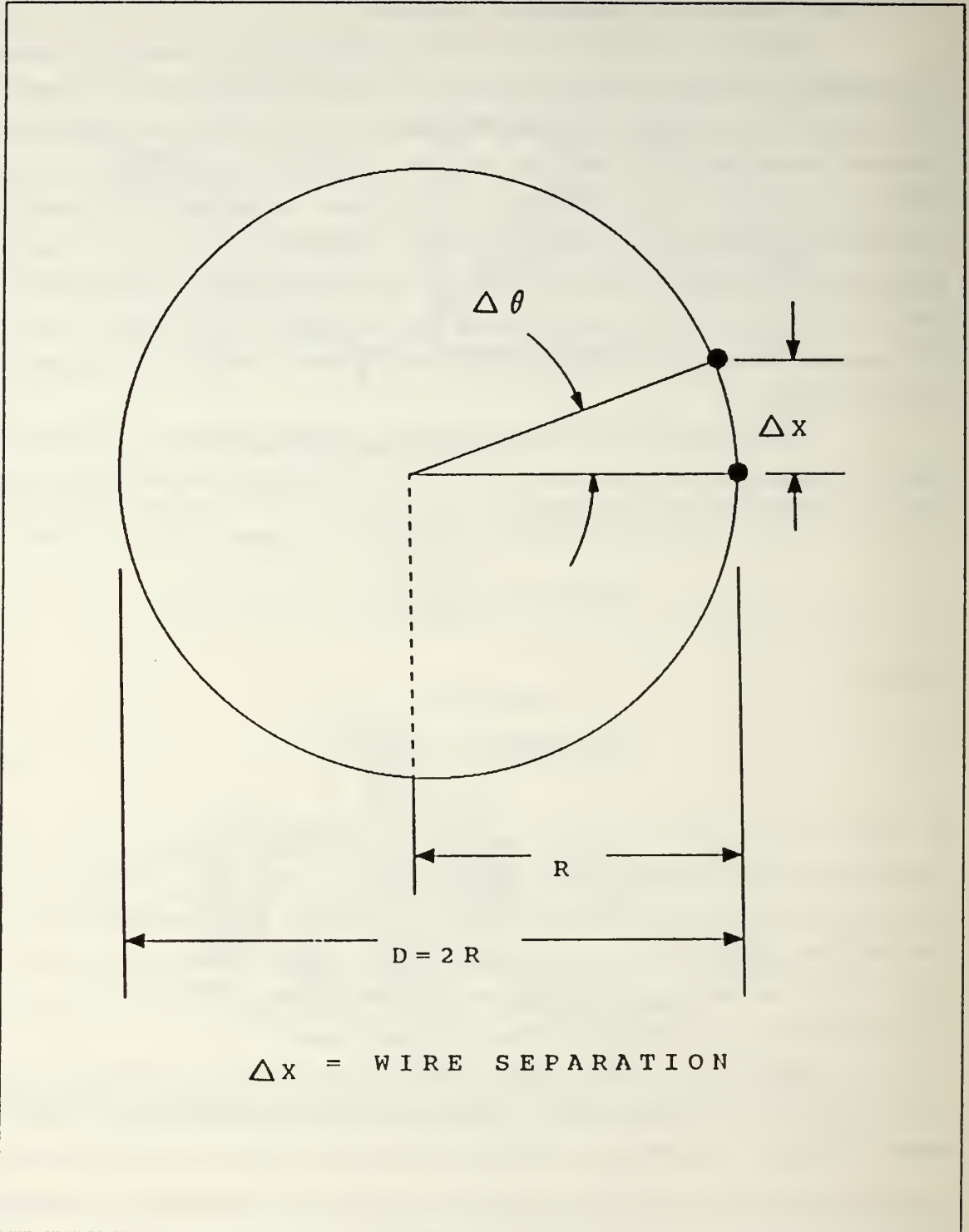


Figure 6. Geometry of an Angular Potentiometric Transducer

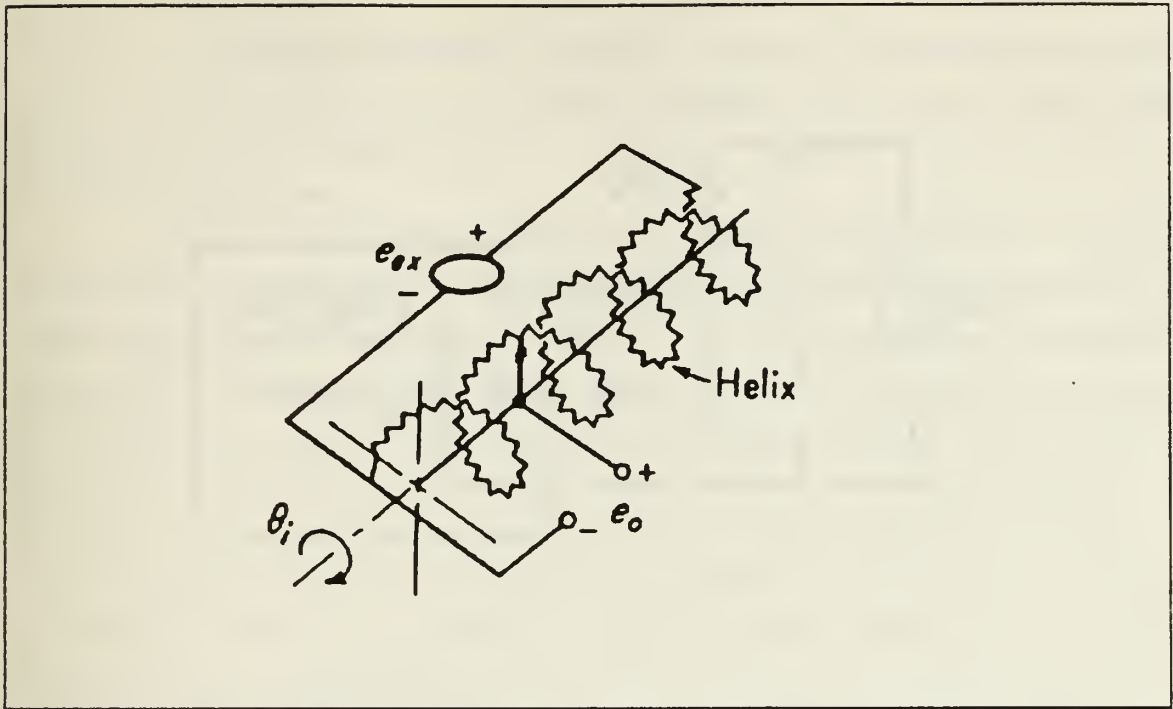


Figure 7. Multiturn Potentiometer: From Ref. 6: p. 218

output. The nonlinear relationship can be seen by analyzing the circuit shown in Figure 8. In the diagram the following variable definitions apply:

- e_x = Input voltage,
- e_o = Output voltage,
- R_p = Total resistance of the potentiometer,
- R_m = Meter resistance,
- x_t = Total range of the potentiometer, and
- x_i = Actual displacement of the potentiometer.

Assuming that R_p is uniformly distributed over x_t , analysis of the voltage divider circuit gives,

$$\frac{e_o}{e_x} = \frac{1}{\frac{x_t}{x_i} + \left(\frac{R_p}{R_m} \right) \left(1 - \frac{x_i}{x_t} \right)} \quad (3)$$

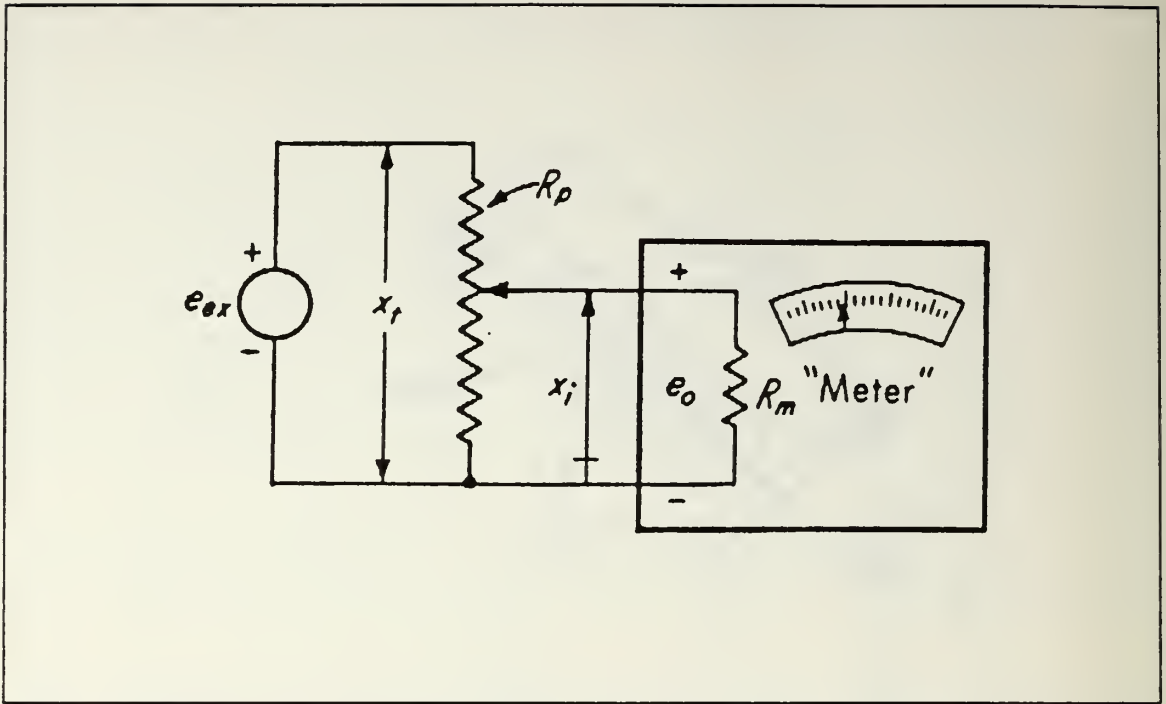


Figure 8. Potentiometric Transducer: From Ref. 6: p. 219

Thus, the ideal (i.e., linear) relationship,

$$\frac{e_o}{e_x} = \frac{x_i}{x_t} , \quad (4)$$

is true only when $R_p R_m = 0$, and since $R_p \neq 0$, and $R_m \neq \infty$, the nonlinear relationship in (3) will always exist. Doebelin states that "for values of $R_p/R_m < 0.1$ the position of maximum error occurs in the neighborhood of $x_i/x_t = 0.67$, and the maximum error is approximately $15(R_p/R_m)$ percent of full scale." [Ref. 6: p. 218] Other potentiometric transducers, which use a resistive element made of carbon film or a conducting plastic, are not subject to the same kind of resolution limitations as wirewound devices; however, they do have high output impedances and the corresponding nonlinearities described above. [Ref. 6: pp. 217-224]

A high quality multiturn potentiometer used in conjunction with a high quality voltmeter offered one possible solution to the design problem. However, the nonlinearity of this arrangement was a significant disadvantage, and the primary reason why potentiometers were not used.

d. Encoders

The angular displacement transducer, referred to in general as an angular encoder or shaft encoder, converts an angular displacement into a digital signal without the use of an analog-to-digital converter. In today's increasingly digital world this can be a distinct advantage.

There are three different transduction methods used in encoders. Magnetic encoders use a pattern made from magnetized and nonmagnetized segments and one or more magnetic sensors that register as either "1's" or "0's" depending on the magnetic characteristics of the section that they are adjacent to. Brush-type encoders are similar, but the sections are made of conducting and nonconducting materials. The conductors are all tied to a common source and the "sensor" is one or more brushes connected to the output. When the brush is in contact with one of the conductors the output is "on" and when the brush is in contact with an insulator the output is "off". Optical encoders (See Figure 9) use a pattern of opaque sections marked on an otherwise transparent disk. A light emitting diode (LED), or other light source, is placed on one side of the disk, and as the disk rotates a light sensor on the other side of the disk "sees" periods of dark and light which it converts into a digital signal. [Ref. 2: p. 106]

Angular encoders are further categorized as either absolute encoders or incremental encoders. Absolute encoders, similar to the optical encoder shown in Figure 9, use a multitrack pattern on a code wheel to produce a unique coded output signal for each incremental change in the measurand. These wheels use a variety of codes, including binary code, binary-coded decimal (BCD) and Gray code, to determine the shaft position. The resolution of an absolute shaft encoder is limited by the number of tracks on the disk and the type of code used. A simple binary or Gray code encoder, which are more efficient than the BCD encoders, with N tracks has an optimum angular resolution of

$$\Delta\theta = \frac{360^\circ}{2^N} . \quad (5)$$

Thus, to achieve the desired resolution of 10^{-4} radians on the Pan axis with an absolute encoder would require a code wheel with $N \geq 16$. Since the output from the encoder is unique for each position, these devices are not affected by power outages, and the requirements for a signal processor for such a device would be limited to a simple decoding circuit. These encoders can measure angles of up to 360° without ambiguity.

Incremental encoders use a code wheel which has only one track. As the shaft of the incremental encoder rotates the output from the encoder is a series of equally spaced pulses. These pulses can then be used as an input signal to an up/down (U/D) counter of some sort. The output from the counter is an indication of the displacement of the axis from some predetermined reference. The resolution of an incremental encoder is a function of the number of pulses the code wheel generates per revolution and is given by;

$$\Delta\theta = \frac{360^\circ}{n \times \text{PPR}} \quad (6)$$

where PPR is the number of pulses per revolution of the code wheel, and n is the number of revolutions that the code wheel makes per revolution of the axis of interest. If the incremental shaft encoder was mounted on the shaft of interest ($n=1$) at least 62,832 PPR would be required to ensure a resolution of 10^{-4} radians.

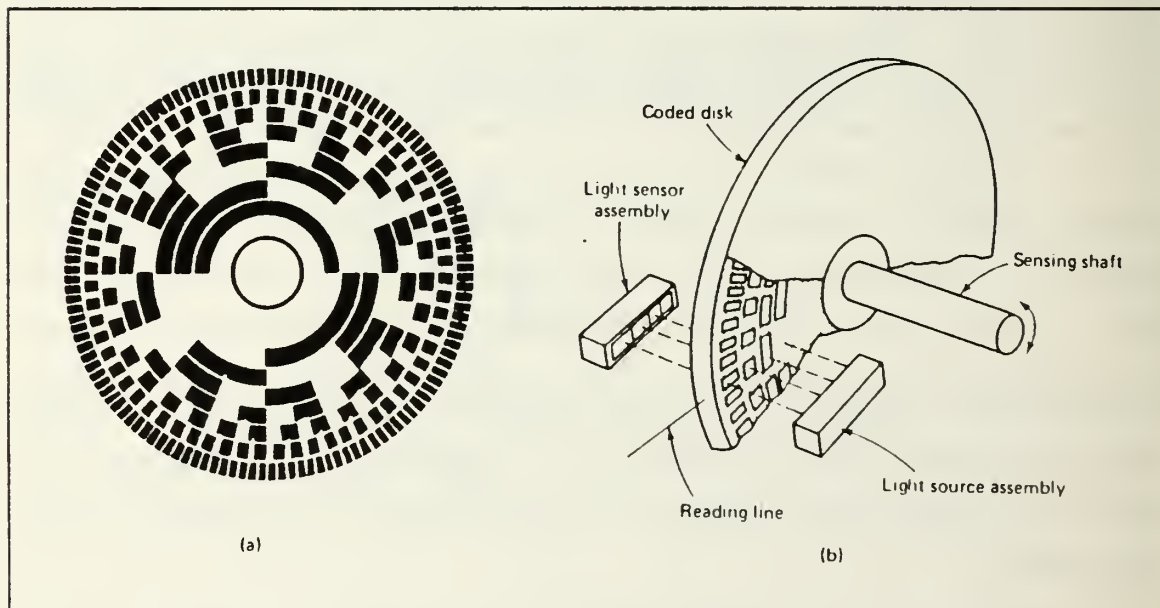


Figure 9. Absolute Photoelectric Angular Encoder: (a) typical code disk; (b) encoder elements. From Ref. 2: p. 107.

Shaft encoders currently range in price from less than \$100.00 to several thousand dollars depending on their capabilities and the method of transduction used. Litton Encoder's Model 60 absolute shaft encoder uses a natural binary code, has 15 tracks (0.1917 mrad resolution) and is available "off the shelf" for approximately \$3000.

Other absolute encoders with comparable resolutions are available at similar prices. No incremental encoders were found which offered the same kind of resolution as Litton's Model 60; however, because they are not limited to one revolution of the axis, the resolution of an incremental encoder can be improved by a factor of n by causing its code wheel to rotate n times for every rotation of the axis of interest. Incremental encoders with 1024 PPR are available from a variety of manufacturers for about \$100 each. Connecting such a device to the axis of interest via a gear train with a 50:1 ratio would theoretically result (from (6)) in a resolution of 0.1227 mrad. Incremental encoders do require more complex signal processing than absolute encoders, and they are affected by power shut-off. Additionally, unlike absolute encoders, any missed or erroneous count that occurs with an incremental encoder will cause a persistent error. [Ref. 7: p. 16]

After considering the measurement system performance criteria and the capabilities and limitations of the various transducers, the use of an incremental, optical shaft encoder appeared to be the best selection for the transducer for each axis. This decision involved balancing the various advantages and disadvantages of the different transducers. The following list gives a summary of the key considerations in this decision.

- Small, lightweight, highly accurate and relatively inexpensive models were readily available. Being small and lightweight suggested that mounting and weatherproofing the transducers in the camera servo should not be too difficult.
- Absolute encoders offer almost all of the advantages of the incremental encoders; they are not affected by power outage, they require less complex signal processing and one time counting errors do not persist. However, these features did not seem to justify the additional price of an absolute encoder.
- Linearity and loading problems associated with the potentiometric displacement transducers were avoided.
- Direct conversion of the measurand into a digital signal precluded the requirement for an A/D converter. (This would have been a disadvantage had the use of an analog signal conditioner been anticipated.)
- Using two identical transducers, each capable of meeting the specifications for the pan axis, would reduce system complexity while still ensuring that the design specifications were met.

C. MOUNTING THE TRANSDUCER

Once the decision to use an incremental optical shaft encoder was made, selection of a specific model remained. Before selection of an actual piece of hardware could be

Table 1. ANGULAR DISPLACEMENT TRANSDUCERS

TRANSDUCER DESIGN	RANGE	RESOLUTION	LINEARITY	OTHER
Reluctive Displacement (RVDT)	0° - 360°	Theoretically infinite; Limited by the signal conditioner.	Poor beyond $\pm 40^\circ$	
Reluctive Displacement (Farrand's INDUCTOSYN)	0° - 360°	$\pm (4 \times 10^{-4})^\circ$	Good	Large size limits usefulness with the camera measuring system.
Capacitive Displacement	0° - 300°	Theoretically infinite; Limited by the signal conditioner.	Good	Temperature sensitive
Potentiometric Displacement	0° - 3500°	Device dependent	Device dependent	The trade-off between range, resolution and linearity due to the loading effect of the noninfinite impedance of the signal conditioning devices used.
Absolute Encoders	0° - 360°	$\frac{360^\circ}{2^n}$	Good	No A/D conversion required. Insensitive to power shut-off.
Incremental Encoders	$\pm \infty$	$\frac{360^\circ}{n \times \text{PPR}}$	Good	Simple. Requires more signal processing than absolute encoder but is less expensive.

done though, one additional practical consideration had to be made; where and how could a transducer be mounted in or on the servo in order to measure the position of the Pan and Tilt axes?

The physical layout of the camera positioning servo made direct connection of any type of transducer to the axes of interest virtually impossible without major modification of the servo itself. Major modification of the servo would have been expensive, time consuming and outside the scope of this thesis. It was not considered an option in this case. Measurement of the Pan and Tilt axes' displacements was most readily accomplished indirectly. Each axis of the servo is positioned by a separate dc motor via a gear train. By mounting the shaft encoder code wheels to the sprockets (items 42 and 43 in

Figure 10) which are each attached to one of the worms, an indirect measurement of the position of each of the wormgears (items 5 and 7 in Figure 10) was possible. This approach, made necessary by the servo design, was a mixed blessing.

The backlash in a worm-wormgear connection will cause the position of the worm to be different for any given wormgear position, depending on whether that position is approached from a clockwise or a counterclockwise direction. In order to correctly determine the displacement of the wormgear by measuring the displacement of the worm, the amount of backlash present must be known (i.e., would have to be determined experimentally) and accounted for by the measurement system. This nonlinear source of error would not have been a concern if the servo was only required to rotate in one direction. This was not the case, however, and hysteresis eventually was determined to be the largest single source of error in the measurement system. A more complete discussion of this topic is included in Chapter IV of this thesis.

Assuming for the moment that the effects of the backlash in the gears could have been completely compensated for, mounting the shaft encoders on the worm provided a measurement advantage analogous to the mechanical advantage afforded by the gear train. Initial measurements indicated that each of the worms turned through $18,000^\circ$ ($50 \times 360^\circ$) for every 360° rotation of the corresponding wormgear. This meant that a shaft encoder with 100 divisions per 360° attached to the worm axis could do the same job as a 5,000 division per 360° encoder attached to the wormgear axis.

D. SELECTING AN OPTICAL SHAFT ENCODER

Once the basic decisions to use incremental optical shaft encoders and to mount the encoders on the worms inside the servo housing had been made, selection of the specific pieces of hardware was relatively straight forward and was primarily a matter of convenience and expediency.

Returning to the design specifications for a moment; the most stringent requirement was to be able to measure the position of the pan axis to within $\pm (5.73 \times 10^{-3})^\circ$. To determine the required resolution for the optical shaft encoder, the following calculations were performed.

First,

$$\frac{360^\circ/\text{Revolution}}{5.73 \times 10^{-3}^\circ/\text{Division}} \simeq 62,827 \frac{\text{Divisions}}{\text{Revolution}} \quad (7)$$

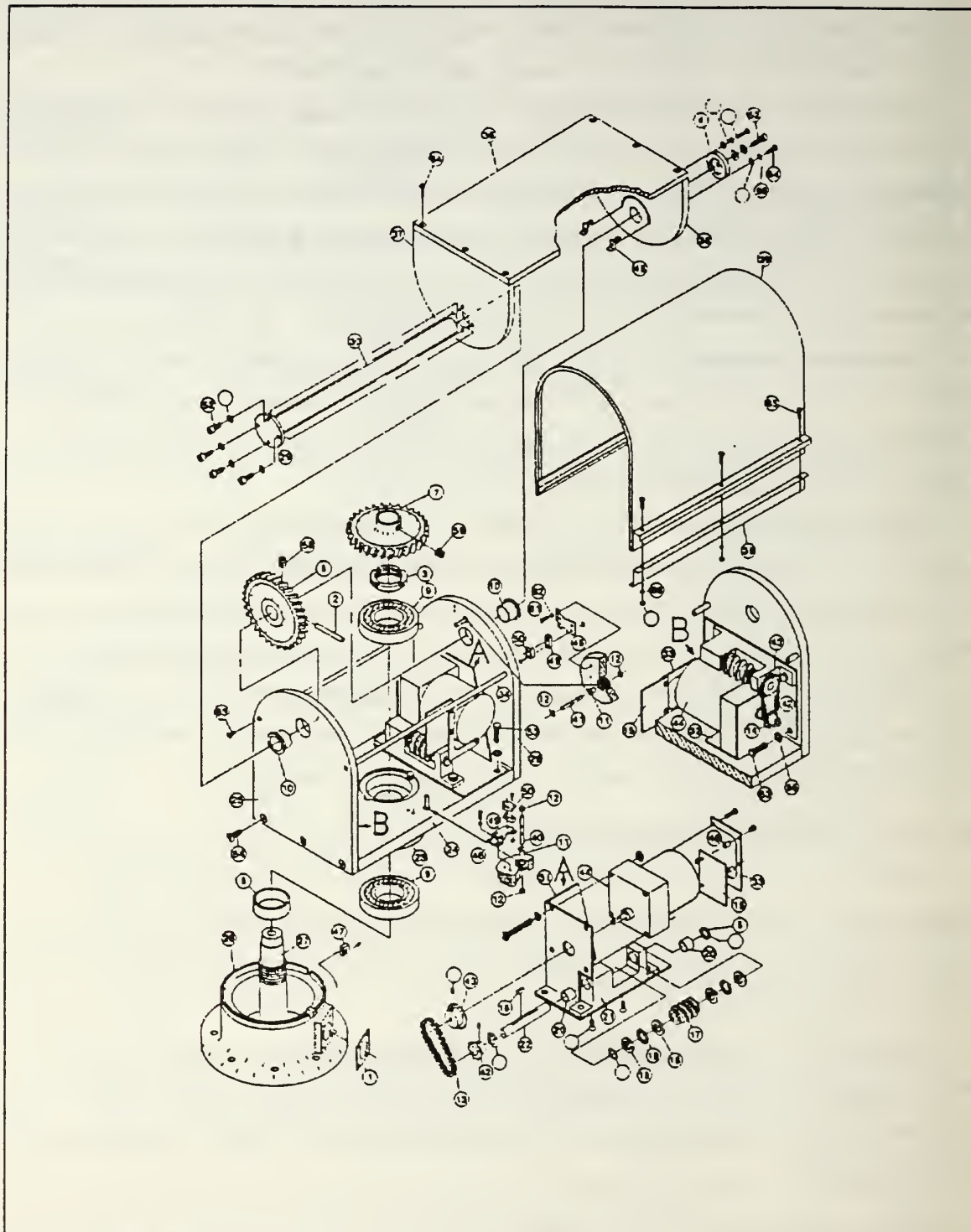


Figure 10. Camera Servo: From Ref. 8: p. 12.

Then, considering the 50:1 gear advantage,

$$\frac{62.827}{50} \approx 1257 \frac{\text{Divisions}}{\text{Revolution}} \quad (8)$$

The task therefore was to find an optical shaft encoder capable of detecting bidirectional rotation with at least 1257 Divisions/Revolution in a package small enough to mount in the servo housing on the worm axis. There was no absolute size limitation; however, due to the construction of the servo it was desirable to find an encoder that was no more than 3 in. in diameter and no more than 1.5 in. in width. The companies that make shaft encoders are capable of custom building devices to meet a customer's specific needs. However, the prices are high, and the lead times are long for these special order parts. The encoder for this system needed to be reasonably priced and readily available to ensure timely completion of the project and to facilitate replacement, if necessary, in the future.

Optical shaft encoders are manufactured by numerous companies including Litton, Honeywell, BEI, IVO and Hewlett Packard. Sales literature from these companies was reviewed prior to making a decision on the specific shaft encoder model to be used. Incremental optical shaft encoders with resolutions that range from one pulse per revolution (PPR) to 2540 PPR are available off the shelf from one or more of these companies. While evaluating sources of supply, incremental optical shaft encoders were also found in use in various laboratories and shops in the Electrical Engineering and Physics Departments at the NPS. Encoders immediately available from stock included two Vernitech 1200 PPR (model VOE-23-1200-AI-LD5-2L1-1603-2) encoders from the Physics Department and two Hewlett Packard (HEDS-6000 J06) encoders from the Electrical Engineering Department. The use of the Vernitech encoders was ruled out because they were unable to detect bidirectional movement without increasing the complexity of the signal conditioning subsystem. Additionally, technical literature requested on two separate occasions from Vernitech was never received.

The HEDS-6000 J06 encoders have a resolution of 1024 PPR. Each encoder provides displacement information in the form of TTL logic level signals via two output channels. When the encoder is properly adjusted the two output signals have a 90° phase difference. This quadrature phase relationship permits these encoders to detect bidirectional displacements. Rotation in one direction will cause Channel A to lead

Channel B (in phase), while rotation in the other direction will cause Channel B to lead Channel A. [Ref. 9: p. 2]

The presence of two output channels in quadrature phase has an additional benefit that is useful in some applications. Since the amount of position information has essentially been doubled, if the signal conditioner is designed to detect both the leading and trailing edges of one of the output channels the resolution of the measurement system can be doubled. The difficulty with using this technique is that multiple oscillations about a single point cannot be detected as such. If the camera were to oscillate less than one half of a pulse width about a transition the signal conditioner would detect and erroneously count the multiple transitions. [Ref. 7: pp. 13-16]

With 1024 PPR, which is less than the 1257 PPR required to meet the 0.1 milliradian accuracy specification on the pan axis, the maximum resolution available, if the HEDS-6000 was attached to the worm, can be calculated as;

$$\frac{360^\circ}{(50 \times 1024)} = (7.03125 \times 10^{-3})^\circ \text{ Pulse}^{-1} . \quad (9)$$

Although this was not sufficient to satisfy the pan axis resolution specification of $(5.73 \times 10^{-3})^\circ \text{ Pulse}^{-1}$ all of the other performance criteria could be satisfied. The trade-off seemed reasonable and was approved prior to proceeding further with the system design.

E. THE DISPLAY

Selecting a method to display the final system output was certainly the least demanding task required in the design of the system. With an expected resolution on the pan axis of approximately 0.007° over a range of 360° (a ratio of about 1:51,500) an analog display seemed out of the question. A five or six digit digital display on the other hand offered a simple, reliable and cost efficient means of presenting the output. Constructing the displays from individual, seven-segment, common anode, LED devices, and the appropriate display drivers was a straight forward task.

F. THE SIGNAL CONDITIONER

Anticipating the use of two incremental shaft encoders as the transducers for the measurement system and the use of digital readouts as the display devices significantly reduced the number of possibilities for the signal conditioning subsystem. In addition to the hardware and software described in each of the subsequent discussions, each

technique listed here would require an edge detector to detect the transitions in the TTL signals from the shaft encoders.

- Up/down counter with table look-up.
- Up/down counter and multiplication.
- Add/subtract.
- Microcomputer.
- Microprocessor.

1. Up/down (U/D) counter with table look-up

This technique would involve the use of a shift register, some associated logic, an U/D counter and a table look-up device such as an erasable programmable read only memory (EPROM). The shift register would serve as a hardware buffer that could be used to account for the hysteresis introduced by the worm-wormgear assembly. The length of the buffer would have to be determined experimentally. The logic associated with the shift register would determine the "validity" of each transition (count) signal from the edge detector by checking the contents of the shift register and comparing the current direction of rotation with the previous direction of rotation. Whenever the logic detected a change in rotation direction, or a partially full, or a partially empty buffer (depending on the direction of rotation), the transition would not represent a "valid" count since any of these conditions would indicate that the transition was due to a change in the position of the worm without a corresponding change in the position of the wormgear. Thus, the present transition would be the result of hysteresis due to the backlash in the gear train and the transition would be "invalid". Such a transition would cause the contents of the hysteresis buffer to be modified appropriately. A more complete discussion of this topic is contained in Chapter IV. The shift register and associated logic could be built from common TTL devices readily available at the NPS.

Once a count had been determined to be valid, an U/D counter would be used to keep a running total of the number of counts. Again, such a device could be built using readily available TTL devices such as the 74LS168A, Synchronous 4-Bit Up/Down Decade Counter, or the 74LS169A, Synchronous 4-Bit Up/Down Binary Counter. The output from the U/D counter would then be used as an address to "look up" a predetermined number stored in an EPROM.

This design approach was considered relatively straightforward, and at least initially seemed like a viable option. Its major advantage was that it was conceptually quite simple. This simplicity had a price though; it would have been very hardware in-

tensive and consequently would have been a very inflexible design. For example, if at a later date the use of an arbitrary reference was desired, additional hardware would have to be added to the signal conditioner so that the counter could be initialized to the arbitrary starting point. Since all of the processing would have to be done in hardware, even a minor modification in the system could necessitate a major design revision. Another consideration was that saving in excess of 51,000 unique positions in the EPROM presented a nontrivial problem that would need to be solved if this technique was used.

2. Up/down counter and multiplication

This is very similar to the previous case, differing only in that instead of looking up a predetermined position, in a memory device, a multiplier would be used to multiply the output of the U/D counter by a predetermined constant. As an example, if experimental results indicated that the shaft encoders generated one pulse for every 0.00703125° that the camera was displaced, then each time a valid count was received, the updated count would need to be multiplied by 0.00703125 in the final stage of the signal processor. The result would be the new position. Again, while conceptually simple this idea had some significant disadvantages. Even more hardware intensive than the first approach, this design would also have extremely limited flexibility.

Accomplishing the multiplication would have posed a formidable task. The scale factor would have to be written as some integer (e.g., 0.00703125 would become 703125, or 70323, or 7031, etc.) depending on the desired accuracy. The count, already an integer, would be multiplied by the constant and the correct position of the decimal point would have to be determined. Locating the decimal point would be a relatively simple task, but multiplication of two numbers such as 51,000 and 70,313 would not be as easy. At least one 16 bit by 16 bit binary multiplier (i.e., TRW's MPY016H) is currently available, but since the number 70313 cannot be represented in binary by less than 17 bits, the multiplication could have been accomplished in either of two ways. One solution would have been to perform the multiplication in two or more stages. Alternatively, 70313 could be "rounded" to 7031. The second option would create a cumulative round-off of about $(1.28 \times 10^{-3})^\circ$ per 360° rotation (assuming 51,200 pulses per 360°). This round-off error would probably have been acceptable, but the complexity and limited flexibility of either multiplication scheme made the U/D counter and multiplication an unacceptable candidate for the signal processing subsystem.

3. Add/subtract

A third design concept considered the elimination of the U/D counter altogether. The same logic proposed for use in the previous two designs could have been

used to check the validity of a count and to determine the direction of rotation. However, instead of valid counts being sent to an U/D counter as before, these counts would now signal an adder to add or subtract a predetermined constant from the running total. Just as before, this simple idea could probably have been made to work at least once, but its usefulness as a part of a larger system would certainly have been limited. The large number of components required to realize this design would have increased the probability of failure, complicated troubleshooting and reduced overall flexibility.

4. Microcomputer

If the signal processing subsystem was built around a microcomputer (PC), virtually all of the disadvantages associated with the previously discussed approaches would be eliminated. Since all of the logic could be implemented in software, modifications to the system would be relatively simple to make, and the system's flexibility would be enhanced. However, dedicating a microcomputer, even an inexpensive model, to the signal processing tasks for this measurement system was considered overkill, and timesharing with one of the PC's already in service was possible, but not considered practical or convenient since these microcomputers had already been dedicated to a variety of tasks.

5. Microprocessor

One final option for the signal processor remained. Microprocessors are relatively inexpensive and powerful and are available in a wide variety of makes and models. If a microprocessor was used instead of a microcomputer or a straight hardware processor, the "nice to have" requirements such as flexibility, ease of modification and capacity for expansion, as well as the required signal processing functions could all be satisfied. On the other hand, microprocessors have one distinct disadvantage; they are not user friendly. The use of a microprocessor implied countless hours spent tracking individual bits, debugging assembly language code, studying timing diagrams, etc.. No matter how distasteful the thought, however, a microprocessor was clearly the best way to perform the signal processing functions of the measurement system.

As with the selection of the transducer, once the basic design approach had been determined, selection of a specific device was a relatively straight forward task. The choice of one microprocessor over another was a function of the processor's ability to perform the required tasks, cost effectiveness and availability. Motorola's MC68705U3 seemed to satisfy all of these requirements. The MC68705U3 is a four kilobyte EPROM microprocessor, built using HMOS (high-density NMOS) technology with an eight bit architecture. The "68705" operates on a 5.0 volt dc supply, has 112 bytes of on chip RAM, four vectored interrupts, 24 TTL/CMOS compatible bidirectional I/O lines (eight

lines are LED compatible), eight dedicated input lines and an internal eight bit timer with a seven bit programmable prescaler. [Ref. 10: p. 1]

In Ref. 10 Motorola advertises the following software features:

- Programming language similar to the 6800 family.
- Byte efficient instruction set.
- Easy to program.
- True bit manipulation.
- Bit test and branch instructions.
- Versatile interrupt handling.
- Powerful indexed addressing for tables.
- Versatile index register.
- A full set of conditional branches.
- Memory usable as registers/flags.
- Single instruction memory examine/change capability.
- Ten powerful addressing modes.
- All addressing modes apply to EPROM, RAM and I/O.

One key advantage to using the MC68705U3 was that one of the microprocessors, and a Motorola M68705EVM (the evaluation/programming module for the M6805 family of devices) were both available for immediate use at the NPS. The fact that the 68705 utilized HMOS technology suggested that it should be a relatively low cost microprocessor. In fact, except for the price of a phone call, a second microprocessor was obtained free of charge from a local electronics wholesaler. Additional microprocessors, to be used as replacements and as backup devices were ordered for about \$20.00 each.

One potential problem with using a microprocessor begged checking prior to proceeding. Initial measurements of the camera's maximum rotation velocity produced the following results.

$$\omega_{PAN(\max)} \simeq 1.0 \text{ rpm} \quad (10)$$

$$\omega_{TILT(\max)} \simeq 0.5 \text{ rpm} \quad (11)$$

Again the requirements for the pan axis presented the most stringent design limitations. Since the optical shaft encoders were anticipated to deliver 51,200 PPR (1024×50) the

microprocessor on the pan axis had to be capable of processing 51,200 pulses/minute (1.172 ms / pulse). The MC68705U3 is designed to operate with an oscillator frequency (f_{osc}) of between 0.4 MHz and 4.4 MHz and has an instruction cycle time ($4/f_{osc}$) of between 0.950 μ s and 10 μ s. Assuming that a 4.0 MHz clock was used, the instruction cycle time would be 1.0 μ s. This would mean that the processing of each pulse would have to be accomplished in no more than 1172 instruction cycles to ensure that no pulses would be missed.

III. DESIGN

A. GENERAL

The schematic diagrams for the measurement system are shown in Appendix A; Appendix B contains copies of the printed circuit board plans. Before describing the detailed operation of each of the individual components of the measurement system, a brief overview of its basic theory of operation is in order. The measurement system is actually two separate systems operating independently. The system designed to measure the azimuth or pan angle will subsequently be referred to as the "Pan System", and the other system, designed to measure the elevation or tilt angle, will be referred to as the "Tilt System". However, because the two systems are quite similar the discussion which follows will only specifically describe the operation of both systems where their operation differs.

In the most general terms, the measurement system shown in Figure 2 on page 6 uses two microprocessors to count the pulses generated by the incremental shaft encoders, and to provide output signals to the display devices. The counting function performed by each microprocessor involves determining the direction of rotation and determining whether each count is "valid". Valid counts are encoder pulses which result from the displacement of the camera servo, while invalid counts are a result of the hysteresis in the gear train. The number of valid counts is directly proportional to the angular displacement of the camera axis.

Both of the displays are capable of presenting the position information in two basic forms. In the Count Mode they display the number of pulses that have been detected, and in the Position Mode they display the angle in degrees that the number of pulses represents. A third display mode, which is a combination of the first two, is also available. In the third mode, referred to as the "Blinking Mode", the display will alternately display the count and the angle.

B. SHAFT ENCODER AND LINE DRIVER

Figure 11 shows the basic components of the HEDS-6000 incremental optical shaft encoder. The encoder is approximately 56 mm in diameter and 20 mm deep. The code wheel assemblies for the HEDS-6000 J06 encoders are designed to mount on 0.25 in. shafts. Since the mounting surface shown in Figure 11 is not part of the encoder kit, and did not exist on either of the worm axes, two such surfaces were machined in the

Physics Department Shop and attached to one end of each of the worms. Each surface has a 0.25 in. diameter shaft to which one of the code wheel assemblies is attached. Two sheet metal brackets, also made in the Physics Department Shop, are bolted to the servo frame. The encoder bodies are mounted to these brackets. Figure 12 shows the shaft encoders mounted in the camera servo. [Ref. 9: p.1]

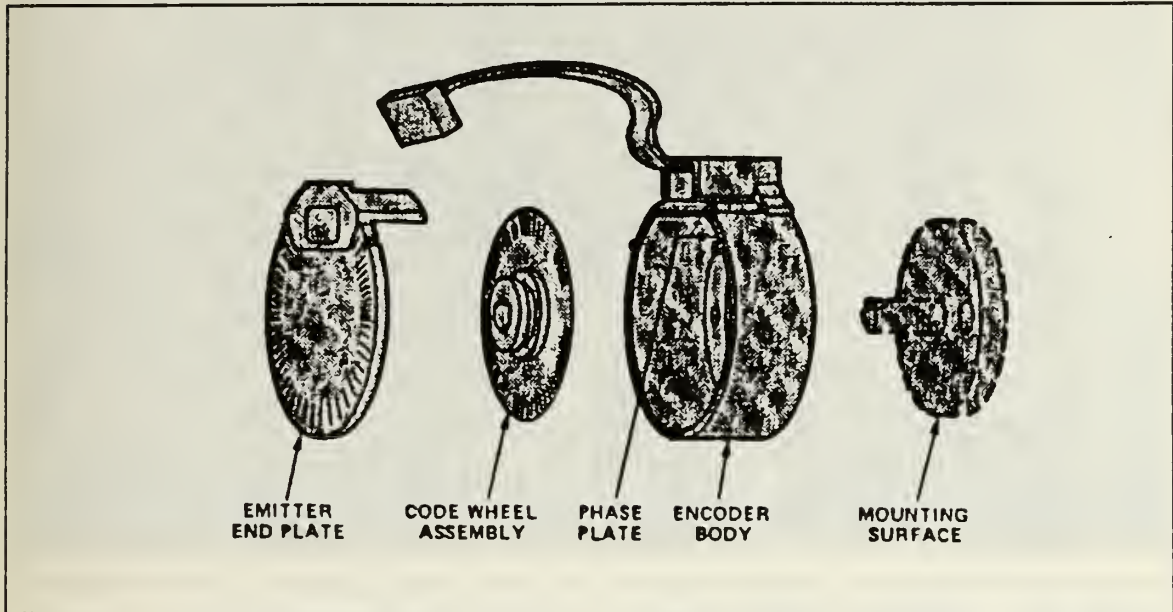


Figure 11. HEDS-6000 Series Encoder Kit: From Ref 9: p.6.

Also seen in Figure 12 is a printed circuit board mounted between the two optical shaft encoders. Each of the encoders is electrically connected to the board via a separate ten wire ribbon cable. The power and the output signals from the shaft encoders are transmitted through these cables. A sketch of the ribbon cable connector and the pinout for the connector are shown in Figure 13. Each connector is attached to a ten pin header on the printed circuit board. Pins 2, 7 and 9 are connected to a +5.0 Vdc power supply external to the camera servo. A description of the power supply is given later in this chapter. Pins 3, 4, 5 and 6 are connected to the power supply ground. The HEDS-6000 does not have an index pulse, therefore pin 10 is not connected.

The remaining two pins on each header connect the output channels of the shaft encoders to two 74S140 line drivers. Each 74S140 is a dual four-input NAND gate 50-Ohm line driver. The line drivers are powered by the same supply as the encoders. They serve as buffers between the encoders and the transmission lines which are used to transmit the encoder signals to the signal conditioner. The line drivers' typical high

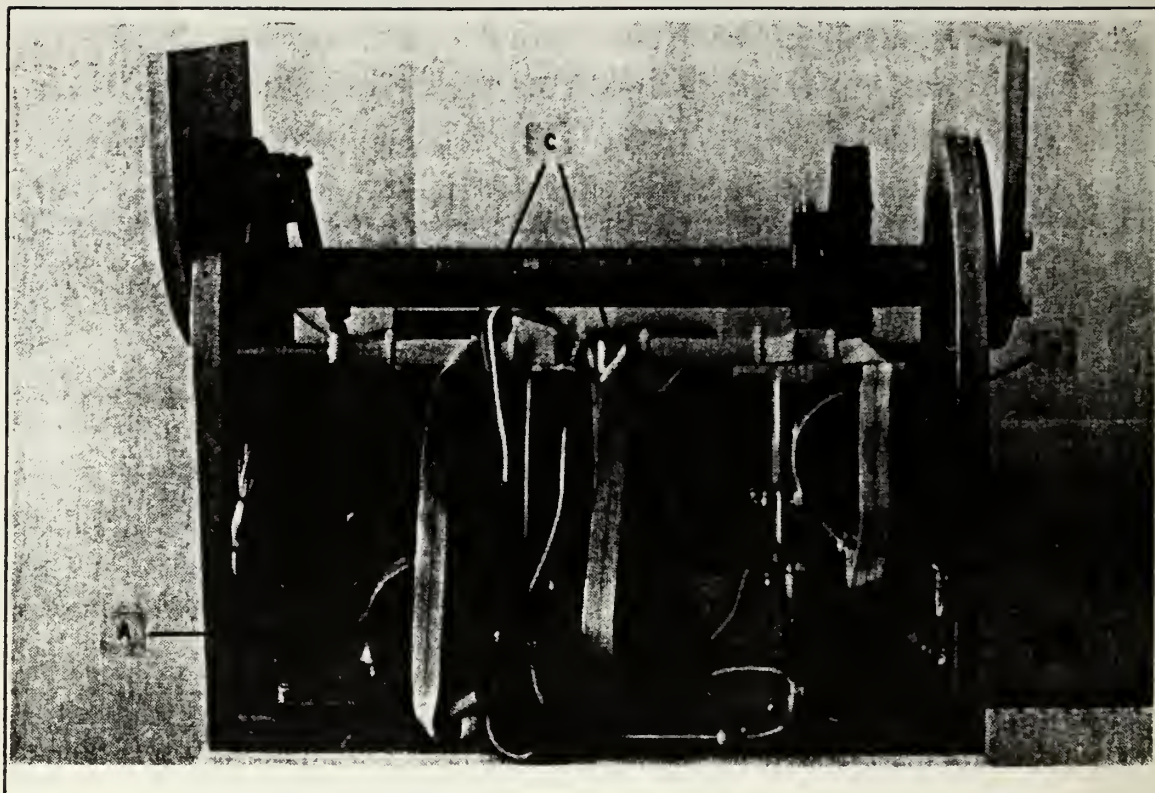


Figure 12. Modified Camera Servo: (a) Optical shaft encoder used to measure Pan axis displacement, (b) Optical shaft encoder used to measure Tilt axis displacement, (c) Ribbon cable, (d) Printed circuit board.

output current is 10 mA and the maximum is 18 mA. Resistance in the transmission line was measured to be approximately $35\ \Omega$, and to be on the safe side a $10\ \Omega$ connector loss was assumed. The voltage drop due to an 18 mA current through a $45\ \Omega$ resistance is 0.81 V. A "voltage high" signal received at the signal conditioner should therefore be about 4.19 V. This is well above the maximum, positive-going threshold voltage specification of 2.0 V for the 7414 Schmitt triggers, which are used to receive the signals at the signal processor. [Ref. 11: pp. 5-73, 5-74, 6-44]

C. ENCODER-MICROPROCESSOR INTERFACE

The signals transmitted by the two line drivers are Channels A and B of each of the shaft encoders. These signals contain the raw data which the signal processor converts into position information. Three pairs of multiple pin connectors are used in the encoder-microprocessor interface. The pinouts for these connectors are shown in



PINOUT

PIN #	FUNCTION
1	CHANNEL A
2	V _{CC}
3	GROUND
4	N.C. OR GROUND
5	N.C. OR GROUND
6	GROUND
7	V _{CC}
8	CHANNEL B
9	V _{CC}
10	CHANNEL I

Figure 13. Encoder Connector Specifications: From Ref. 9: p. 6.

Figure 14. Each of the four signals is received at the signal processor by a 7414 Schmitt trigger which is used to “clean up” the signal. The Schmitt triggers lower the system’s susceptibility to errors caused by slow state transitions and increase the signals’ fan out capabilities [Ref. 7: p. 13].

The output of each Schmitt trigger is routed to an input port of the appropriate microprocessor. Each Channel A signal is also the input to an edge detector. The edge detectors each consist of three 7414 inverters, a 74LS86 EXOR gate and a 47 nF capacitor, configured in the manner shown in Figure 15. This configuration causes the interrupt line to go low for approximately 2 μ s each time Channel A transitions from low to high or from high to low. Since an oscillator frequency, f_{osc} , of 4.0 MHz is being used, the interrupt pulse width, t_{WL} , must be greater than or equal to 1.25 μ s [Ref. 10: p. 3]. The value of the capacitor required to achieve the 2 μ s delay was determined experimentally.

D. SWITCHES

The measurement system has 10 switches that allow the operator to control specific functions of the signal processors and the displays. Figure 16 shows the physical location of these switches on the control panel. Switches SW1(P) and SW1(T) control the reset lines to the microprocessors. Switches SW2(P), SW2(T) and SW5 control the display mode. The Function and Set switches; (SW3(P), SW3(T), SW4(P) and SW4(T)) allow the user to change the length of the hysteresis buffer in the microprocessor. The

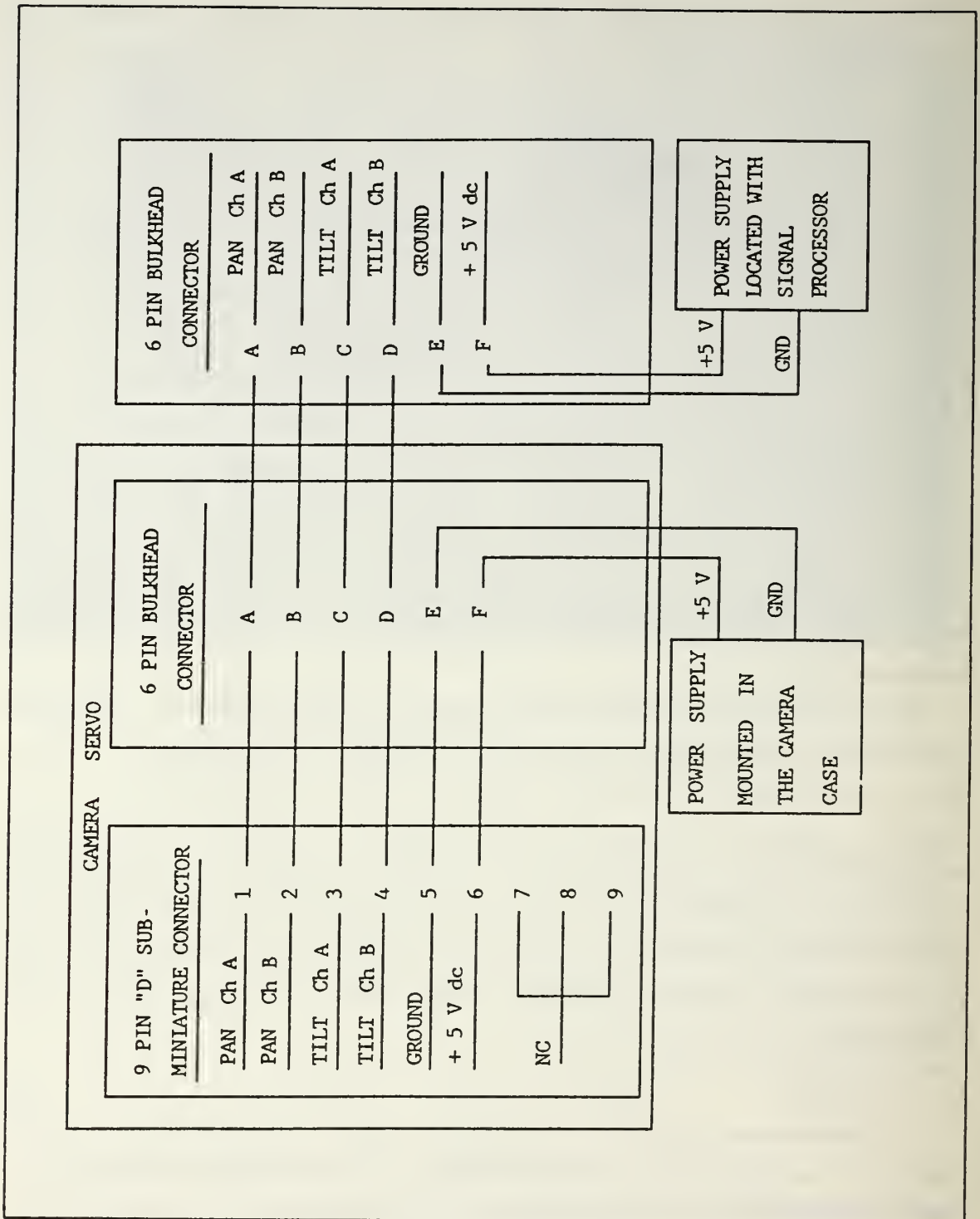


Figure 14. Encoder-Microprocessor Connector Specifications

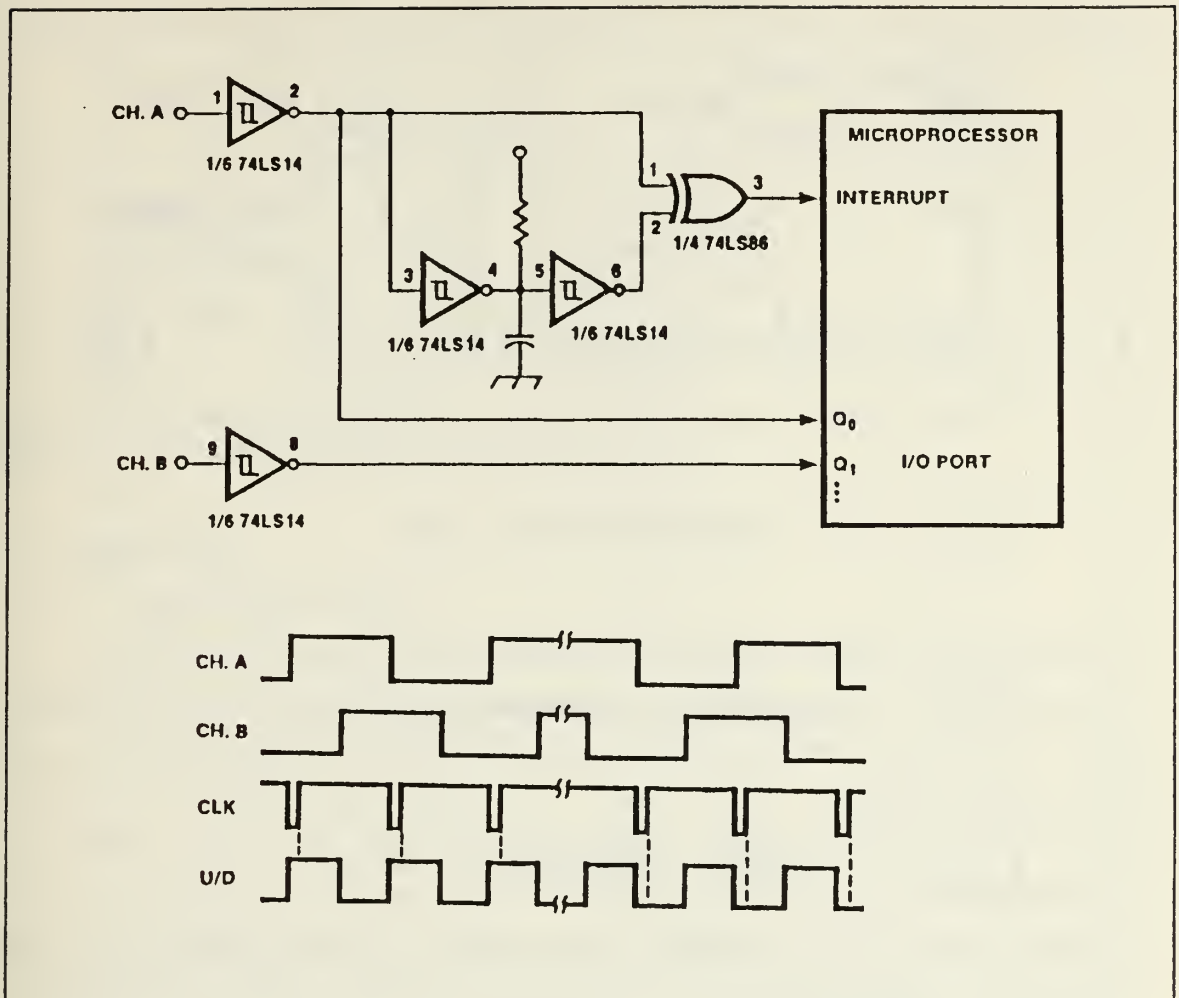


Figure 15. Interrupt Interface: After Ref 7: p. 14.

master power switch is SW6. Table 2 identifies the switches by name, description and function.

Any mechanical switch will “bounce” or “chatter” when it is thrown, and since the operation of the signal processor depends on the number of times that the Display Mode and Set switches change position, these switches had to be “debounced”. A very simple but effective way to do this is with an \overline{RS} latch. Switches SW2(P), SW2(T), SW4(P) and SW4(T) are each debounced in this manner. Each latch is made from two 74S00 NAND gates connected in the manner shown in Figure 17. [Refs. 13: pp. 132-135, 12 : pp. 3,4]

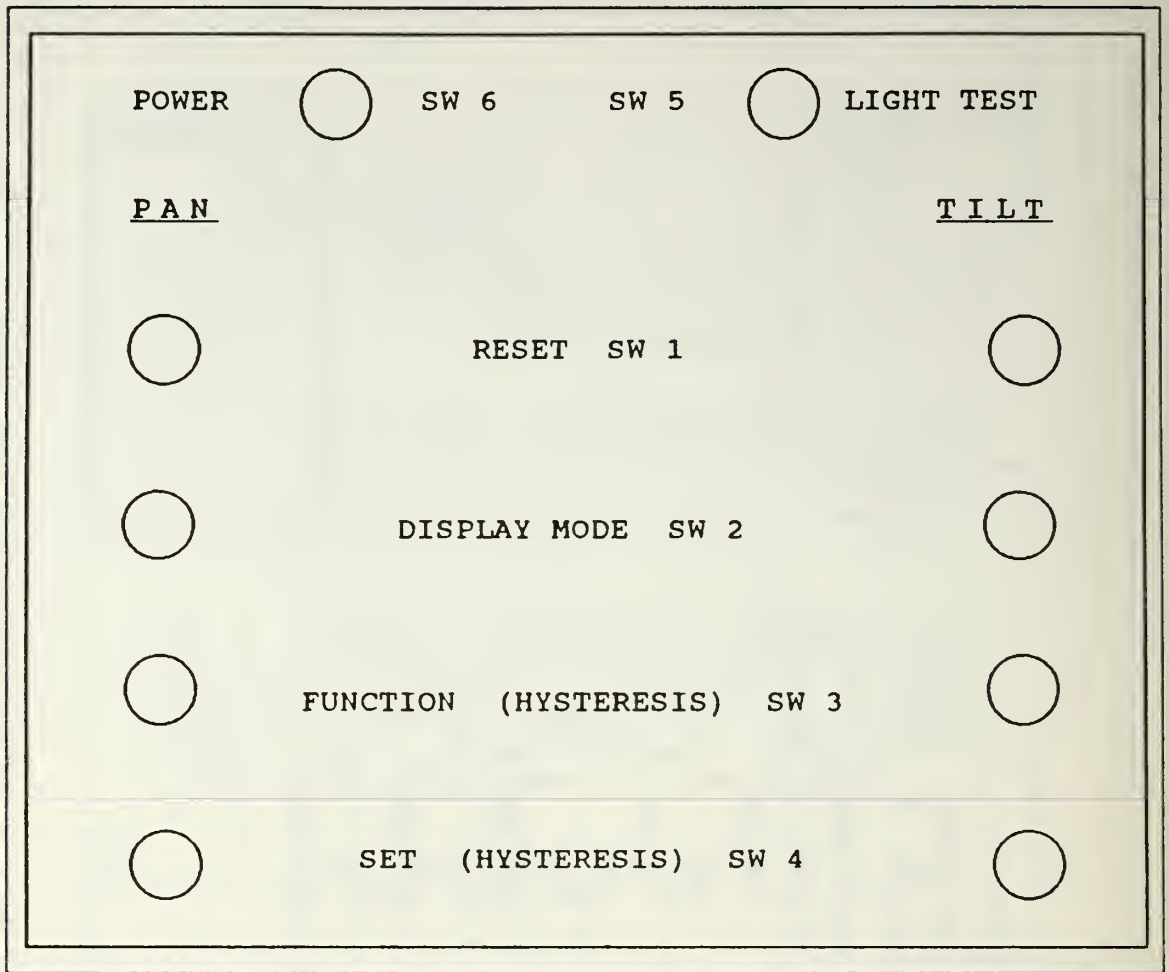


Figure 16. Control Panel

E. MC68705U3

1. General

The two 40 pin MC68705U3 microprocessors (MPU's) are the heart of the measurement system. With the exception of the light test signal, every signal in the system is either part of the input to one of the MPU's or part of their output. The MPU's were programmed using the assembly language syntax, assembler directives and instruction set for the M6805 family of microprocessors which are described in Ref. 14. The Pan and Tilt programs are listed and their operation is described in Appendix D. The pin assignments for the MC68705U3 are shown in Figure 18. Table 3 briefly describes the purpose of each pin and the actual connections for the two MPU's.

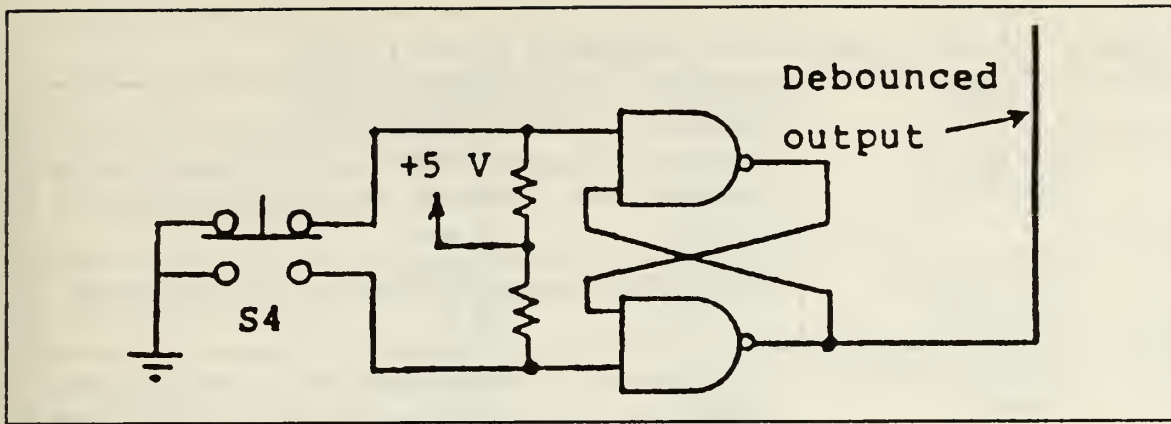


Figure 17. Debouncing circuit: After Ref 12: p. 4.

2. Memory Map

a. Input/Output (I/O)

The memory map for the MC68705U3 is shown in Figure 19. The digits following a "S" are the hexadecimal representation of the address for a specific memory location. The data registers occupy the first four memory locations of each MPU. Thus the information written into the registers at S000, S001 and S002 is written to the output ports A, B and C respectively. Port D, at address S003, is an input only port as indicated in Table 3. In order to determine the state of the input lines, the contents of the register at S003 must be read by the MPU. Registers S004, S005 and S006 are the data direction registers (DDR's) for Ports A, B and C respectively. Because all three ports are used as "output only" ports, in this application, the DDR's are all established as such by an initialization routine performed by the MPU's during their initial power-up and after each external reset. [Ref. 10: pp. 5, 12, 14]

Pin 18 of the MPU can be used as either a general purpose input line or as an interrupt line. The primary interrupt line on each MPU is used to signal the occurrence of a state transition on Channel A. Pin 18 is used as a second interrupt line to signal a display mode change request from the operator. The Miscellaneous Register (MR) at address S0A is used to control the operation of the second interrupt line ($\overline{\text{INT2}}$). In order to establish pin 18 as an interrupt line, bit 6 of the MR is cleared by the Initialization Routine. The $\overline{\text{INT2}}$ Interrupt Request Bit, bit 7 of the MR, is cleared by default upon reset. It is set when a falling edge is detected on the Display Mode line which is connected to pin 18. When this occurs and bit 6 of the MR is cleared, an interrupt request is generated. This interrupt request causes the display mode to change.

Table 2. SIGNAL PROCESSOR AND DISPLAY SWITCHES

NAME	DESCRIPTION AND FUNCTION
PAN RESET (SW1(P))	Momentary action push button switch: Resets the Pan Microprocessor. Causes the Pan Display to be reset to zero.
TILT RESET (SW1(T))	Same as SW1(P) except it affects the Tilt System only.
PAN DISPLAY MODE (SW2(P))	Single pole double throw toggle switch: Each time the switch position is changed the Pan Display toggles from Count mode, to Position Mode, to Blinking Mode, to Count Mode, etc..
TILT DISPLAY MODE (SW2(T))	Same as SW2(P) except it affects the Tilt Display only.
FUNCTION (HYSTERESIS) (SW3(P))	Single pole double throw switch: When closed, causes the "Function" line of the Pan Microprocessor to go low and causes the size of the hysteresis buffer to be displayed on the Pan Display. Enables SW4(P).
FUNCTION (HYSTERESIS) (SW3(T))	Same as SW3(P) except it affects the Tilt System only.
SET HYSTERESIS (SW4(P))	Single pole double throw switch: Inoperable unless SW3(P) is closed. If SW3(P) is closed, each time the position of SW4(P) is changed the length of the hysteresis buffer is incremented by one. Maximum buffer length is 25. Toggling SW4(P) when the buffer length is 25 will cause the buffer length to be reset to zero.
SET HYSTERESIS (SW4(T))	Same as SW4(P) except it affects the Tilt Hysteresis buffer.
LIGHT TEST (SW5)	Single pole single throw switch: When closed, lines 1, 2, 7, 8, 10, 11 and 13 on each of the LED displays will go low. Unless an element is burned out, every digit in both displays should be an eight.
POWER (SW6)	Single pole single throw switch: When closed, applies + 5.0 V dc power to the signal processors and the displays.

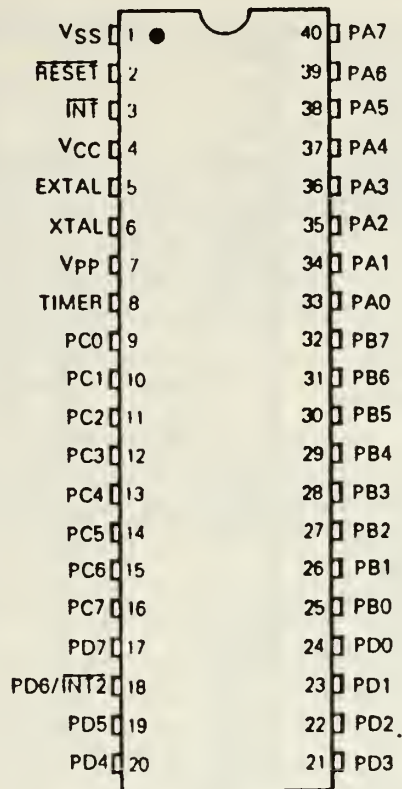


Figure 18. MC68705U3 Pin assignments: From Ref. 10: p. 1.

Once bit 7 has been set by an interrupt, it must be cleared by software to avoid repeated and unwanted interrupts from occurring. This task is performed by the Mode Change Routine in each EPROM. [Ref. 10: pp. 1, 10, 13, 15]

b. Timer

The operator can cause either or both of the displays to “blink” by using the Display Mode Switches, SW2(P) and SW2(T). When one of the systems has its display in the Blinking Mode, the associated MPU uses its timer to generate a timer interrupt request every second. The interrupt request causes the MPU to execute the Mode Change Routine. A block diagram of the timer is shown in Figure 20. The timer consists of an eight-bit counter which is decremented toward zero by the f_{CIN} input. When the counter reaches zero, it sets the Timer Interrupt Request Bit (TIR) of the Timer Control Register (TCR), and a timer interrupt request is generated unless the

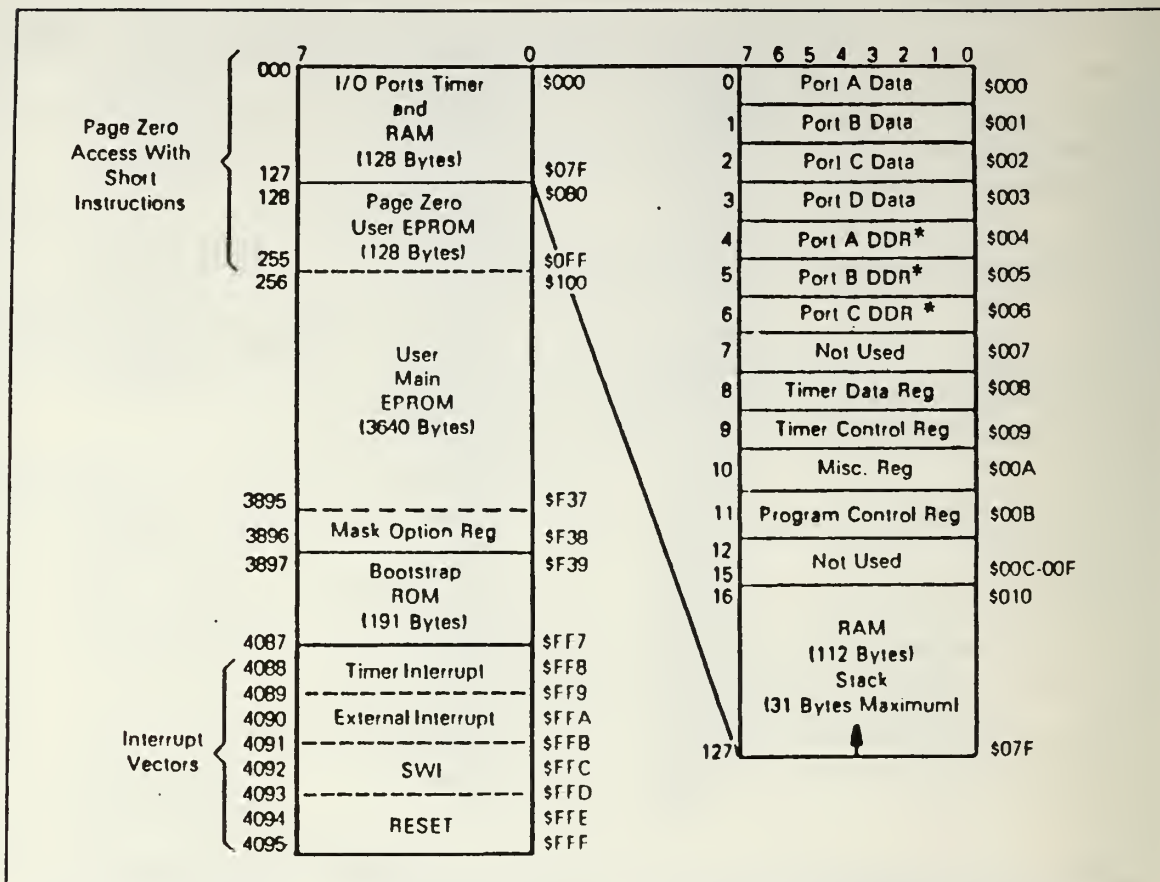


Figure 19. MC68705U3 Memory Configuration: From Ref. 10: p. 5.

Timer Interrupt Mask Bit (TIM) of the TCR is set. A brief description of each of the timer registers and their configuration follows.

(1) *Timer Data Register (TDR)*. The TDR is the eight-bit counter which sets the TIR bit of the TCR when it decrements to zero.

(2) *Timer Control Register*. The contents of the TCR determine the general operation of the timer.

- Bit 7, Timer Interrupt Request (TIR), signals a TDR underflow when it is set and will cause a timer interrupt request if the TIM bit of the TCR is clear. The TIR is cleared by the MPU reset or by program control.
- Bit 6, Timer Interrupt Mask (TIM), inhibits a timer interrupt request when it is set. It is set by external reset or program control to inhibit the Blinking Mode, and is cleared by software when the Blinking Mode is requested by the operator.
- Bit 5, External or Internal Clock Select (TIN), is used to select the timer clock source. Since the internal clock is used in this application, the TIN bits of both

Table 3. MPU CONNECTIONS

Pin	Name	Description
1	V_{SS}	Ground
2	\overline{RESET}	When \overline{RESET} is pulled low program execution halts, all variables are reinitialized and the Pan display is set to zero. SW1(P) controls the RESET line on the Pan MPU.
3	\overline{INT}	Allows asynchronous interruption of the processor. When \overline{INT} is pulled low by the Count Edge Detector the MPU executes the "Count Routine".
4	V_{CC}	+ 5 V dc power connection.
5	EXTAL	External clock input. Connected to a 4.0 MHz external clock which provides the MPU system clock.
6	XTAL	Crystal clock input. Connected to ground since an external clock is used.
7	V_{PP}	Programming voltage pin. Connected to V_{CC} for normal operation.
8	Timer	External timer control input. Connected to V_{CC} since the internal timer is used.
	Port C	General Purpose I/O lines.
9	PC0	The two least significant digits in the display are represented in binary coded decimal (BCD) by these eight lines.
10	PC1	
11	PC2	
12	PC3	
13	PC4	
14	PC5	
15	PC6	
16	PC7	
	Port D	General Purpose input lines.
17	PD7	PD7 is the Channel A input to the MPU.
18	$\overline{PD6}/\overline{INT2}$	PD6 is used as a second interrupt line. When PD6 goes low the MPU changes display modes.
19	PD5	PD5 is the Channel B input into the MPU.
20	PD4	PD4 is the Function input into the MPU.
21	PD3	PD3 is the Set input into the MPU.
22	PD2	PD2-PD0 are not used and are tied to ground.
23	PD1	
24	PD0	

Table 4. MPU CONNECTIONS (CONTD.)

Pin	Name	Description
	Port B	General Purpose I/O lines (LED compatible).
25	PB0	The most significant digit is represented in BCD by PB0-PB3 except on the Tilt MPU where these lines are connected to ground. PB4 determines which digits in the display are blanked. PB5 is not used. Connected to ground. PB6 determines the presence or absence of the display minus sign. PB7 determines the presence or absence of the display decimal point.
26	PB1	
27	PB2	
28	PB3	
29	PB4	
30	PB5	
31	PB6	
32	PB7	
	Port A	General Purpose I.O lines.
33	PA0	The third and fourth least significant digits are represented in BCD by these eight lines.
34	PA1	
35	PA2	
36	PA3	
37	PA4	
38	PA5	
39	PA6	
40	PA7	

MPU's are always cleared. For the same reason the Timer pins are connected to V_{cc} (see Table 3).

- Bit 4, External Enable (TEE), is not used by the measurement system. By keeping the TEE clear at all times, the 68705's internal timer is used exclusively.
- Bit 3, Prescaler Clear (PSC), is not used in this application; always cleared.
- Bits 2-0, Prescaler Select (PS2, PS1 and PS0), are always set during program execution. This causes the internal timer signal frequency to be divided by 128.

(3) *Mask Option Register (MOR)*. Unlike the TDR and TCR the MOR is not software programmable; instead, it is implemented in EPROM.

- Bit 7, the Clock bit, is cleared to allow operation of the external 4.0 MHz clock.
- The Timer Option bit (TOPT), bit 6, is also cleared in this application. This permits the TCR to be software programmable.
- Bit 5 is cleared to permit the use of the internal clock with the timer.
- Bits 4 and 3 are not used.

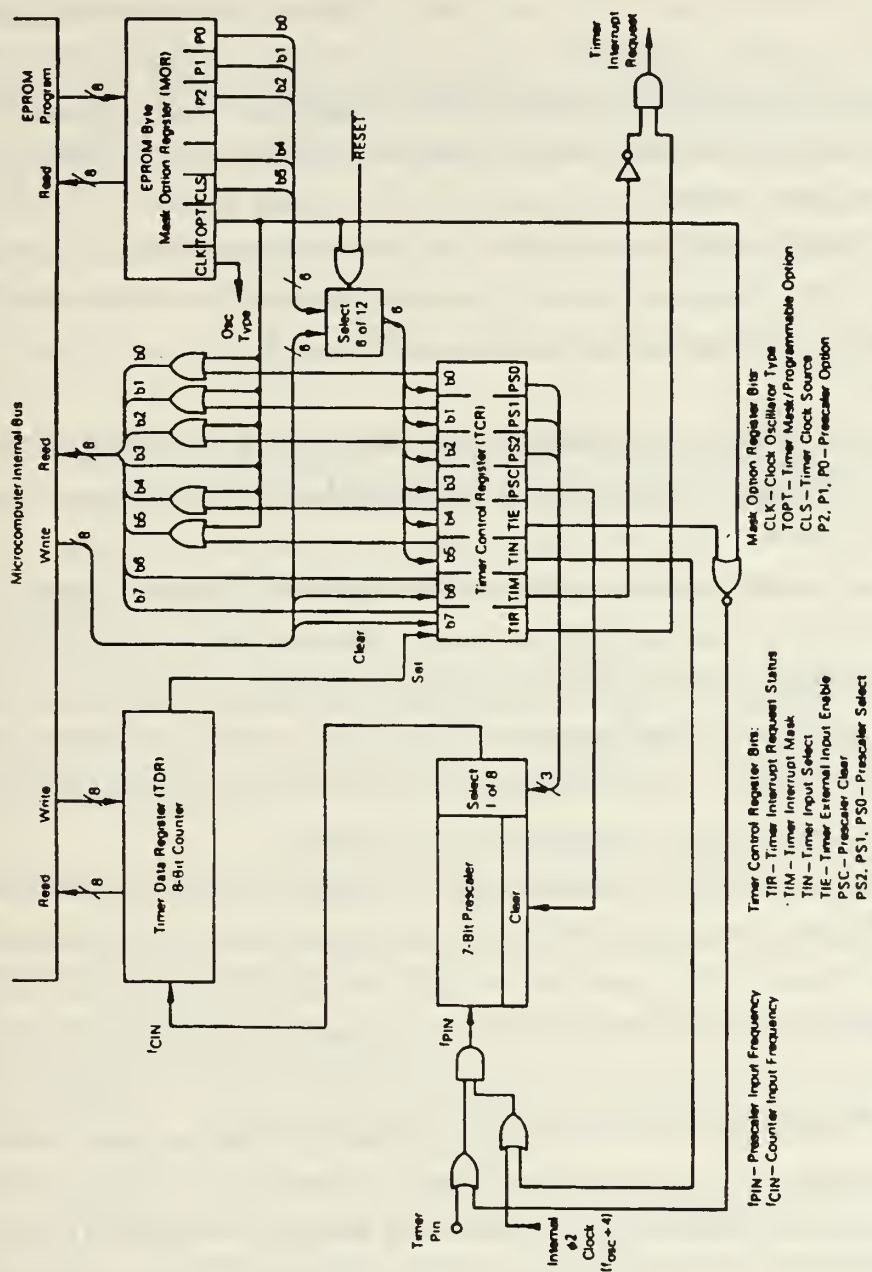


Figure 20. MC68705U3 Timer Functional Block Diagram.: From Ref. 10: p. 8.

- Bits 2-0 are all set and serve the same function as PS2, PS1 and PS0 bits of the TCR. [Ref. 10: pp. 6-8, 13-15]

3. RAM

The MC68705U3 has 112 bytes of RAM. The 112 bytes includes 31 bytes that can be used for the stack. Use of the stack is quite limited. During interrupts it is used to save the contents of the CPU registers and the program counter. During subroutine calls only the program counter is saved. The user's program has no other access to the stack. The programs written for each of the MPU's require less than 25% of the available RAM. The Pan MPU uses 27 of the 112 available bytes and the Tilt MPU uses only 22 bytes. The programs listed in Appendix D explain the function and give the location in memory for each of the variables. [Ref 10: p. 5]

4. ROM

The 3776 bytes of user EPROM in the MC68705U3 are divided into three separate blocks in the memory. Page Zero User EPROM is the ROM located between address S080 and S0FF. Because these addresses are only one byte long, instructions located in Page Zero ROM can be referenced with addressing modes not permitted with instructions located in other parts of the memory. Between address S100 and SF37 is the User Main EPROM. This portion of the memory in each MPU contains the vast majority of the signal conditioning programs. Located in another portion of the EPROM are the Interrupt Vectors. In each of these locations is the address of the first instruction the MPU is to execute when a particular interrupt occurs.

As with the RAM only a fraction of the available EPROM has been used in this application. The Pan MPU uses 899 bytes of the 3776 available and the Tilt MPU uses only 767 bytes. Since both programs are so small, one could reasonably ask why the two programs were not both put in one MPU. The primary problem with this idea is that each microprocessor can perform only one operation at a time. As indicated at the end of Chapter II, if the camera servo is rotating about its vertical axis at its maximum velocity of 1 rpm, the Pan signal conditioner must be capable of counting and displaying 51,200 counts per minute. Using a 4.0 MHz clock this allows the MPU 1172 μ s to count each pulse. Similarly the Tilt MPU has 1758 μ s to count each pulse when the camera is rotating at its maximum velocity about the horizontal axis. Assuming that the camera is rotating at its maximum velocity on both axes at the same time, and one MPU is being used to count the pulses from both encoders, the MPU needs to count 76,800 pulses per minute, which only allows 781.3 μ s per pulse. The Pan MPU currently requires a max-

imum of 1032 instruction cycles or $1032\mu\text{s}$ to count a single pulse, and the maximum execution time for a single pulse on the Tilt axis is $825\mu\text{s}$. Thus, a single 68705 lacks the computational speed required to ensure that no counts would be missed if it was used to process the data from both encoders.

5. Central Processing Unit (CPU)

The CPU of the M6805 Family is implemented independently from the I/O or memory configuration. Consequently it can be treated as an independent central processor communicating with I/O and memory via internal address, data and control buses. [Ref 10: p. 6]

The CPU has five registers that are available for use by the operator. The function of each of these is described below.

- The Accumulator (A) is a general purpose data register used for arithmetic calculation and data manipulation.
- The Index Register (X) can be used as a second accumulator but is generally used for the indexed addressing mode. In the indexed addressing mode an effective address is created by adding the contents of X to a number provided by the instruction.
- The Program Counter (PC) contains the memory address of the next instruction to be executed by the MPU.
- The five bits of the Condition Code Register (CCR) keep information concerning the results of the last instruction executed by the MPU. Reference 14 gives a detailed description of each of the instructions in the M6805 Family Instruction Set and explains the effect of each instruction on the CCR. A brief description of each bit in the CCR follows.
 - The Carry (C) bit is set if a carry or a borrow was generated by the last arithmetic instruction. The state of the C bit can be software controlled.
 - The Zero (Z) bit is set if the result of the last arithmetic, logic or data manipulation instruction was zero.
 - The Negative (N) bit is set if bit seven of the result of the last arithmetic, logic, or data manipulation instruction is set.
 - The Half Carry (H) bit is set if an ADD or an ADC instruction causes a carry to occur between bits 3 and 4 of the result.
 - The Interrupt Mask (I) bit is set when an external interrupt ($\overline{\text{INT}}$) occurs. If another interrupt occurs (e.g. Timer Interrupt or $\overline{\text{INT2}}$) when the I bit is set, the second interrupt is latched so that it can be processed as soon as the I bit is cleared. The I bit can be set or cleared by software.
- The contents of the Stack Pointer (SP) are the address of the next available location on the stack. As previously discussed, the stack is only used to keep track of the PC during subroutine branches, and all of the CPU registers during an interrupt. [Refs. 10: p. 6, 14 : pp. 14-15]

6. Input

Each MPU uses six input lines. Two of these lines, $\overline{\text{INT}}$ and $\overline{\text{INT2}}$, are interrupt lines that detect a negative-going edge on their respective lines. The other four lines are general purpose input lines on Port D. All of the pins on Port D are TTL compatible which made the hardware design relatively straightforward. The electrical characteristics for the input pins are listed on p. 2 of Ref. 10.

The general operation of the two interrupt lines is described in Table 3 on page 39. Once they are understood, interrupts are a simple yet powerful tool. Only three of the four interrupts available on the MC68705U3 are used by the Pan and Tilt programs. The software interrupt is not used. When the MPU is interrupted, current program execution is halted, the contents of the CPU registers are placed on the stack, and the MPU fetches the contents of the appropriate interrupt vector from memory. After the interrupt vector has been fetched, the PC is moved to that address and execution of the interrupt routine begins. There is no ambiguity when an external interrupt occurs since there is a dedicated interrupt vector in memory. The timer interrupt and $\overline{\text{INT}}$ however share the Timer Interrupt Vector. When one of these interrupts occurs, the interrupt routine must determine the source of the interrupt by checking the TIR bit of the TCR and bit 7 of the MR to determine the source of the interrupt [Ref. 10: p. 11]. Normal program execution resumes at the point at which the interrupt occurred when the interrupt routine executes a return from interrupt (RTI) instruction.

The Function and Set lines on pins 20 and 21 are connected to the Function and Set switches. The operation of these switches is described in Table 2 on page 36. The remaining two input lines to each MPU are Channels A and B from the respective shaft encoders. The MPU programs use the information from these two inputs to determine the direction of rotation and to identify repeated oscillations about a single transition.

7. Output

Each MPU is designed to provide position information at its output in two basic forms. On the Pan axis, in the Count Mode a number between -51,200 and +51,200 constitutes the output while in the Position Mode the output is an angle between 0° and 360°. A five digit display with a minus sign is sufficient for the count display. Using a five digit display with a decimal point in the Position Mode permits the angle to be displayed to the nearest hundredth of a degree. This resolution is not quite as good as the resolution of the shaft encoders ($\pm 0.007^\circ$); however, final testing of the measurement system revealed that resolution is actually limited to about $\pm 0.02^\circ$ on the Pan axis and

about $\pm 0.14^\circ$ on the Tilt axis. The five digit display is therefore completely adequate for this system.

The Pan MPU uses 23 of its 24 output pins to represent the five digits, a minus sign and a decimal point. Each of the five digits is available in BCD form on four output pins of the MPU. The five digits are referred to as Digit 1, Digit 2, etc., with Digit 1 being the least significant digit and Digit 5 being the most significant digit. Port A has as its output the BCD representation of Digit 3 and Digit 4. Digit 1 and Digit 2 are represented by the output of Port C. The low four bits of Port B contain the BCD representation of Digit 5. These 20 output lines are the input to five 74LS47, BCD/7-Segment Decoder/Drivers, which decode the BCD signals and drive the common anode LED indicators. The output from Pin 29, PB4, is one input to a 74LS32 OR gate, the output of which is used to blank leading zeros out of the display. Pin 30 is not used and is tied to ground. The remaining two output pins drive two LED segments in the display. The signal on pin 31 turns the minus sign off and on, and the signal on pin 32 determines whether the decimal point is displayed.

The electrical characteristics of the I/O Ports are given on p. 4 of Ref. 10. The output characteristics of Ports A, B and C are compatible with the input characteristics of the 74LS47 and the 74LS32 given on pp. 4-59 and 4-48 of Ref. 11. The pins on Port B are capable of sinking 10 mA when Port B is configured as an output port. A 220 Ω resistor placed in series with each of the display segments limits the current to approximately 9 mA and permits the MPU to drive the decimal point and minus sign directly.

One consideration in the design of this system was to provide a system capable of being readily expanded to meet changing needs. To this end, in addition to being connected to the LED display devices via the 74LS47's, the BCD data lines are also connected to a header on each of the MPU circuit boards. If, at a later date, the position information needs to be used in another system, a jumper connected to each of the headers could provide the information with little or no modification.

The Pan and Tilt signal processing subsystems are virtually identical in the hardware used to implement them. The only difference is that the Pan system has a five digit display, and the Tilt system needs only four digits to display its position information. Consequently, the Tilt system does not use Digit 5, and pins 25-29 are tied to ground.

F. DISPLAY

Each digit represented in BCD at the output of the MPU is decoded by a 74LS47 BCD/7-Segment Decoder/Driver. The decoding devices each convert a four bit BCD representation of a number into seven signals that each drive a separate segment of a common anode, seven segment, LED display. The 74LS47 is capable of sinking 24 mA from each of the LED segments. Without a current limiting resistor between each of the output pins on the 7447 and the corresponding pin on the display element however, this maximum current is exceeded. When this happens the LED's have a very short life, the 7447 overheats and the system fails to function properly. The addition of a 220 Ω resistor in each branch limits the current to about 9 mA per segment, and permits trouble-free operation.

Three of the output pins on each MPU are not used as inputs to the 7447's. As discussed in the previous section, the Decimal and Minus lines each drive individual LED segments directly. The third line, also mentioned briefly in the preceding section, is used with the Blanking In/Ribbon Blanking Out (BI/RBO) signal from Digit 4's 7447 to determine the Ribbon Blanking In (RBI) signal into the 7447 which drives the display for Digit 3.

The term "blanking" simply means removing the leading zeros from the display. The two display modes available from the MPU's have different blanking requirements. In the Position Mode the three least significant digits are not blanked, while in the Count Mode, all but the least significant digit are blanked. The RBI and BI/RBO pins on the 7447's, the Blank line out of each MPU and the OR gates, connected as shown in the schematics in Appendix A, provide this capability.

The Light Test (LT) pin on each 7447 is connected to SW5. When the switch is closed, the Light Test line goes low and each of the output lines on each of the 7447's also goes low, thus sinking current from all of the LED segments simultaneously. This feature allows the operator to check for inoperable display segments.

G. POWER SUPPLIES

The two power supplies shown in Figure 2 on page 6 are each +5.0 Vdc supplies. The power supply which provides power to the shaft encoders and the line drivers is physically mounted in the camera housing. It was built by modifying the +12 Vdc auto iris power supply. This was accomplished using an LM7805 Voltage Regulator in the manner shown in Figure 8 of Appendix A. The auto iris requires only 100 mA at +12 Vdc for correct operation, and the LM7812 Voltage Regulator has an available

output current of 1.0 A [Refs. 15, 16]. The remaining 900 mA is available to the LM7805 to power the encoders and the line drivers. Reference 9 lists the maximum power requirement for the IIEDS-600 as 40 mA at +5 Vdc, and Ref. 11 specifies the maximum power requirement for a 74S140 is 1 mA at +5 Vdc. Thus, the 84 mA requirement for the two encoders and four line drivers is well within the capabilities of the modified power supply.

The second power supply is capable of providing 6.0 A at +5 Vdc which is more than adequate to provide the 1.4 A needed by the signal processors and the display devices. The power supply also has 12 Vdc and -5 Vdc ports. To preclude the potentially disastrous results which might occur if the power supply were incorrectly connected to the signal processor/display devices, the circuitry shown in Figure 21 was included on each MPU and display printed circuit board.

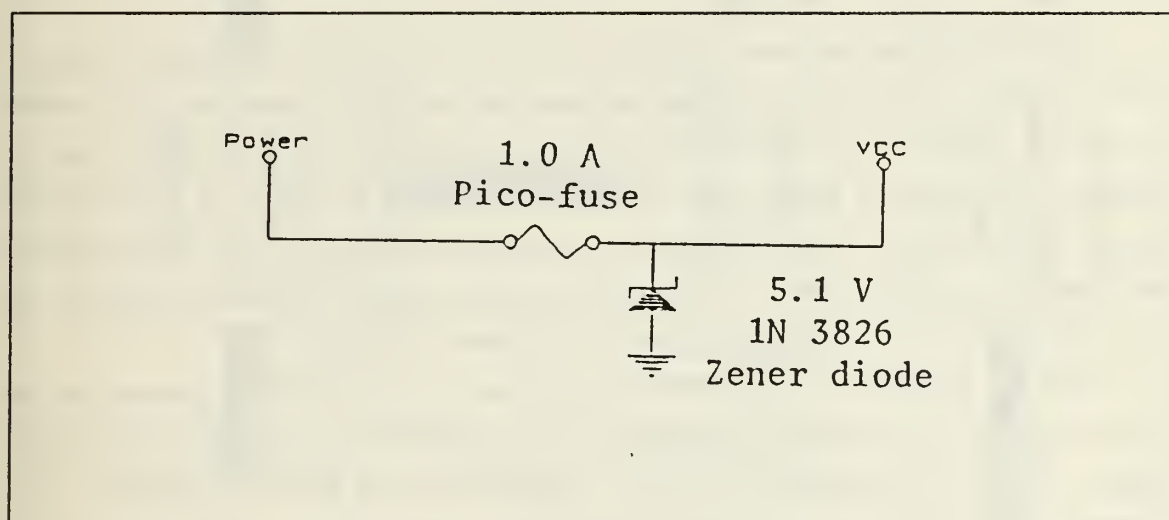


Figure 21. Reverse/Over-voltage Protection Circuit

IV. CALIBRATION , TESTING AND IMPLEMENTATION

A. GENERAL

Once the basic system design had been completed, and the MPU programs had been written, a prototype system was constructed. The prototype system might also be called the development model, since it was not only used to test the design , but was also used to calibrate the MPU programs. A block diagram of the prototype system is shown in Figure 22. The M68705EVM Evaluation Module (subsequently referred to as the EVM) provided the capability to debug and evaluate the MC68705U3-based signal processing subsystem. Operation of the signal processing MPU was performed by an MC68705U3 resident on the EVM.

The prototype system provided considerable flexibility in the testing and calibration of the system. The assembly language programs for the MPU's were written and edited on the PC. They were then assembled and linked using the 2500 A.D. 6805 Cross Assembler and 2500 A.D. Linker [Ref. 17: pp. (1-1)-(2-38)]. The result, a Motorola S19 output file (see [Ref. 17: pp. (A-1)-(A-4)]), was then down-loaded to the EVM using the file transfer program, Kermit. Downloading procedures are detailed in [Ref. 18: pp. (3-10)-(3-25),(3-37)]. The PC-EVM interface is shown in Figure 23.

After the program had been down-loaded into the MC68705U3 resident on the EVM, data entry and program debugging were controlled via the CRT monitor keyboard. The CRT-EVM interconnection is shown in Figure 24 and the monitor commands are described in [Ref. 18: pp. (3-8)-(3-25)].

The remainder of the signal processing functions were realized using hardware external to the EVM. These functions included edge detection of the output signals from the shaft encoders, decoding the output of the MPU, and generating the signals to drive the display devices. This portion of the prototype, referred to by [Ref. 18] as the "target system", was built on breadboards and is represented by the block in the center of Figure 22. The target system was connected to the MCU via a 40-pin jumper header, J1, on the EVM. The pinout for J1 is shown in Figure 25. The labels in Figure 25 refer to the labels used in the schematic diagrams which are shown in Appendix A.

B. CALIBRATION

Once the MPU programs were capable of counting the pulses generated by the shaft encoders, the programs needed to be "calibrated". This calibration procedure required

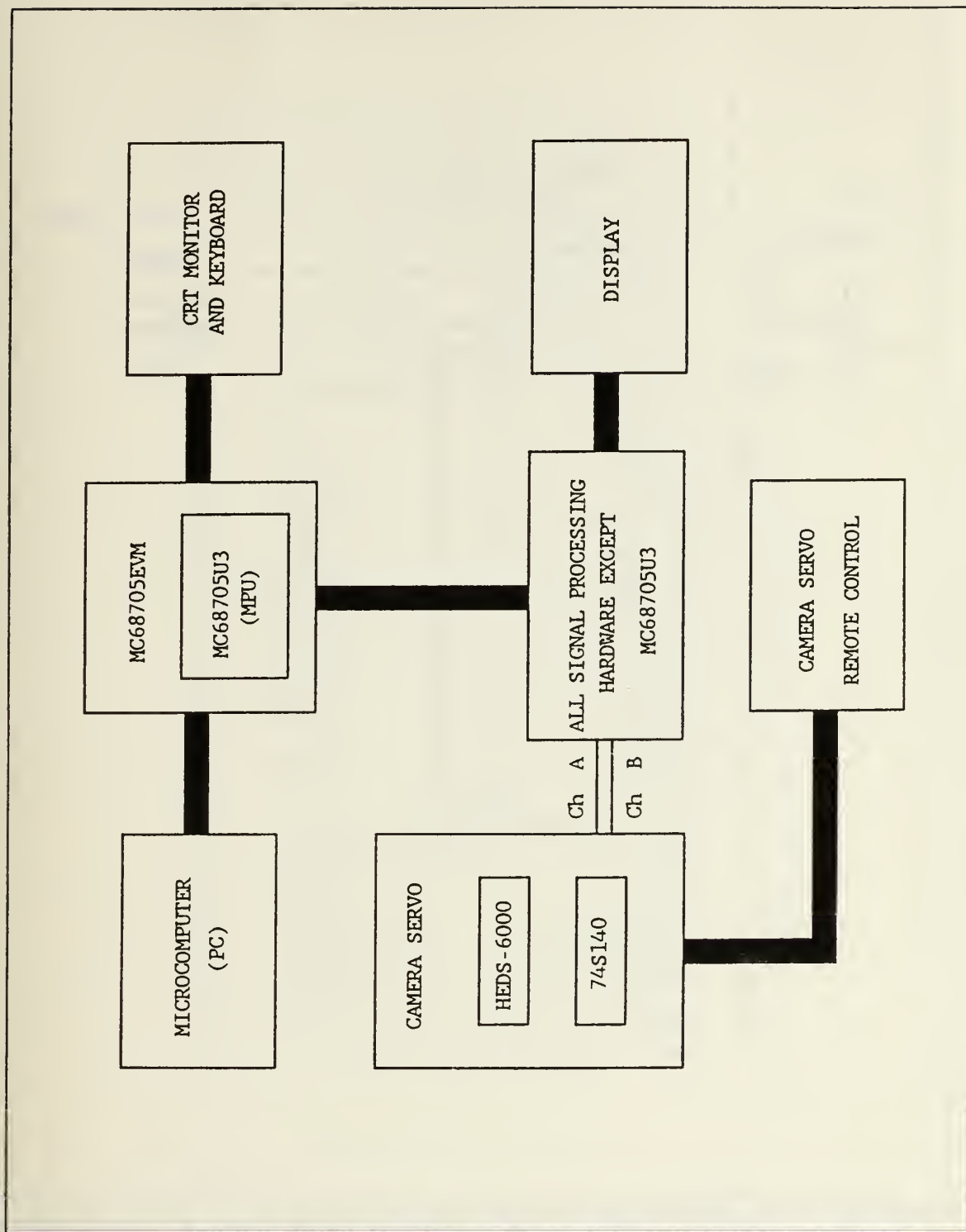


Figure 22. Prototype/Development Model

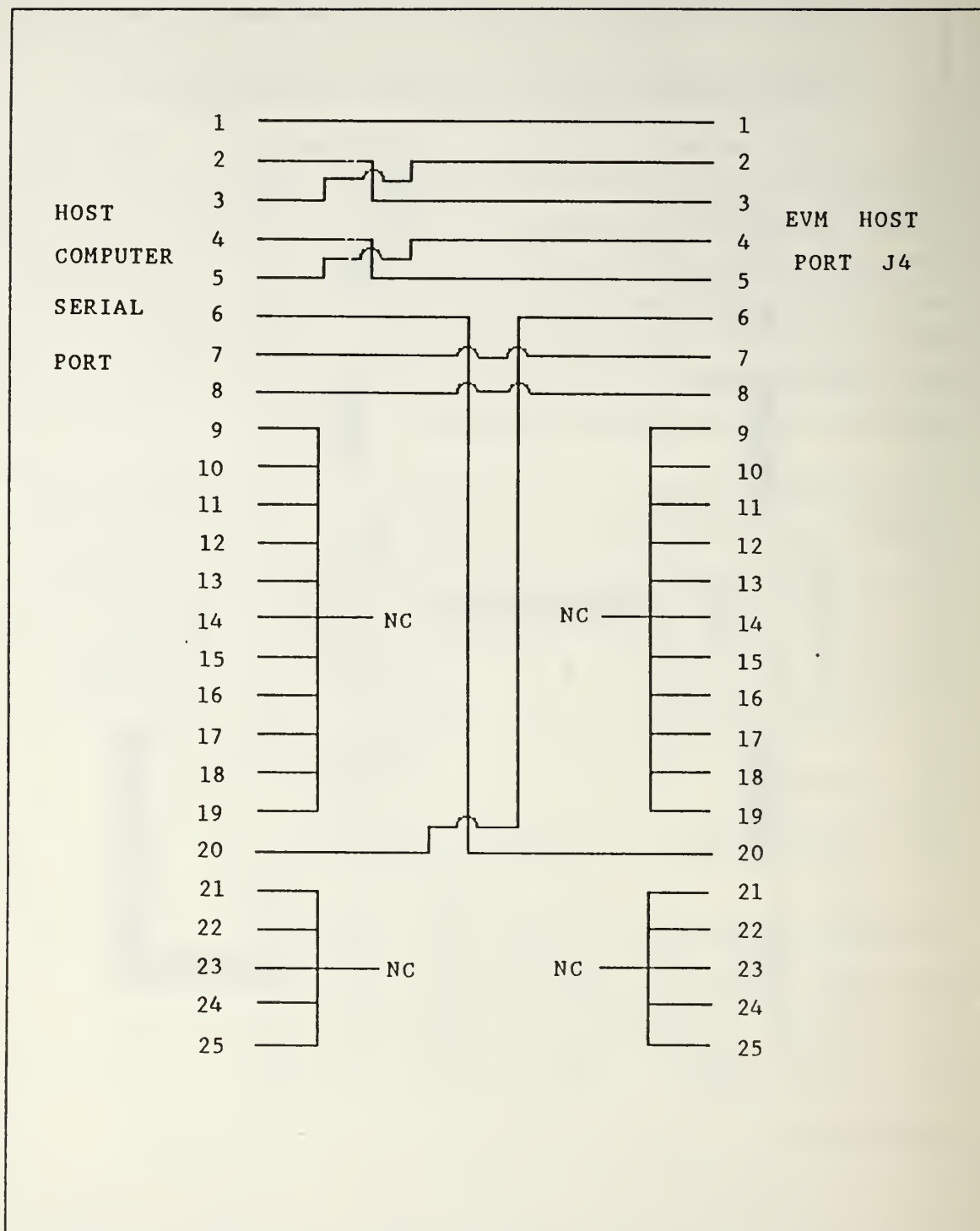


Figure 23. Host Computer - Evaluation Module Connections

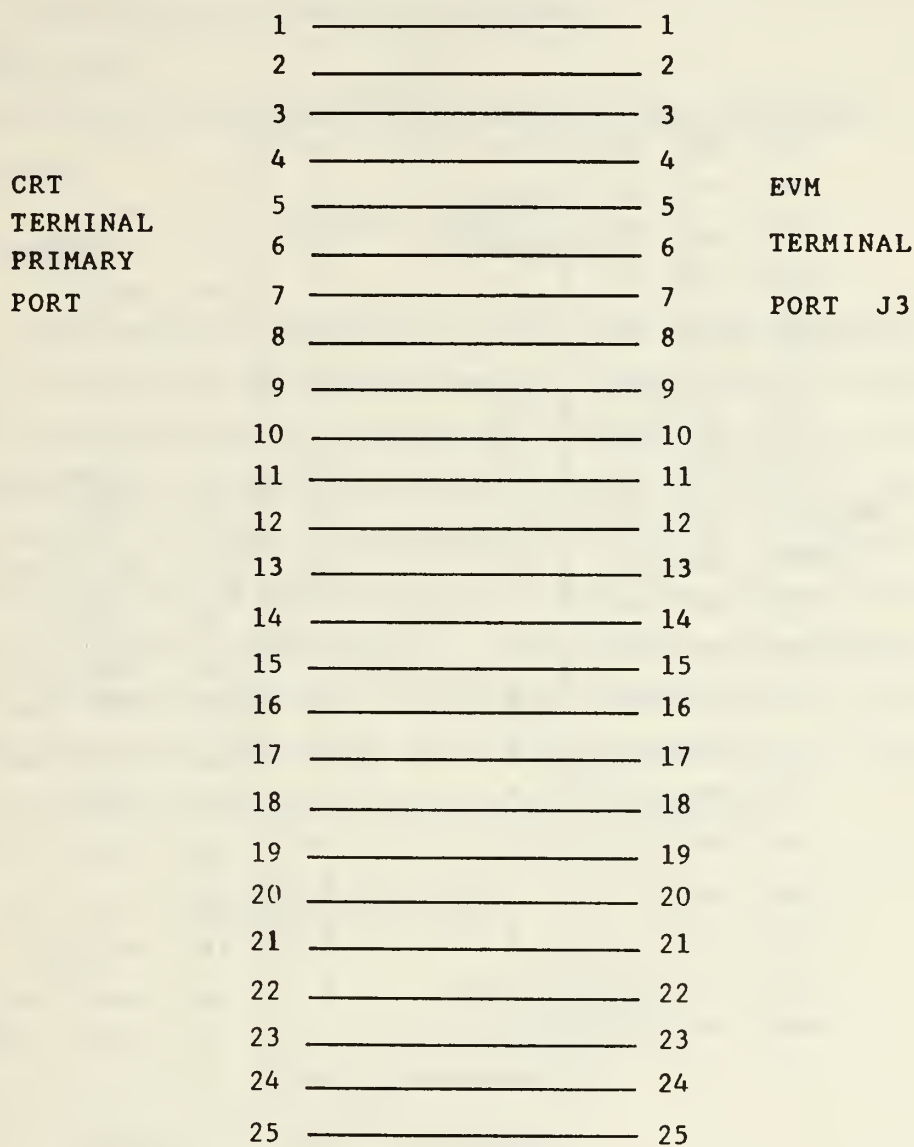


Figure 24. Monitor - Evaluation Module Connections

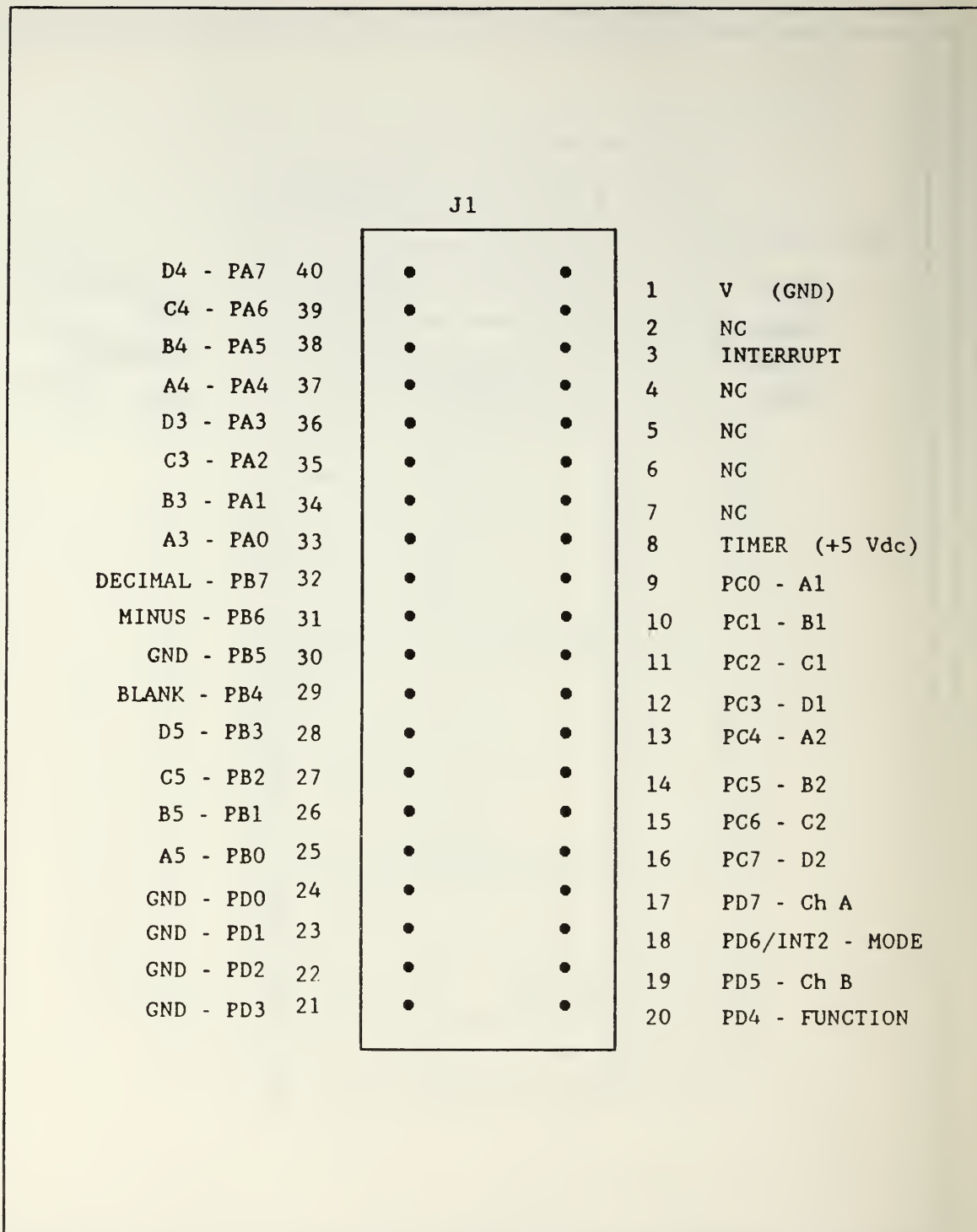


Figure 25. Evaluation Module - Signal Processor Connections

determining the angular distance through which the camera rotated between successive pulses from the shaft encoder. This number is a scale factor, which, when multiplied by the total number of pulses from the shaft encoder, yields a number equal to the angular displacement of the camera. The calibration procedure also involved determining the amount of hysteresis present in each of the gear trains.

1. Scale Factor

To determine the scale factor (SF) the simple geometric relationship

$$\theta = \tan^{-1}\left(\frac{\text{opposite}}{\text{adjacent}}\right) \quad (12)$$

was used. Using a small laser attached to the camera servo, and the geometry shown in Figure 26, the SF could be experimentally determined. As the camera servo was rotated through an angle, θ , the MPU was used to count the output pulses from the shaft encoder. The laser beam was projected on a vertical surface at a distance, a , away from the axis of rotation. The beam of the laser spread to a diameter of approximately 0.4 in. over a distance of 30 ft. A template with a 0.4 in. diameter aperture was used to mark the location of the "spots" on the distant wall. The distance between the spots, l , was measured by selecting one edge of one of the marks and measuring the distance to the corresponding edge of the distant mark. Then, having determined l and a and reading the count, C , from the display, the SF could then be determined from

$$\begin{aligned} \text{SF}(\text{degrees/Pulse}) &= \frac{\theta}{C} \\ &= \frac{\tan^{-1}\left(\frac{l(\text{in})}{a(\text{in})}\right)}{C} \end{aligned} \quad (13)$$

Using Equation (13) to simplify the expression,

$$d(\text{SF}) = \frac{\delta(\text{SF})}{\delta l} dl + \frac{\delta(\text{SF})}{\delta a} da \quad (14)$$

yields

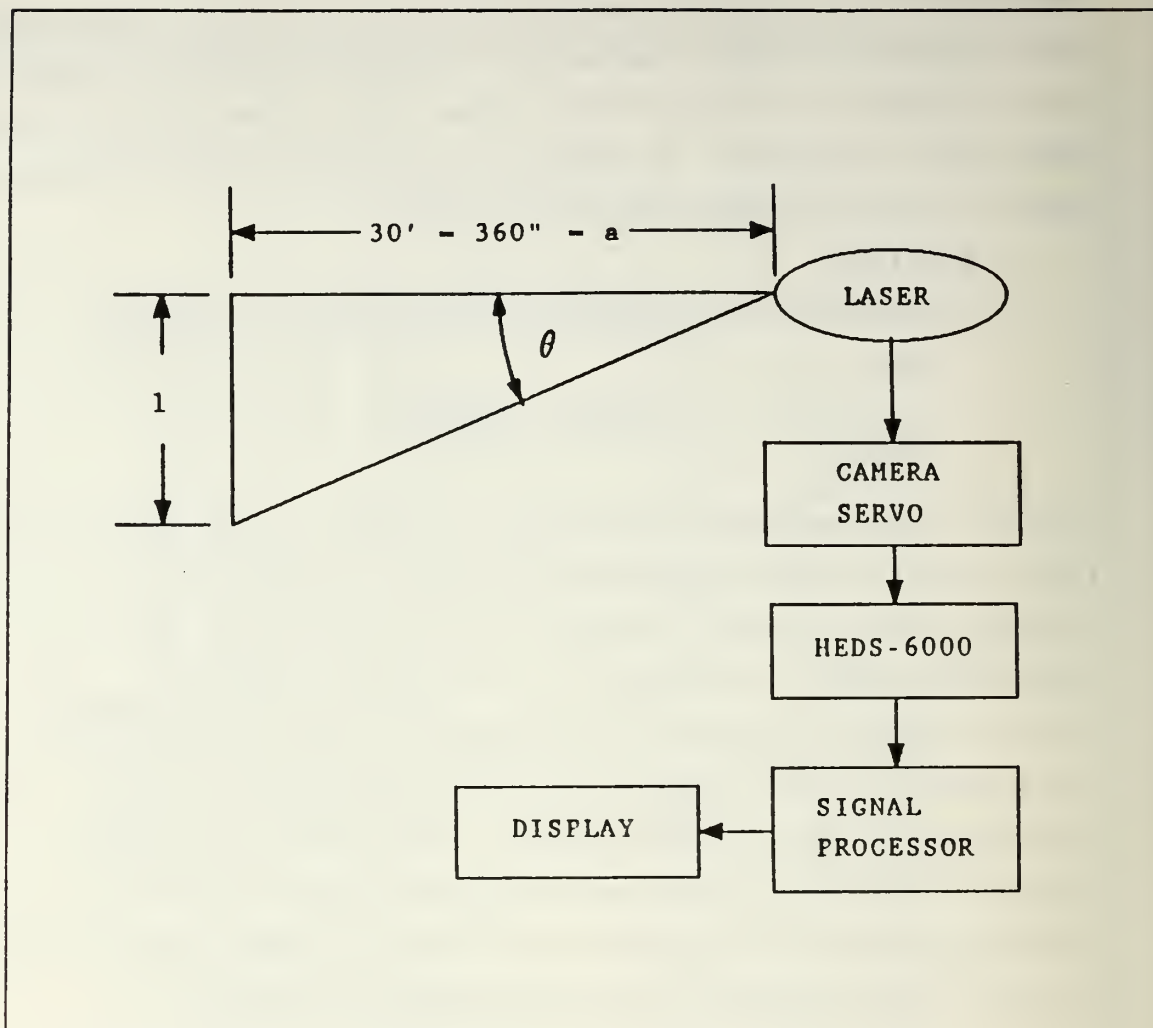


Figure 26. Geometry Used to Determine the Scale Factor

$$\begin{aligned}
 d(SF) &= \frac{1}{C} \frac{\delta \theta}{\delta l} + \frac{1}{C} \frac{\delta \theta}{\delta a} da \\
 &= \frac{1}{C} \left(\frac{a}{a^2 + l^2} \right) dl + \frac{1}{C} \left(-\frac{l}{a^2 + l^2} \right) da \\
 d(SF) &= \frac{(a dl - l da)}{C(a^2 + l^2)},
 \end{aligned} \tag{15}$$

which indicates that C , a and l should all be as large as possible to minimize the error in SF due to a measurement error in a or l . The physical size of the laboratory limited the distance, a , to 30 ft. When $a = 30$ ft, l was limited to about 3.5 ft in the horizontal

plane and about 4.0 ft in the vertical plane. By modifying the geometry as shown in Figure 27, the count, which from Equation (13) is directly proportional to θ , could also be maximized. The configuration shown in Figure 27 was used to obtain the scale factor calibration data for the Pan axis. However, since the servo is incapable of rotating 360° about the Tilt axis, the test configuration shown in Figure 26 had to be used to collect the data for that axis.

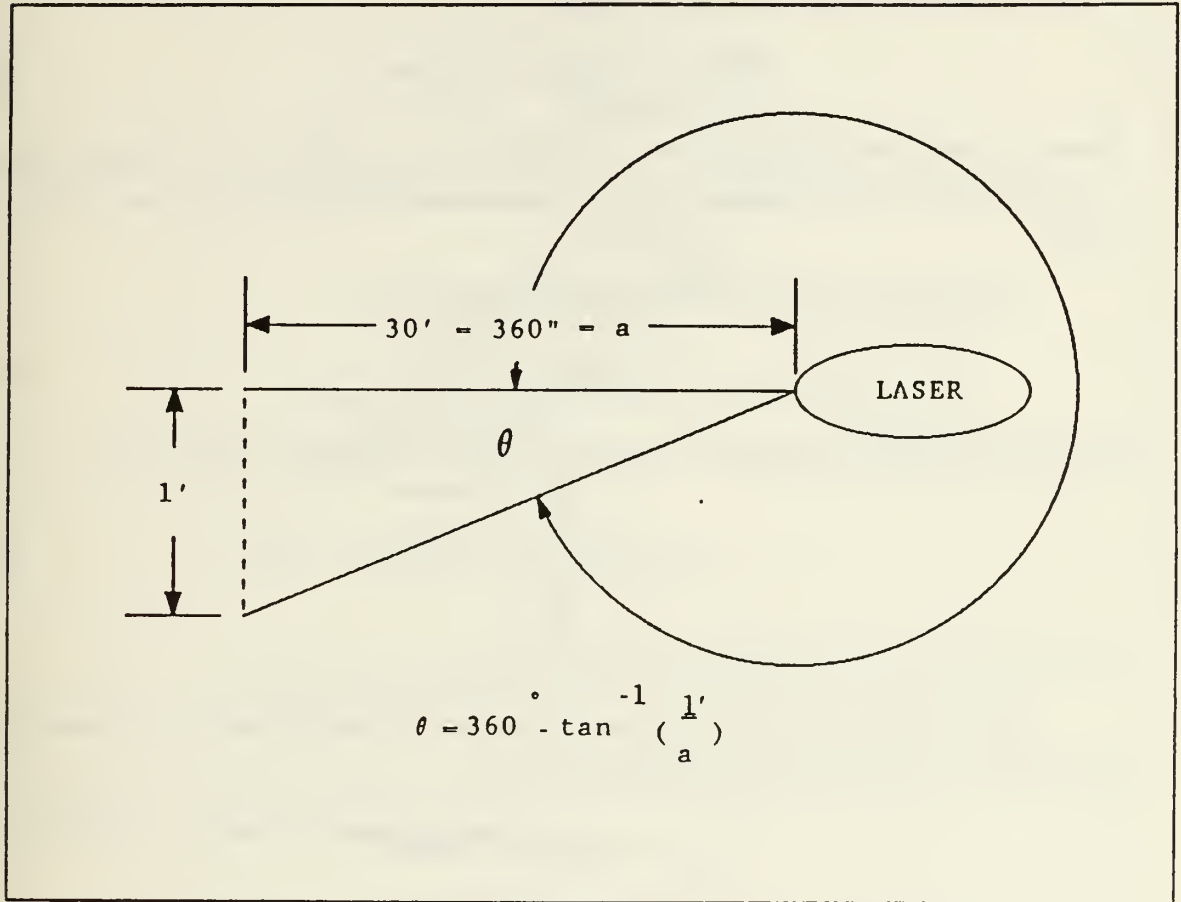


Figure 27. Alternate Geometry Used to Determine the Scale Factor

Adopting the notation, \bar{X} , to represent the mean value of a random variable, X ; if X is discrete with N measured values,

$$\bar{X} \approx \frac{1}{N} \sum_{i=1}^N X_i \quad (16)$$

where X_i is the i th measured value of X , and the approximation becomes better as N approaches infinity.

Using the expression in Equation (16) and the measured data for the scale factors, from 31 measurements on the Pan axis,

$$\overline{SF}_{\text{Pan}} = (7.0312 \times 10^{-3})^\circ \text{Pulse}^{-1} , \quad (17)$$

and after 32 measurements on the Tilt axis,

$$\overline{SF}_{\text{Tilt}} = (7.0452 \times 10^{-3})^\circ \text{Pulse}^{-1} , \quad (18)$$

where the subscripts indicate the axis. The actual implementation of these scale factors is described later in this chapter and in the documentation for each of the MPU programs.

If the error in the i th measurement is described by

$$e_i = X_i - \bar{X} , \quad (19)$$

then the root mean square (RMS) error in N measurements of X is given by;

$$\sigma_x = \sqrt{\frac{1}{N} \sum_{i=1}^N (X_i - \bar{X})^2} . \quad (20)$$

Note that this is also the definition of the standard deviation of X .

The RMS errors in the Pan and Tilt scale factor measurements were determined from Equation (20) and the measured data to be;

$$\sigma_{SF_{\text{Pan}}} = (4.62 \times 10^{-6})^\circ \text{Pulse}^{-1} \quad (21)$$

$$\sigma_{SF_{\text{Tilt}}} = (6.89 \times 10^{-6})^\circ \text{Pulse}^{-1} . \quad (22)$$

As before, the subscripts are used to identify the axis and the source of the error. The fact that the errors are small compared to the mean values suggests that the means should closely approximate the actual values for the scale factors.

2. Hysteresis

Houghton defines backlash in wormgearing as "...the total play between the surfaces of the worm and worm wheel teeth measured normal to the faces." [Ref. 19: pp. 1.4, 1.5] Backlash only poses a problem in the measurement system when the servo's

direction of rotation changes. Figure 28 is a typical hysteresis curve. As long as the direction of rotation of the worm is increasing the $\theta_{\text{WORM}}/\theta_{\text{WORMGEAR}}$ relationship is linear. However, when the direction of rotation reverses there is a region, depicted by the left pointing arrows, where the position of the worm changes without a corresponding change in the position of the wormgear. Note that once all of the backlash has been taken up the $\theta_{\text{WORM}}/\theta_{\text{WORMGEAR}}$ relationship is again linear until the direction of rotation changes.

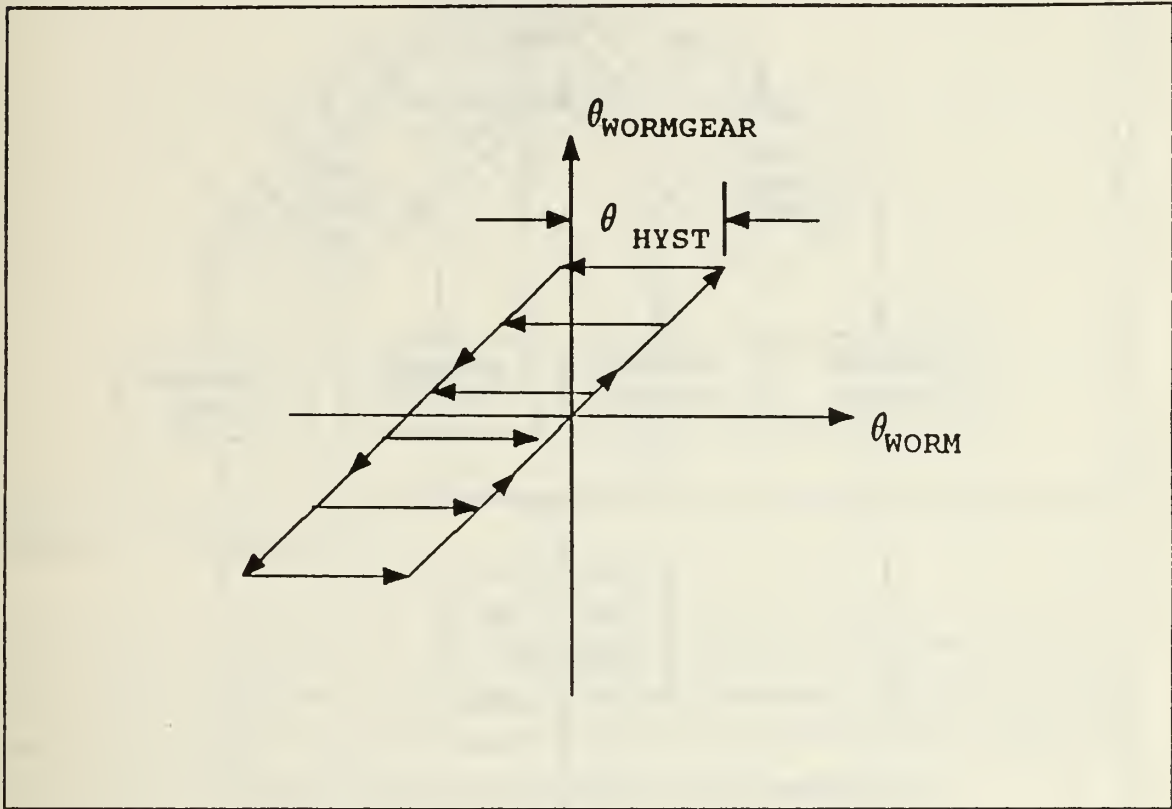


Figure 28. Typical Hysteresis Curve

The purpose of the hysteresis buffer in the MPU is to permit the signal processor to account for the backlash error introduced into the measurement by the worm-wormgear connection. The theory of operation for the buffer is relatively straight forward and is best described by the flow diagram in Figure 29. The buffer is a data byte in the MPU RAM. As long as the buffer is full, i.e., the contents are equal to the predetermined buffer length, a clockwise (CW) signal from the shaft encoder (increasing elevation and increasing azimuth are defined as CW rotation for the purposes of this system) causes the position counter to be incremented. Similarly, counter-clockwise

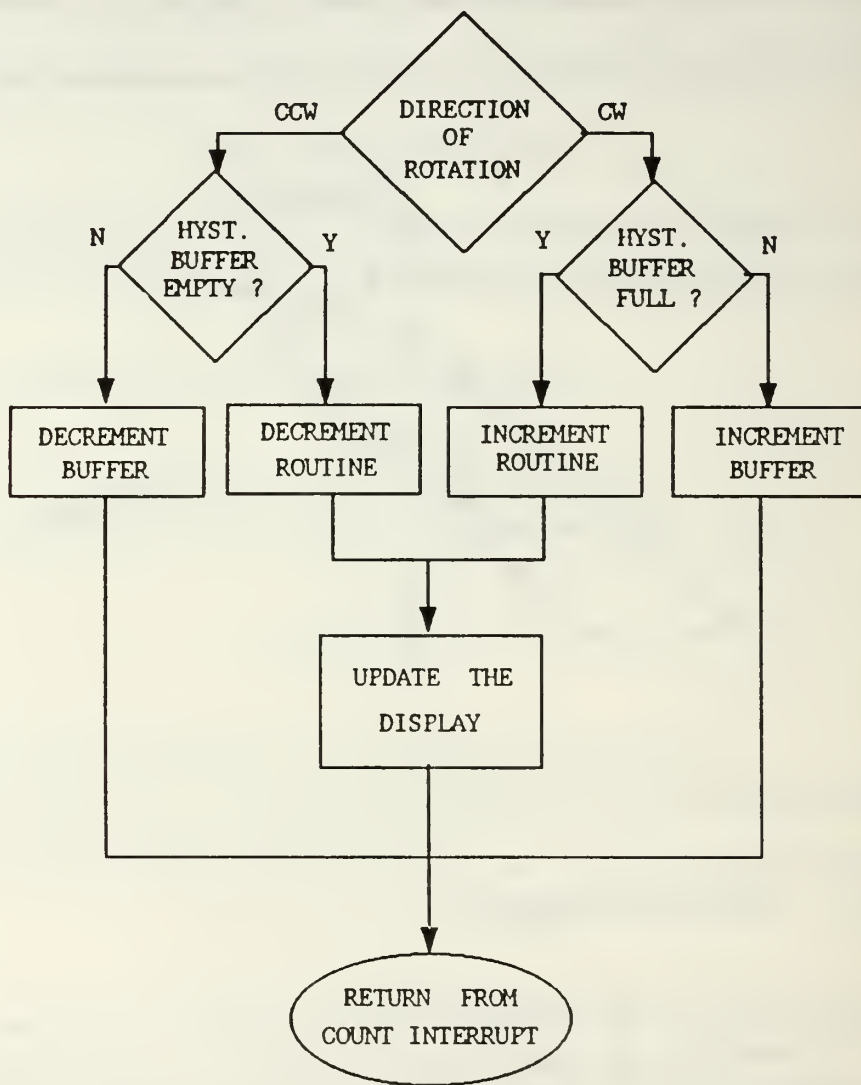


Figure 29. Operation of the Hysteresis Buffer

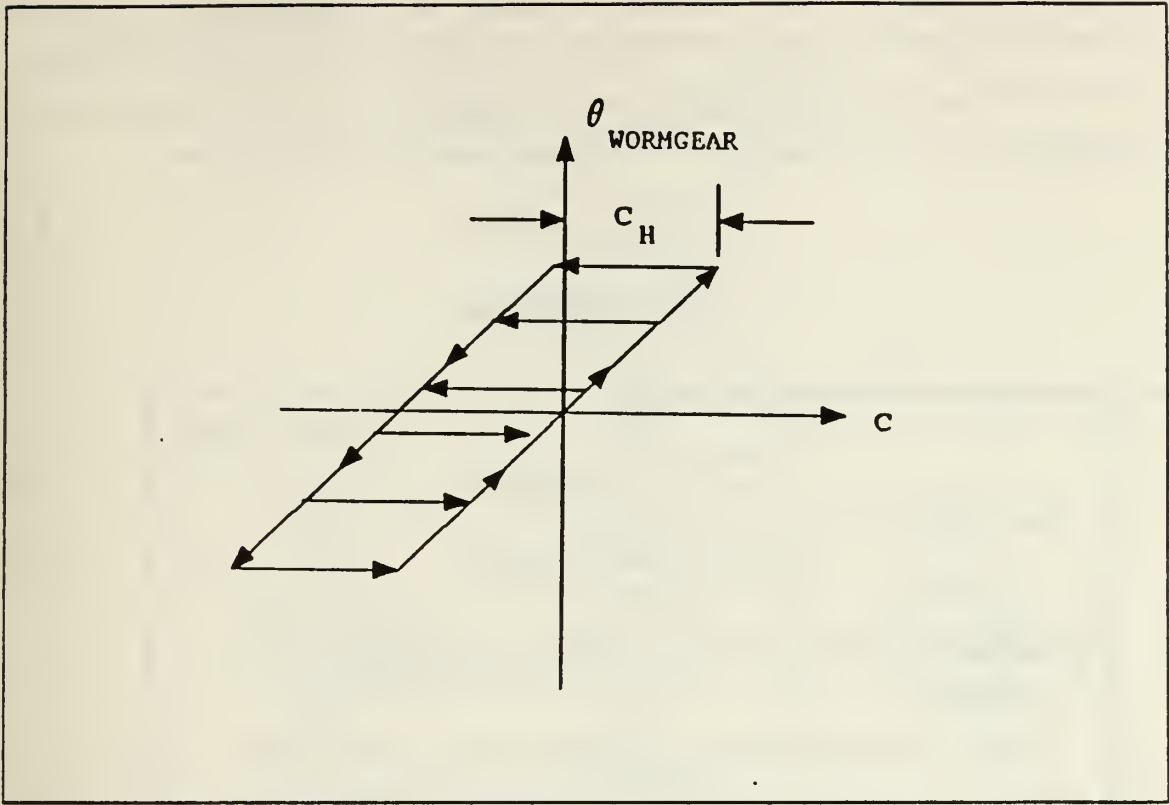


Figure 30. Hysteresis Curve

(CCW) signals cause the position counter to be decremented if the hysteresis buffer is empty, i.e., the contents are equal to zero. These two situations correspond to the two linear sections in Figure 28. From Equation (13), the horizontal separation of these two lines is related to the length of the hysteresis buffer, C_H by the expression

$$C_H = \frac{\Delta\theta_H}{SF} \quad (23)$$

Similarly, using the \overline{SF} to map θ_{WORM} into C , and the fact that the displacement of the wormgear equals the displacement of the axis of interest, the curve shown in Figure 30 can be obtained from Figure 28. From Figure 30 it is apparent that two different pulse counts can be obtained for any given position, θ , depending on whether that position is approached from a CW or a CCW direction. The difference in the two counts is a measure of the hysteresis present in the gear train and is also the required length for the hysteresis buffer. By using this difference as the length of the hysteresis buffer, counts received by the MPU which occur while the gears are operating on one of the horizontal

sections of the curve in Figure 30 are not considered "valid" and therefore do not cause the MPU to modify the position. Using Equation (23) and data collected in the laboratory the average hysteresis present in each of the gear trains was determined (from 45 measurements on the Pan axis and 30 measurements on the Tilt axis) to be

$$\overline{C}_{H(\text{Pan})} = 7.39 \text{ Pulses} \quad (24)$$

$$\overline{C}_{H(\text{Tilt})} = 6.06 \text{ Pulses} \quad (25)$$

and the RMS errors were calculated to be,

$$\sigma_{C_{H(\text{Pan})}} = 1.0 \text{ Pulses} \quad (26)$$

$$\sigma_{C_{H(\text{Tilt})}} = 0.91 \text{ Pulses} \quad (27)$$

C. IMPLEMENTATION OF THE CALIBRATION DATA

1. Background

Figure 31 outlines the basic operation of each of the MPU's. Although each of the routines is described in detail by the comments included in the programs, the operation of the Count Routine is the heart of the program and should be explained prior to discussing the actual implementation of the experimental results.

When the system operator causes the camera servo to rotate, each optical shaft encoder translates the displacement of one of the axes into two series of digital pulses. The two pulse trains, referred to as Channels A and B, are TTL logic level signals. When the logic level of Channel A transitions from low to high (rising edge transition) or from high to low (falling edge transition), the edge detector (See Figure 15 on page 33) pulls pin 3 of the associated MPU low for approximately 2 μsec . When this occurs an external interrupt (EXT INT or $\overline{\text{INT}}$) request is generated and the MPU begins execution of the Count Routine.

As mentioned in Chapter III, since both rising and falling edge transitions are detected by the edge detector, the signal processor must be capable of detecting multiple oscillations of the shaft about a single logic level transition point. Accordingly, the first tasks performed by the Count Routine are to determine the direction of rotation and to simultaneously determine whether the interrupt is the result of a stationary shaft oscillation. To do this the Count Routine checks the state of pin 17 (Channel A) and pin 19 (Channel B). Operation of this portion of the routine is summarized in Table 5.

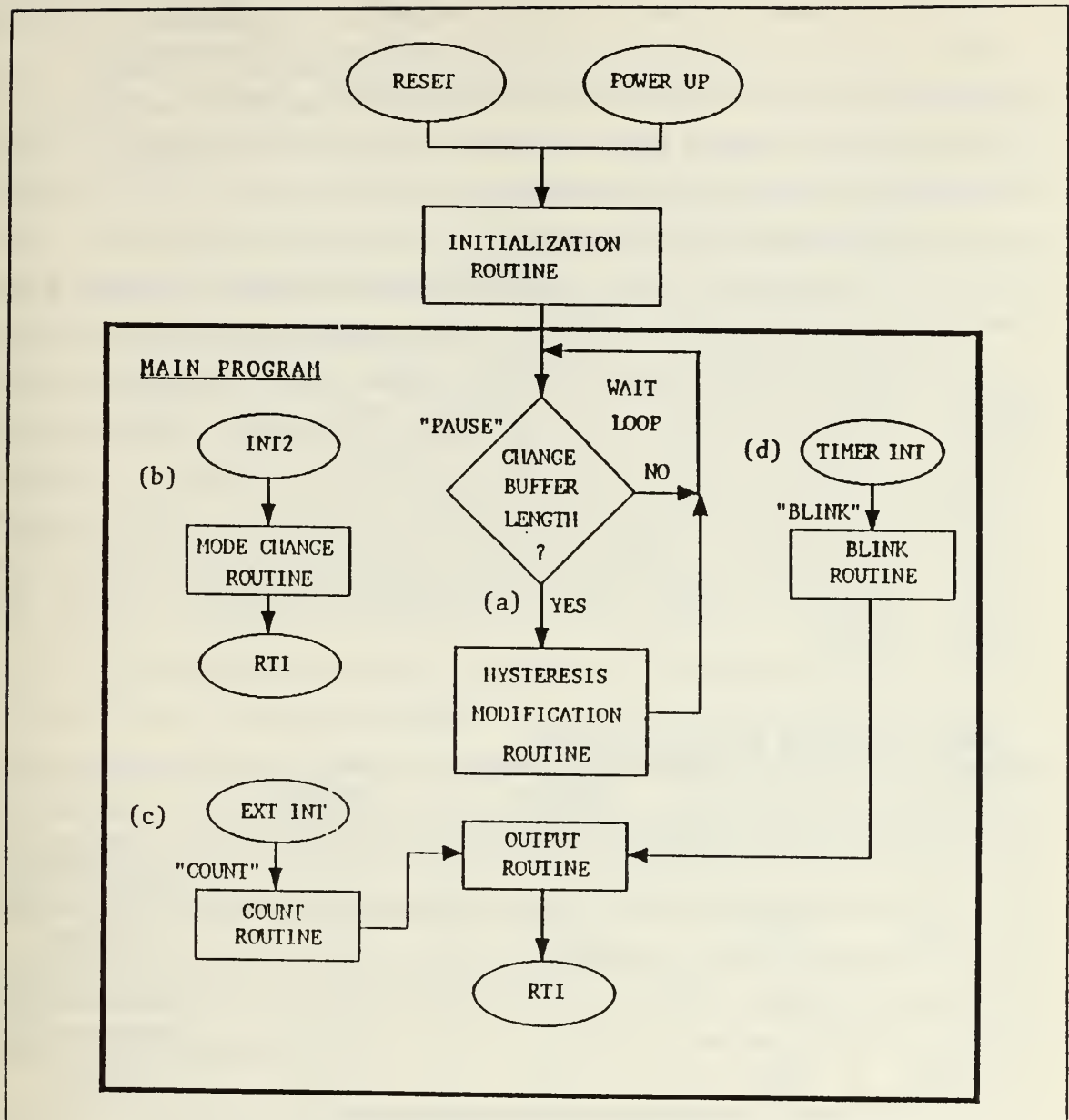


Figure 31. Program Flow Diagram: Program executes in the Wait Loop until; (a) the operator requests to modify the hysteresis buffer, (b) the operator requests to change the display mode, (c) an external interrupt is generated by the Channel A edge detector or, (d) a timer interrupt causes the display mode to "blink". All interrupt routines are terminated with a return from interrupt (RTI) command.

Note that CW rotation is indicated when Channel B leads Channel A in phase and CCW rotation is indicated if Channel A is leading Channel B. The possibility of erroneously counting multiple oscillations about a single point is eliminated by "counting" only the leading edge transitions when the shaft is rotating CW and only the trailing edge transitions when the rotation is CCW. All other transitions cause the program to execute a "return from interrupt" (RTI) instruction.

2. Implementing the Hysteresis Buffer

The transitions that are to be counted cause the program to compare the contents of the hysteresis buffer, HYSTCT, and the direction of rotation to the experimentally determined buffer length, $HYST \approx \overline{C}_H$. If the rotation is CW and the buffer is full (i.e., $HYSTCT = HYST$), or if the rotation is CCW and the buffer is empty (i.e., $HYSTCT = 0$), then the "slack" due to the gear backlash should have been taken up, the transitions are considered "valid" and the MPU modifies the position appropriately. "Invalid" counts cause the contents of the hysteresis buffer to be incremented or decremented depending on whether the present direction of rotation is CW or CCW (Figure 29 refers).

Table 5. COUNT ROUTINE LOGIC

Channel A	Channel B	Direction of Rotation	Count the Pulse?	Action
Low	Low	CW	No	Increment the hysteresis buffer.
Low	High	CCW	Yes	Decrement the position.
High	Low	CCW	No	Decrement the hysteresis buffer.
High	High	CW	Yes	Increment the position.

From the calibration data for the Pan axis, $\overline{C}_{H(Pan)} \approx 7.4$ and $\sigma_{C_{H(Pan)}} \approx 1.0$. Because the length of the hysteresis buffer must be an integer value, $\overline{C}_{H(Pan)}$ needed to be rounded off. Rounding to the nearest whole number initially seemed the most logical approach. Upon further consideration, however, it was decided to round 7.4 up to 8. Considering the relatively small data base (45 measurements) upon which the average was based, the fact that the standard deviation was 1.0 and that the gear backlash will only increase

with time, this seemed like the most reasonable approach. The buffer length for the Tilt axis was set equal to 6 ($\overline{C}_{H(Tilt)} = 6.06$).

3. Implementing the Scale Factor

There are three counters in each MPU that keep track of the position information for the axis of interest. The first, BINCT, is simply a binary counter that is incremented by one for each valid CW count and decremented by one for each valid CCW count. The other two counters consist of two sets of pointers, two sets of data registers and a shared data table. Each byte in a pointer points to an address in the table that contains two BCD digits which make up a portion of the position information.

In order to increment (decrement) the pulse count, BCDCT, by one, the count pointer, CTPTR, is incremented (decremented) by one causing it to point to a new table address. The contents of the table at the new addresses are then moved into BCDCT. Modification of the position counter, DEGRES, is performed in much the same manner. DEGRES contains a BCD number that, when multiplied by 0.001, represents the angular position (in degrees) of the shaft of interest. Thus, each time the camera is displaced in a CW direction through one degree, the contents of DEGRES should be incremented by 1000. To do this, the position pointer, PTR, must be incremented (decremented) by seven or eight each time CTPTR is incremented (decremented) by one. Incrementing PTR by seven corresponds to an angular displacement of 0.007° and since \overline{SF}_{Pan} and \overline{SF}_{Tilt} are each slightly larger than 0.007° , periodically PTR must be incremented by eight to reduce the cumulative round off error. Specifically, if PTR is incremented by seven each time a valid CW pulse is detected (except when BINCT is an even multiple of 32) and is incremented by eight when BINCT is a modulo 32 number, the effective scale factor is given by:

$$\begin{aligned} SF_{eff1} &= \frac{1}{32} (31(0.007) + 0.008) \\ &= 0.00703125^\circ \text{Pulse}^{-1}, \end{aligned} \tag{28}$$

which is slightly larger than the desired $0.0070312^\circ \text{Pulse}^{-1}$, for the Pan axis and slightly smaller than the desired $0.0070452^\circ \text{Pulse}^{-1}$ for the Tilt axis. To further reduce the cumulative round off on the Pan axis, every 16,384 ($2^{14} = 32 \times 512$) counts PTR is incremented by seven instead of eight. This results in an effective scale factor of,

$$\begin{aligned}
 SF_{eff_2} &= \frac{1}{512} \left\{ 511 \left[\frac{1}{32} (31(7) + 8) \times 10^{-3} \right] + 0.007 \right\} \\
 &= (7.03119 \times 10^{-3})^\circ \text{Pulse}^{-1} ,
 \end{aligned} \tag{29}$$

which is within two parts in one million.

The maximum error introduced into the measurement should occur when the camera is rotated through the largest possible angle. To predict this error on the Pan axis, when the camera has been displaced by 360° ,

$$\begin{aligned}
 \text{BCDCT} &= \frac{360^\circ}{SF_{\text{Pan}}} \\
 &= 51,200 \text{ Pulses}
 \end{aligned} \tag{30}$$

so the position error using SF_{eff_1} and SF_{eff_2} should be;

$$\begin{aligned}
 e_{\text{Pan}} &= 360^\circ - [3(SF_{eff_2}) + (51,200 - 3(16,384))(SF_{eff_1})] \\
 &= 0.00295^\circ .
 \end{aligned} \tag{31}$$

Thus, the error due to the scale factor on the Pan axis should be well within the desired resolution of $\pm 0.006^\circ$.

Using SF_{eff_1} alone as the scale factor for the Tilt axis, the maximum theoretical error over $\pm 12^\circ$ due to the scale factor round off is determined in the same manner.

$$\begin{aligned}
 \text{BCDCT} &= \frac{12^\circ}{SF_{\text{Tilt}}} \\
 &= 17,033 \text{ Pulses}
 \end{aligned} \tag{32}$$

So that,

$$\begin{aligned}
 e_{\text{Tilt}} &= 12^\circ - 17,033(SF_{eff_1}) \\
 &= 0.0234^\circ ,
 \end{aligned} \tag{33}$$

which again is significantly less than the required resolution of $\pm 0.23^\circ$ for the Tilt axis.

The final step in the Count Routine is a branch to the Display Routine. Depending on whether the MPU is in the Count or Position Mode, the Display Routine copies the contents of BCDCT or DEGRES to the output ports and then executes an RTI instruction.

D. FINAL TESTING

1. General

Final laboratory testing and evaluation of the measurement system was performed after the calibration results had been implemented in each of the MPU Count Routines. The purpose of the testing was to verify that the calibration results had been properly coded into the MPU's and to determine the resolution capabilities of the measurement system experimentally.

This verification process included determining the combined error due to the hysteresis and scale factor errors. The use of some simple multiple random variable theory was therefore required. From [Ref. 20: pp. 121,122] the variance of a weighted sum of M random variables is the weighted sum of their covariances, $C_{X_i X_j}$, and is given by,

$$\sigma^2 = \sum_{i=1}^M \sum_{j=1}^M \alpha_i \alpha_j C_{X_i X_j} , \quad (34)$$

where α_i is the weight associated with X_i . Additionally, the covariance can be expressed as

$$C_{XY} = \rho \sigma_X \sigma_Y , \quad (35)$$

where ρ is the normalized second-order moment and is known as the correlation coefficient of X and Y . The correlation coefficient is bounded by

$$-1 \leq \rho \leq 1 . \quad (36)$$

In the case where there are two equally weighted random variables, $M = 2$ and $\alpha_i = \alpha_j = 1.0$. Substituting into Equation (34) and expanding

$$\sigma^2 = C_{XX} + C_{XY} + C_{YX} + C_{YY} . \quad (37)$$

Using Equation (35),

$$\sigma^2 = \sigma_X^2 + 2\rho\sigma_X\sigma_Y + \sigma_Y^2 . \quad (38)$$

Combining (36) and (38) yields

$$\sigma_X^2 - 2\sigma_X\sigma_Y + \sigma_Y^2 \leq \sigma^2 \leq \sigma_X^2 + 2\sigma_X\sigma_Y + \sigma_Y^2 . \quad (39)$$

The bounds of the combined scale factor and hysteresis errors can therefore be determined from

$$\sqrt{\sigma_{e_{SF}}^2 - 2\sigma_{e_{SF}}\sigma_{e_H} + \sigma_{e_H}^2} \leq \sigma_e \leq \sqrt{\sigma_{e_{SF}}^2 + 2\sigma_{e_{SF}}\sigma_{e_H} + \sigma_{e_H}^2} . \quad (40)$$

where:

- σ_e = standard deviation of the combined error,
- $\sigma_{e_{SF}}$ = standard deviation of the scale factor error, and
- σ_{e_H} = standard deviation of the hysteresis error.

Note that the bounds are determined by the two cases where the hysteresis error, e_H , and the scale factor error, e_{SF} , are “completely correlated”. The upper bound corresponds to the case where an increase in e_{SF} implies an increase in e_H , and the lower bound corresponds to the case where an increase in e_{SF} directly implies a decrease in e_H .

A third case is also of particular interest. If e_H and e_{SF} are completely uncorrelated, i.e., $\rho = 0$, then from Equation (38),

$$\sigma_e = \sqrt{\sigma_{e_{SF}}^2 + \sigma_{e_H}^2} . \quad (41)$$

which can also be written as

$$e = \pm \sqrt{e_{SF}^2 + e_H^2} , \quad (42)$$

where $e = \pm \sigma_e$ is the 1.0 σ error due to the scale factor and hysteresis errors, e_{SF} and e_H respectively. Based on the physical nature of the two errors it is reasonable to assume that e_{SF} and e_H are statistically uncorrelated; however, no experimental data was collected to support this hypothesis. Due to this lack of a priori information, the maximum RMS error, $e_{max} = \pm \sigma_{e_{max}}$, given by

$$e_{max} = \pm \sqrt{e_{SF}^2 + 2e_{SF}e_H + e_H^2} , \quad (43)$$

will be used to describe the resolution capabilities of the measurement system.

2. Pan Axis

a. Hysteresis

To test the operation of the Pan axis hysteresis buffer, the Initialization Routine was programmed to set the buffer length to 8. Then, as described in the first section of this chapter, the servo was used to position the beam of a small laser on a fixed target. By approaching the target alternately from a CW and a CCW direction and

comparing the difference in the output counts from the shaft encoders, the hysteresis error was determined. The average error after 31 measurements was

$$\bar{e}_{H(\text{Pan})} = -0.1880 \text{ Pulses} , \quad (44)$$

and the RMS error was

$$\sigma_{e_{H(\text{Pan})}} = 1.7699 \text{ Pulses} . \quad (45)$$

Since the mean error is "near zero" compared to the standard deviation, the 1.0σ error e_H , due to the hysteresis can be determined from

$$e_H = \pm (\sigma_{e_H}) \overline{SF} \quad (46)$$

so that

$$e_{H(\text{Pan})} = \pm 0.0124^\circ . \quad (47)$$

b. Scale Factor

Verification of the scale factor was performed in the same manner as the scale factor calibration, except that the MPU was calibrated in the Count Mode and tested in the Position Mode. Since these tests sought to find the maximum error due to the scale factor, and the error is directly proportional to the angle that is being measured, these tests were conducted by displacing the camera servo through the maximum angles permitted by the camera and the laboratory. Specifically, on the Pan axis the servo was rotated through approximately 360° . The mean error due to the scale factor on the Pan axis was determined from 15 samples to be

$$\bar{e}_{SF(\text{Pan})} = -0.0018^\circ \quad (48)$$

and the RMS error was

$$\sigma_{e_{SF(\text{Pan})}} = 0.00890^\circ . \quad (49)$$

As with the hysteresis error, if we neglect the small bias due to the $\bar{e}_{SF(\text{Pan})}$, we can describe the 1.0σ RMS error due to the scale factor as

$$\begin{aligned} e_{SF(\text{Pan})} &= \pm \sigma_{SF(\text{Pan})} \\ &= \pm 0.00890^\circ \end{aligned} \quad (50)$$

c. Combined Error

From Equation (42) the combined error on the Pan axis if e_H and e_{SF} are uncorrelated can be estimated as

$$\begin{aligned} e_{Pan} &= \pm \sqrt{(0.0124)^2 + (0.0089)^2} \\ &= \pm 0.01526^\circ . \end{aligned} \quad (51)$$

And from Equation (43) the maximum combined error on the Pan axis is

$$e_{Pan_{max}} = \pm \sqrt{(0.0124)^2 + 2(0.0124)(0.0089) + (0.0089)^2} \quad (52)$$

$$e_{Pan_{max}} = \pm 0.0213^\circ . \quad (53)$$

The combined error is approximately three times larger than the design specification limit and is due primarily to the hysteresis error.

3. Tilt Axis

a. Hysteresis

The procedure used to verify the operation of the calibrated Tilt MPU was identical to that described in the previous section. Using a hysteresis buffer length of 6 resulted in

$$\bar{e}_{H(Tilt)} = -0.0965 \text{ Pulses} \quad (54)$$

and,

$$\sigma_{e_{H(Tilt)}} = 1.3156 \text{ Pulses} \quad (55)$$

after 13 samples. As before we can define the 1.0σ error from $e = \sigma \overline{SF}$ to be

$$e_{HTilt} = \pm 0.00529^\circ . \quad (56)$$

b. Scale Factor

Testing the scale factor on the Tilt axis was limited by the physical construction of the servo and the size of the laboratory. The angle over which testing could be performed was limited to $\pm 6^\circ$ from the horizontal plane. Consequently, the RMS error for the scale factor on the Tilt axis was determined in exactly the same manner as

the RMS error for the Pan axis scale factor, but since the error due to rounding of the scale factor is directly proportional to the angle being measured the results were multiplied by 2.0 to account for the limited range of the test. The modified results should therefore be representative of the maximum error one should expect if the measurement system is used to measure elevation angles over a range of $\pm 12^\circ$.

The error due to the scale factor is described from 16 samples by

$$\bar{e}_{SF(Tilt)} = 0.0070^\circ \quad (57)$$

and,

$$\sigma_{e_{SF(Tilt)}} = 0.0665^\circ . \quad (58)$$

Including the factor of two in the calculation we have

$$\begin{aligned} e_{SF(Tilt)} &= \pm 2(0.0665^\circ) \\ &= \pm 0.1330^\circ . \end{aligned} \quad (59)$$

c. Combined Error

The combined RMS error is determined in the same manner as before. If e_H and e_{SF} are uncorrelated,

$$\begin{aligned} e_{Tilt} &= \pm \sqrt{(0.1330)^2 + (0.00529)^2} \\ &= 0.1331^\circ , \end{aligned} \quad (60)$$

and the maximum combined RMS error is

$$e_{Tilt_{max}} = \pm \sqrt{(0.1330)^2 + 2(0.1330)(0.00529) + (0.00529)^2} \quad (61)$$

$$e_{Tilt_{max}} = \pm 0.1383^\circ . \quad (62)$$

The Tilt axis measurement system appears to perform well within the required resolution specifications.

E. FINAL IMPLEMENTATION

Once the program debugging, calibration and testing were completed, final implementation of the system remained. Taking the design from the prototype/development model to a fully functional system was a straightforward but time-consuming evolution.

The plans for the printed circuit boards (PCB's) were made directly from the schematics shown in Appendix A; the boards were then etched and assembled from the plans which are shown in Appendix B. All of this work was performed by sailors attached to the Academic Division of the NPS.

As previously discussed, the M68705EVM Evaluation Module provided a powerful and flexible means of debugging and evaluating the performance of the microprocessor based signal conditioner. Additionally, once program testing was completed the EVM's EPROM microprocessor programmer provided the means to program the EPROM MCU's. A detailed, but simple to follow, programming procedure for programming the MC68705U3 is given in [Ref. 18: pp. (3-26)-(3-27)].

V. CONCLUSIONS AND RECOMMENDATIONS

A. SYSTEM PERFORMANCE

The prototype system was calibrated and successfully tested in a laboratory environment. Experimental results indicate that the system is capable of measuring the video camera's elevation over a range of $\pm 12^\circ$ with a resolution of $\pm 0.138^\circ$ and its azimuth over 360° with a resolution of $\pm 0.021^\circ$. The system was designed to be low cost, reliable, and easy to operate. Only time will tell whether these objectives were truly achieved.

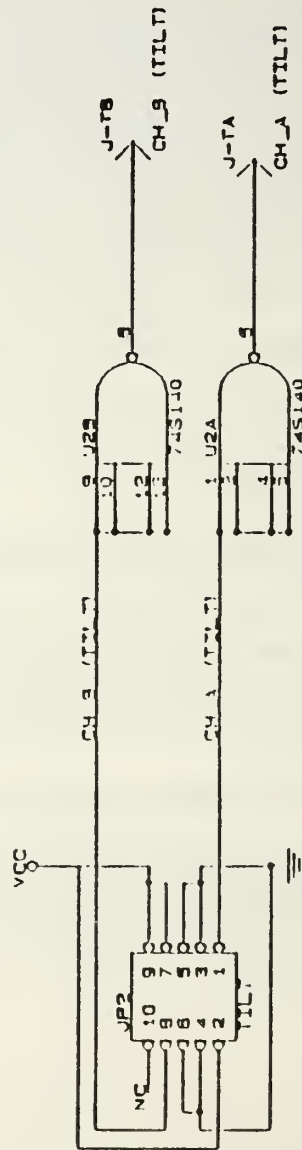
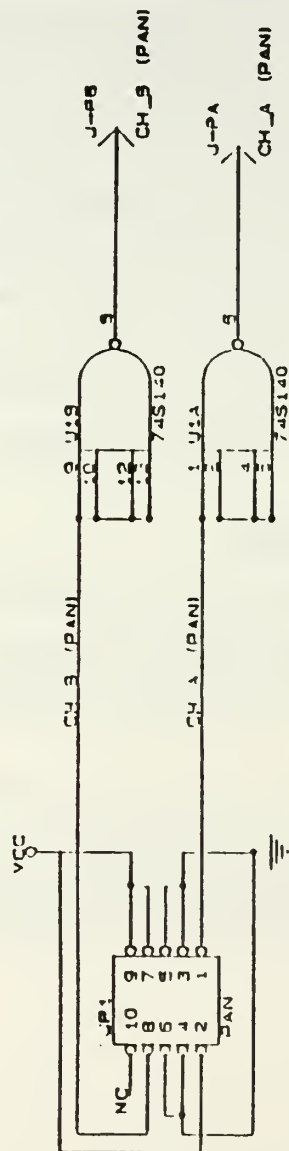
The portion of the system that will be located outdoors has been weatherproofed and is ready to be placed in service. Printed circuit board plans for the remainder of the system have been developed, but final implementation of the system is still ongoing. Once the system is fully operation additional testing should be performed in order to verify the completed system's performance. Although the laboratory results indicate that the system is capable of meeting all of the design criteria except for the required resolution on the Pan axis, the system must be further tested in a non-laboratory environment. "...The proof of a good design rests in the ability of the system to function in the outside world." [Ref 21]

B. RECOMMENDATIONS FOR FURTHER WORK

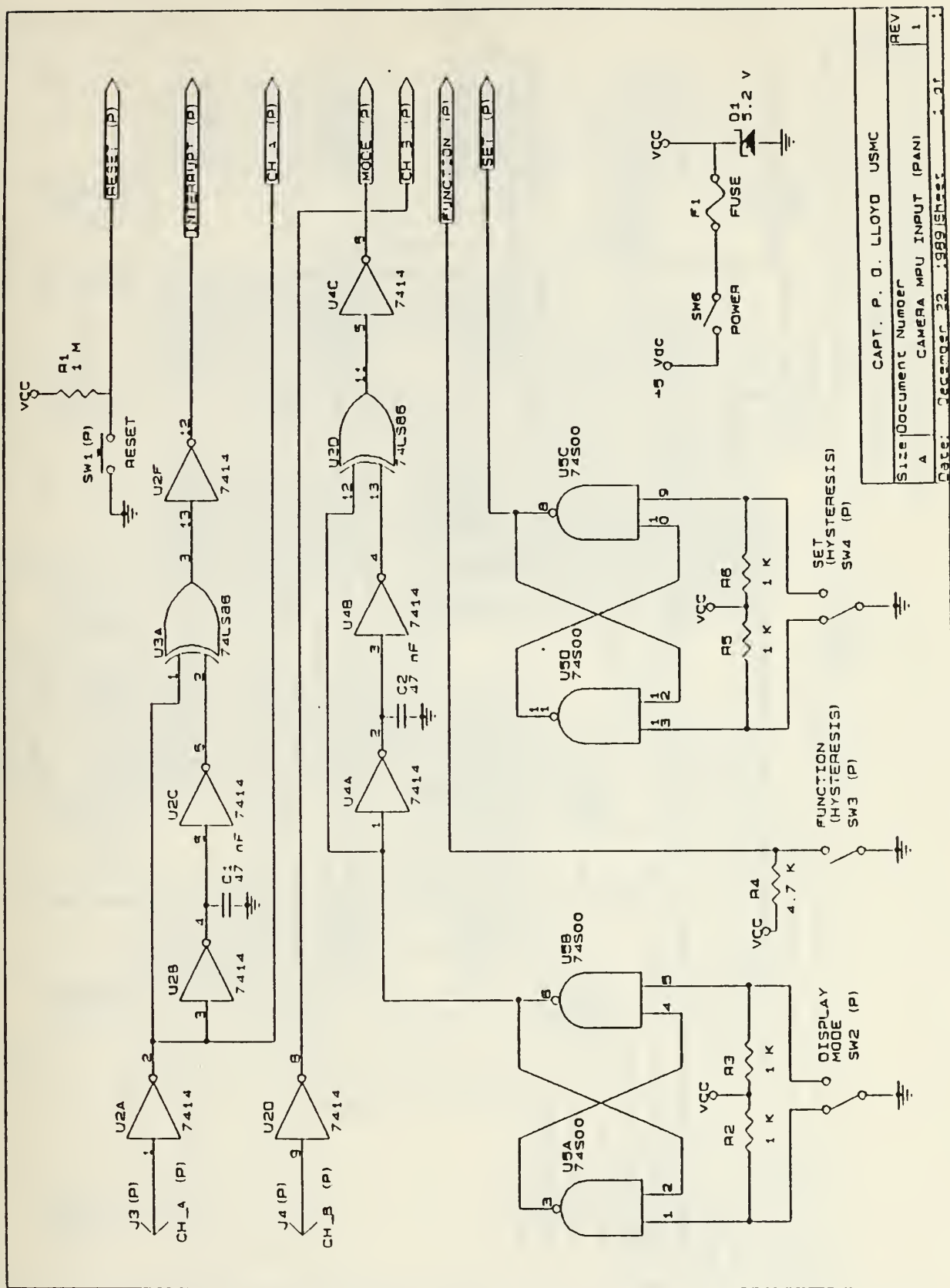
There are several areas for follow-on work with this project. Some possibilities are:

- Incorporate the measurement system's output into the video image being created by the video camera. This would permit a permanent record of the position information to be stored with the video image and would facilitate identification of the image at a later date.
- Design and build an automatic feedback control system for the camera.
- Implementation of a second video camera at the NPS, together with the NPS modified IRSTD, would permit triangulation of a target and would consequently provide range information which is not currently available. This information could provide valuable additional information to those who are developing the signal processing algorithms.

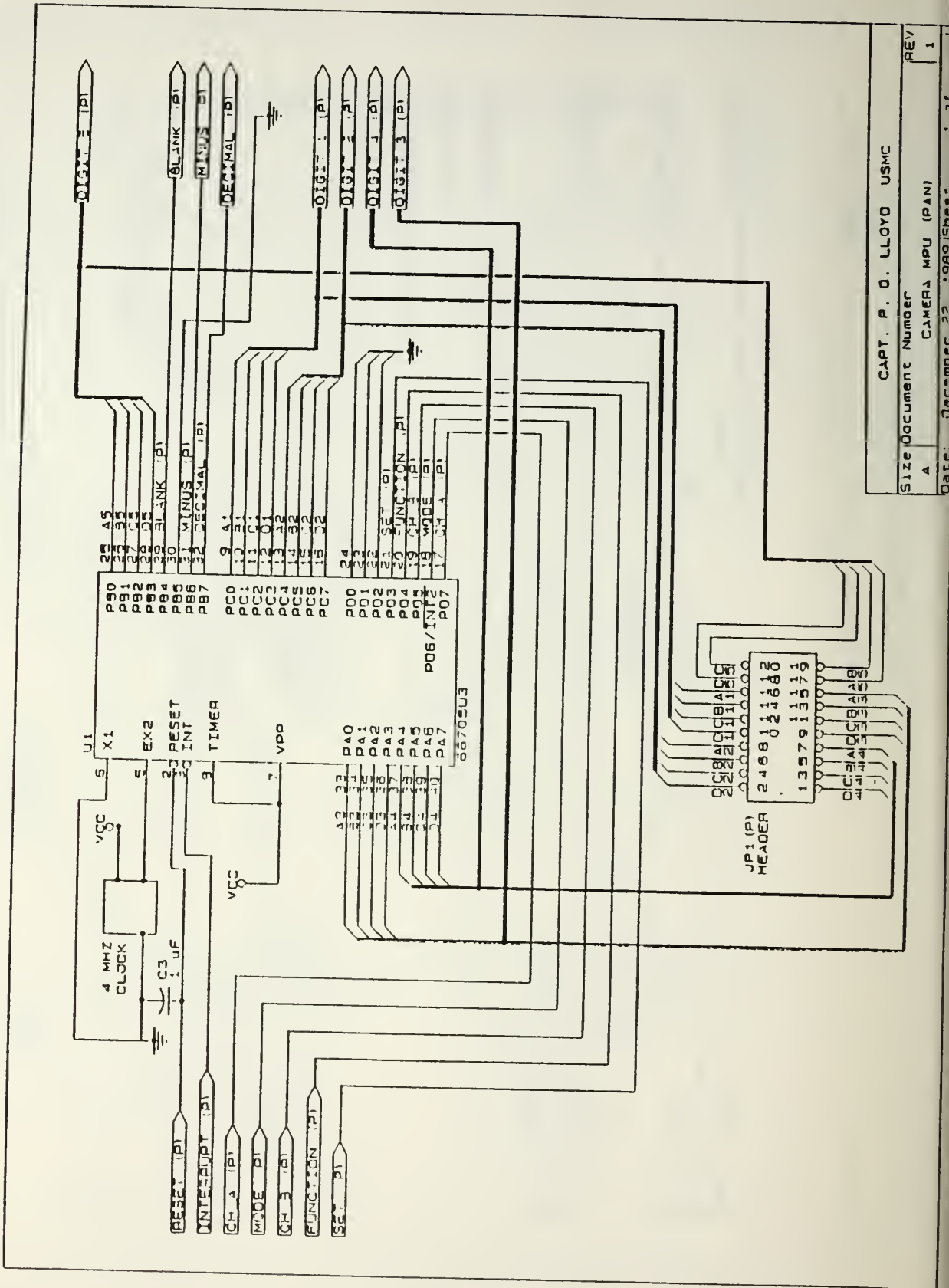
APPENDIX A. SCHEMATIC DIAGRAMS



CAPT. P. O. LLOYD USMC	
Size: Document Number	REV
A	1
LINE DRIVER	
Date: December 22, 1989 Sheet 1 of 1	



CAPT. P. O. LLOYD USMC	
Size	Document Number
A	CAMERA MPU INPUT (PANI)
REV	1
Date:	December 22, 1989 JED:st



CAPT. P. O. LLOYD USMC

Size Document Number

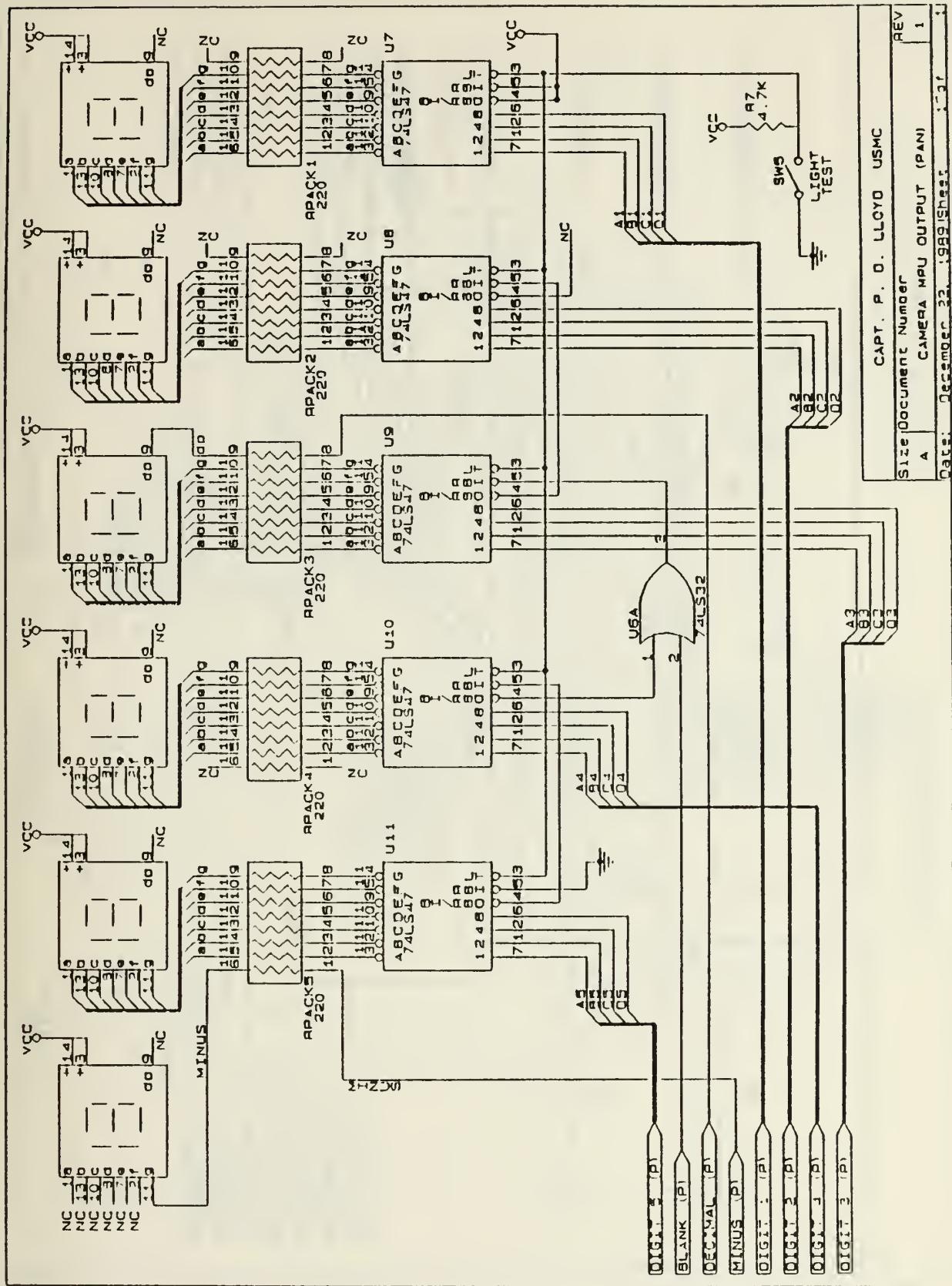
A

CAMERA MPU (PANI)

REV

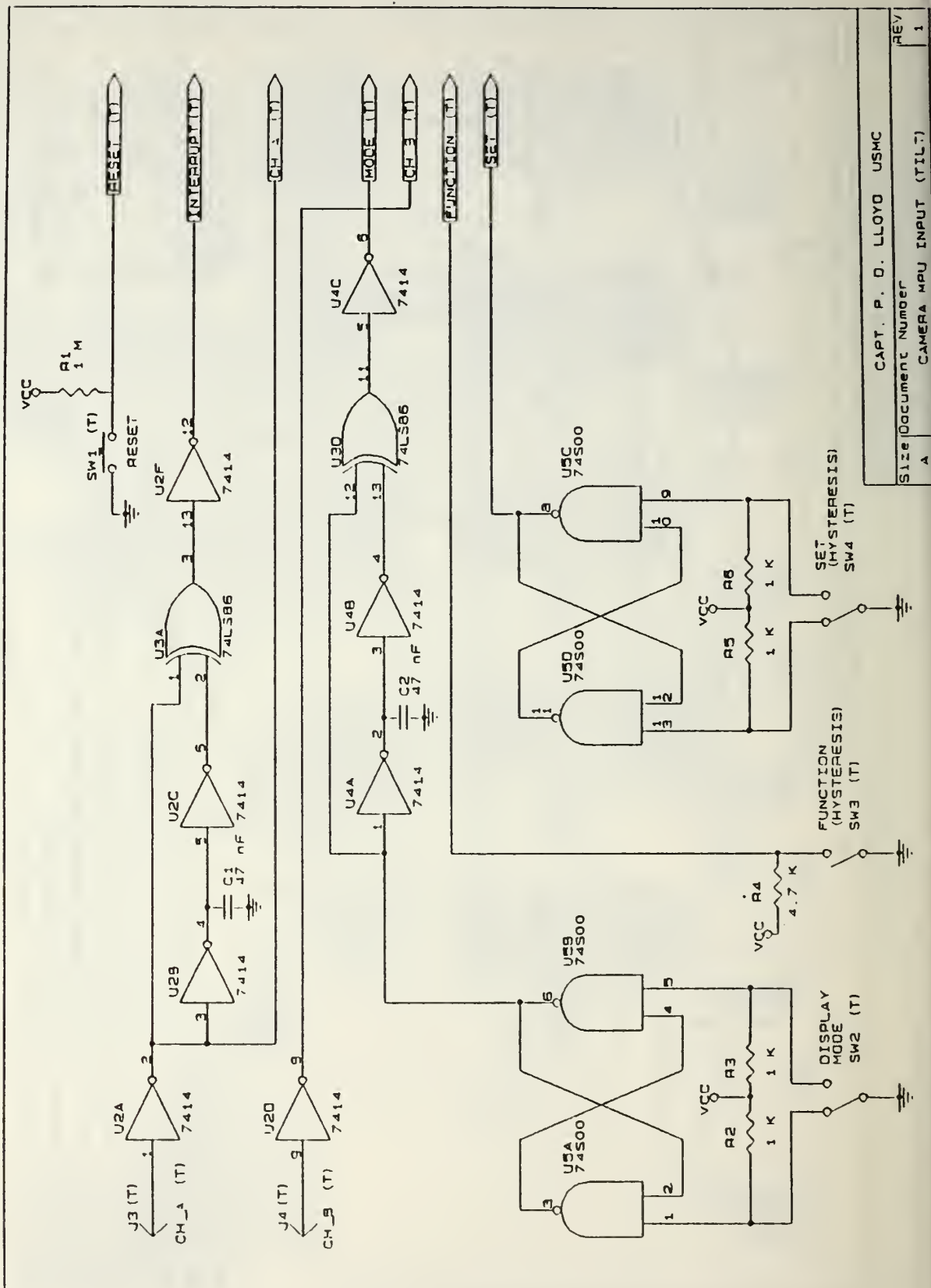
1

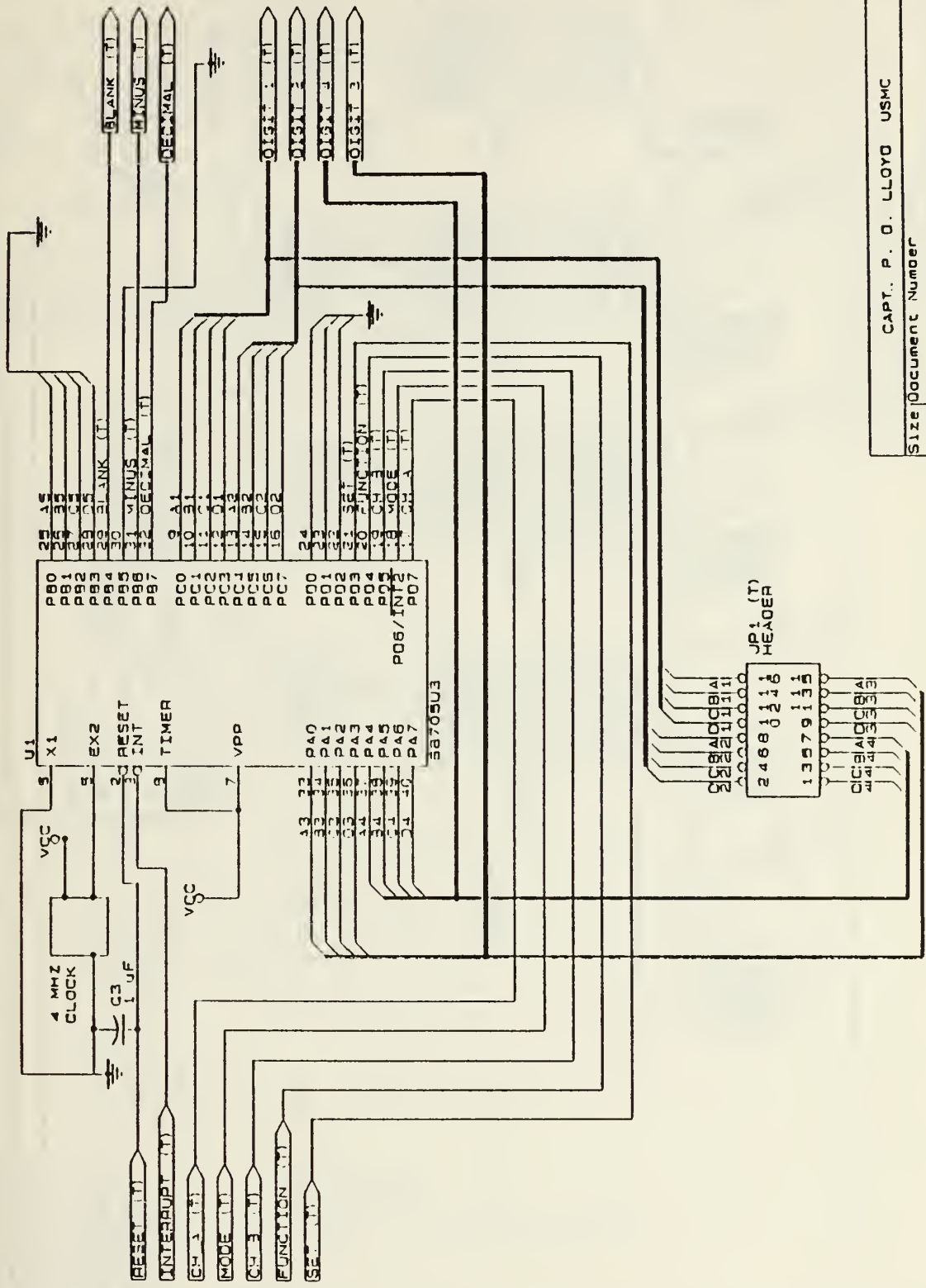
Date: December 22, 1989/Shea

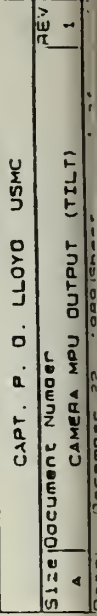


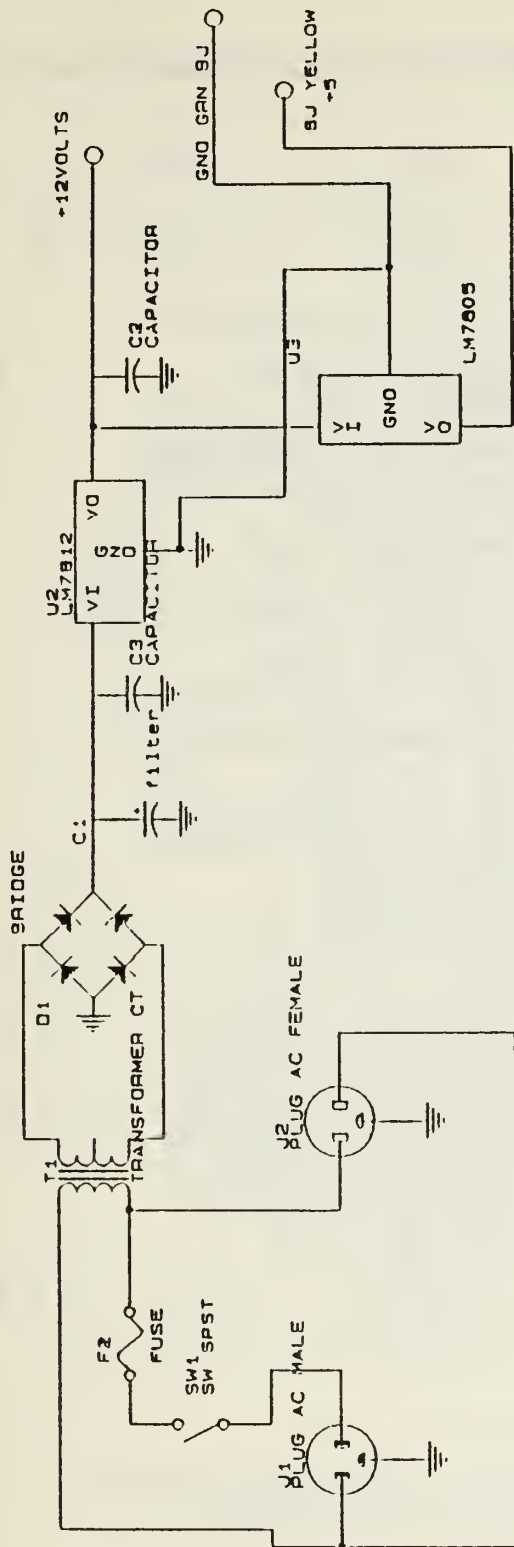
CAPT. P. O. LLOYD USMC

Size	Document Number	REV
A	CAMERA MPU OUTPUT (PAN)	1
Date	December 22, 1989	Sheet 1





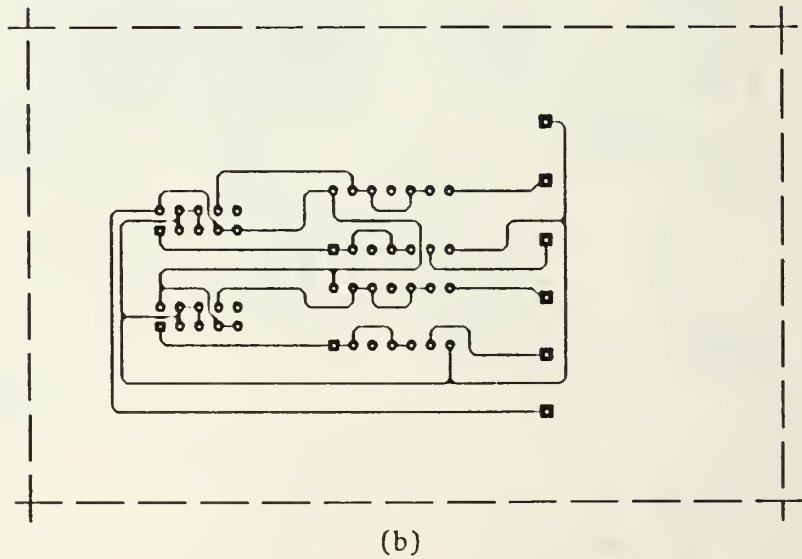
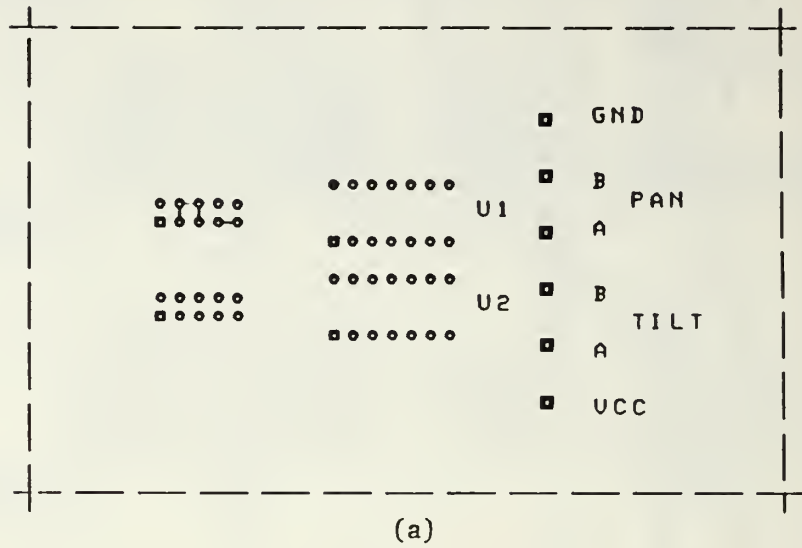




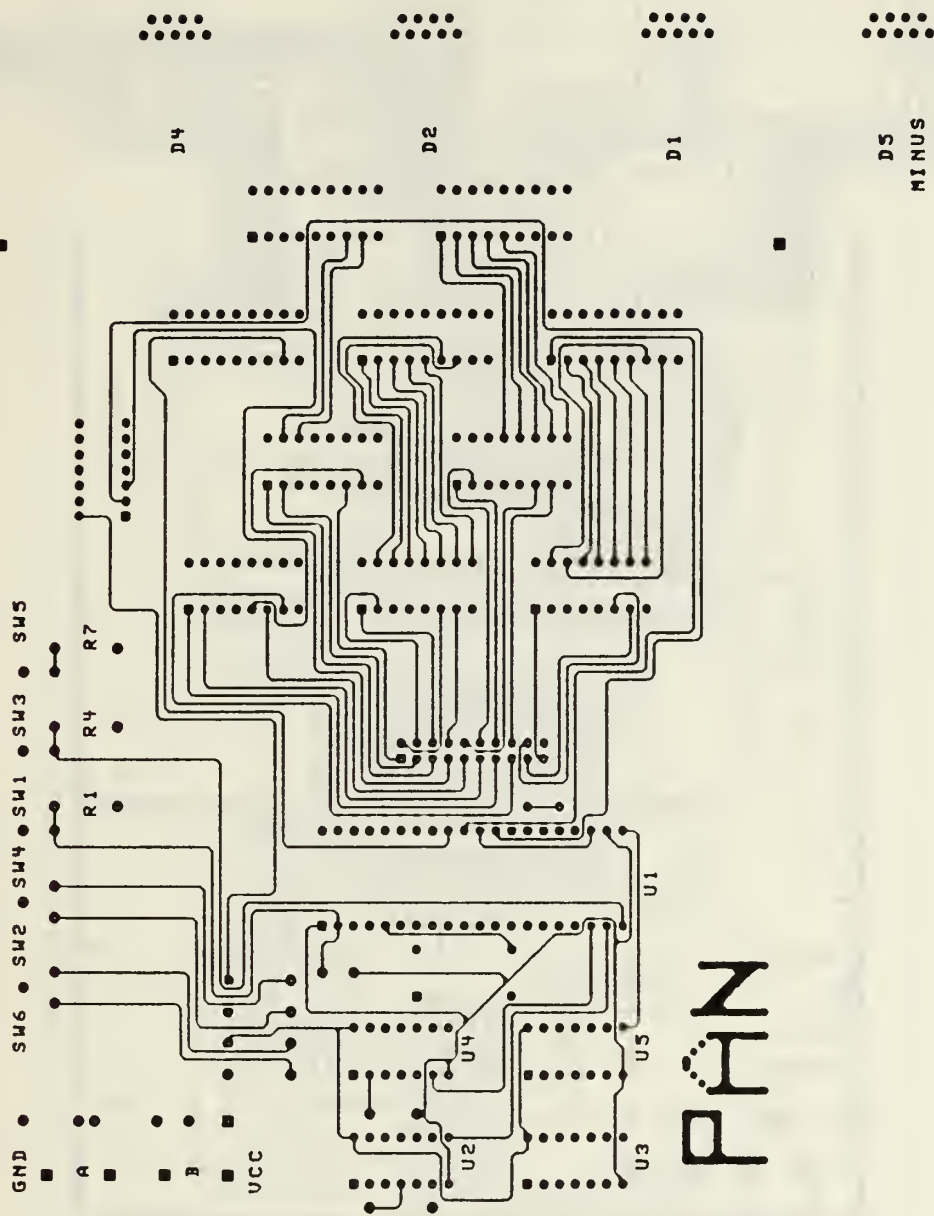
camera power supply and AC

Size	Document Number	REV
A	camera POWER SUPPLY	
Date:	January 1, 1980	Sheet 1 of 1

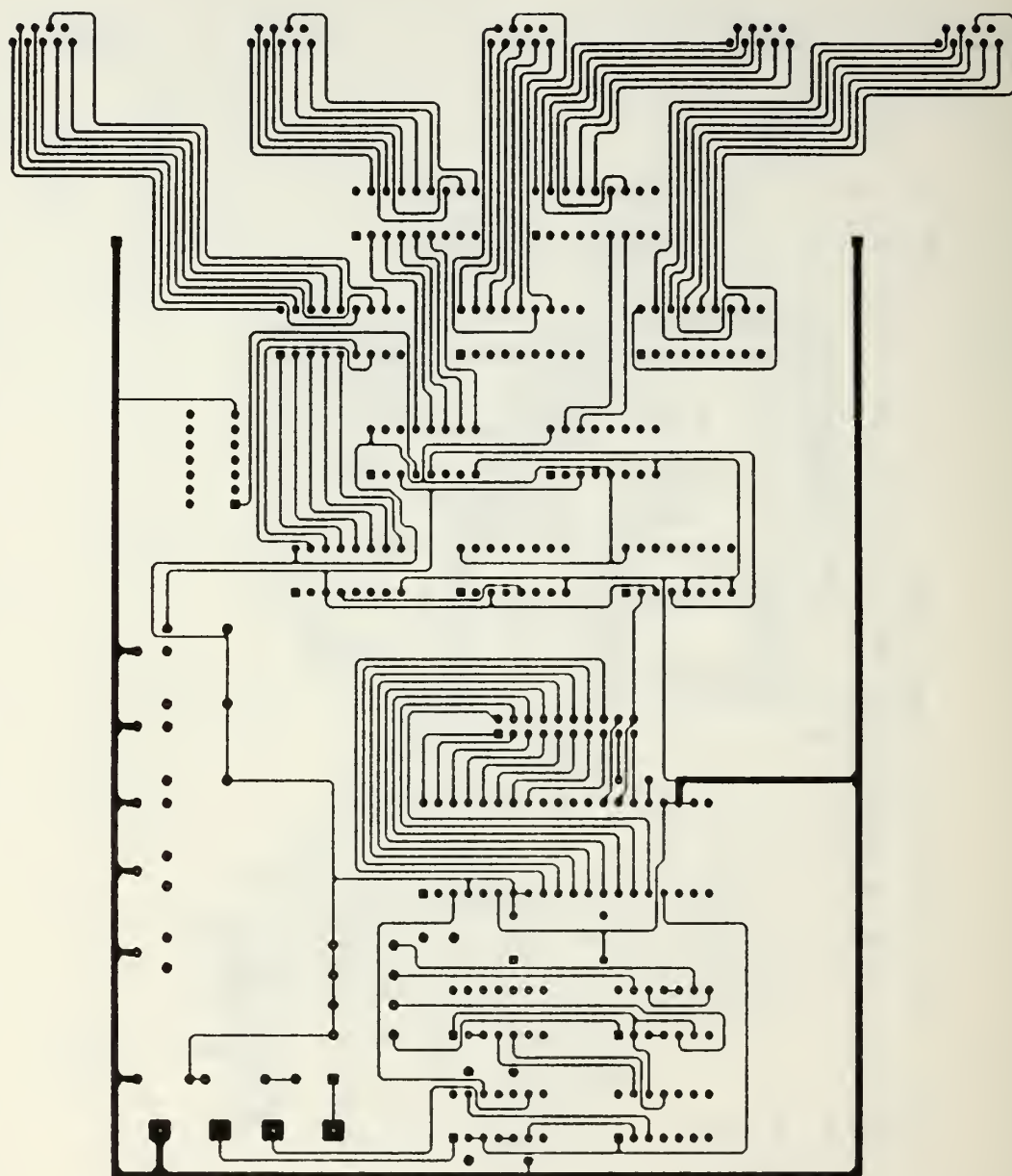
APPENDIX B. PRINTED CIRCUIT BOARD PLANS



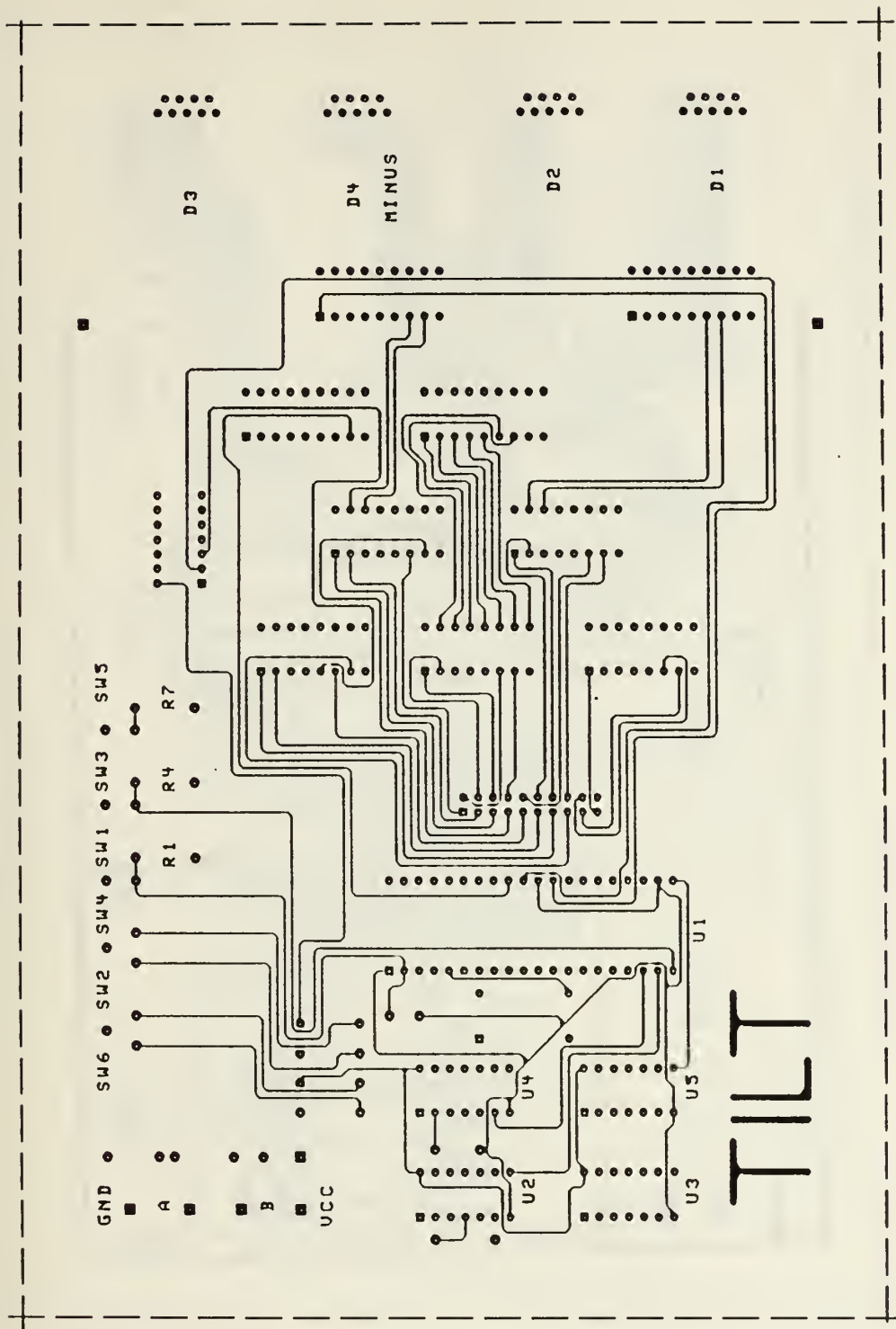
Line Driver, (a) Front and (b) Back. Full scale.



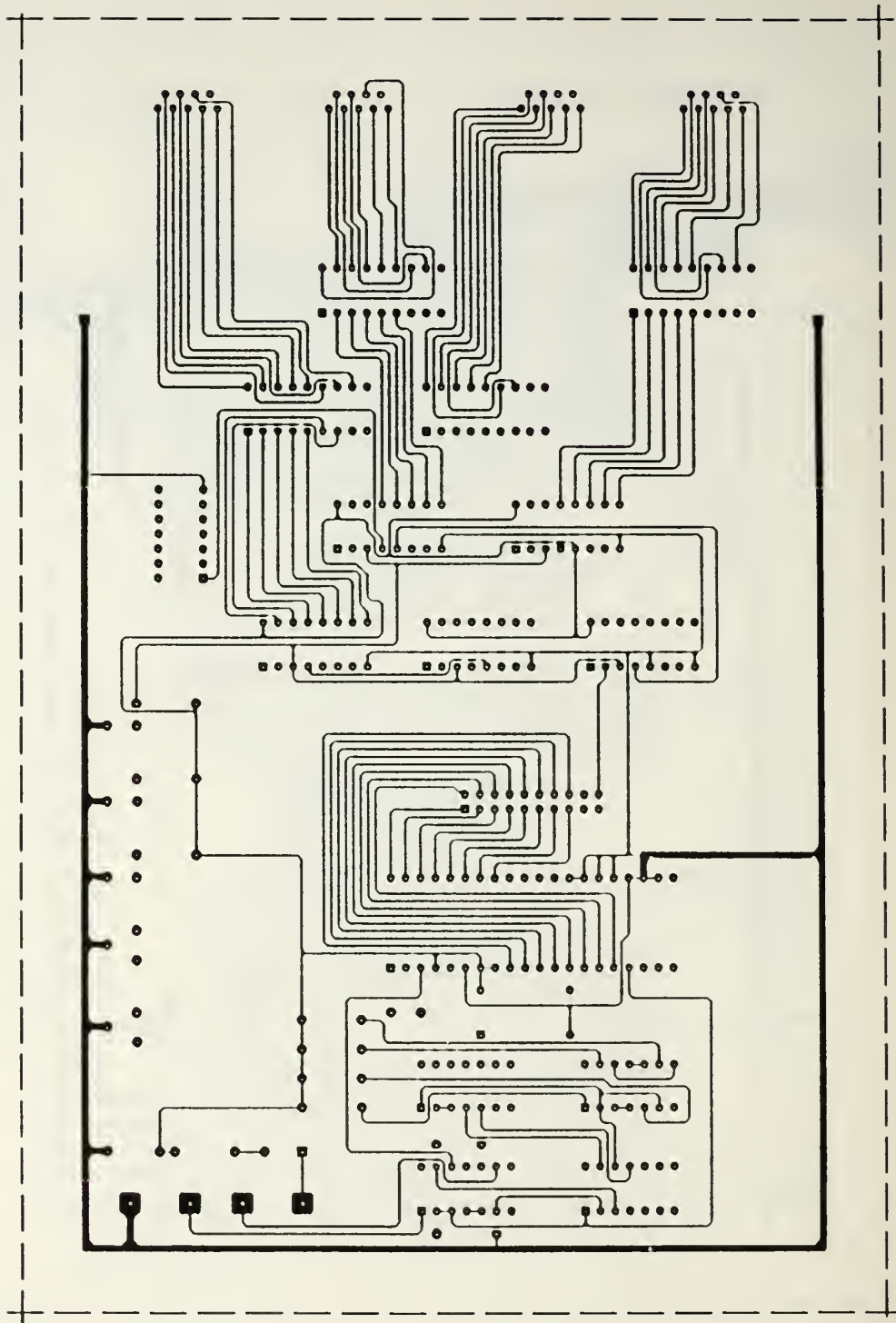
Pan MPU, Front. 90 % of full scale.



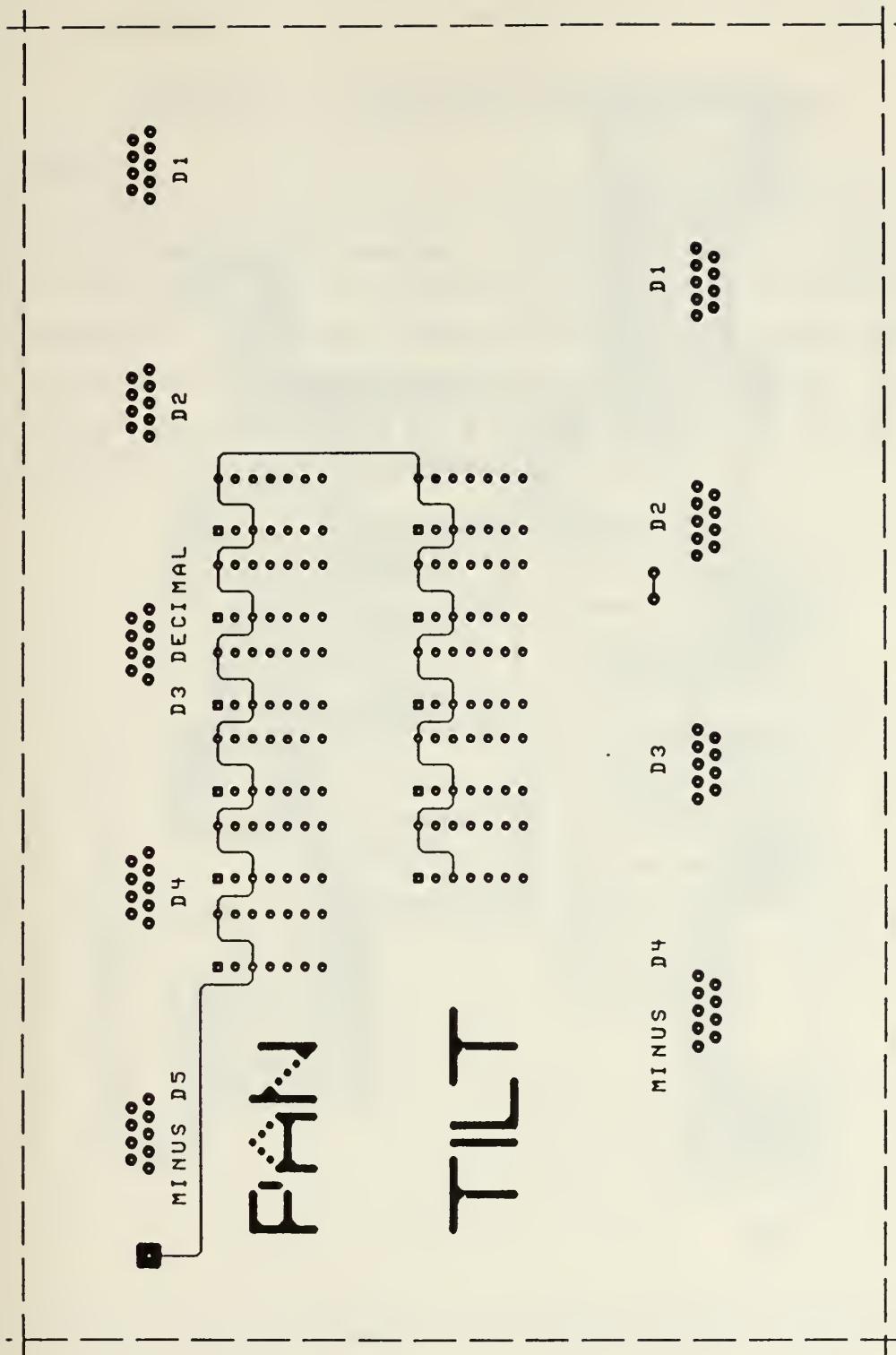
Pan MPU, Back. 90 % of full scale.



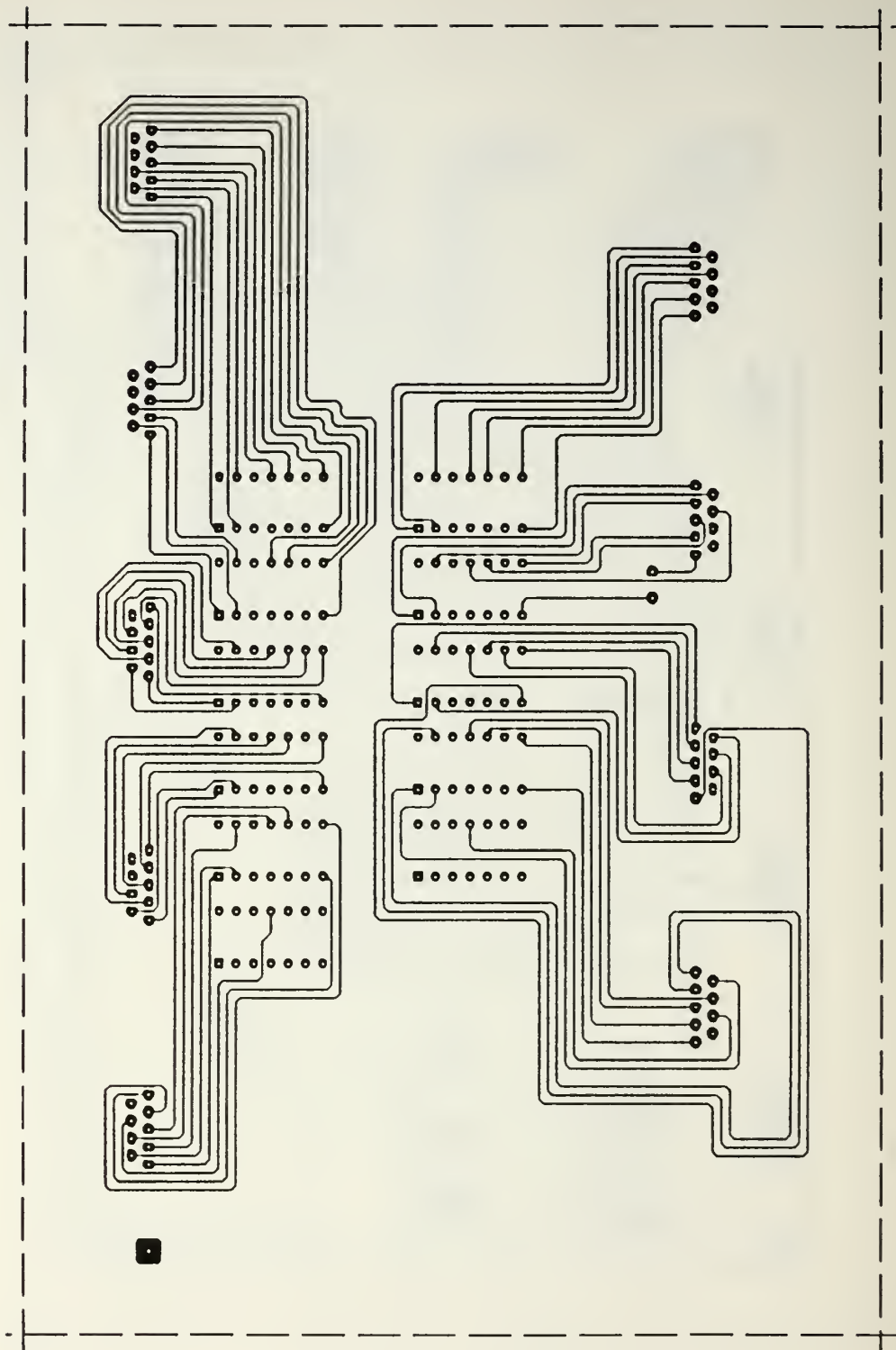
Tilt MPU, Front. 85 % of full scale.



Tilt MPU, Back. 85 % of full scale.



Display, Front. Full scale.



Display, Back. Full scale.

APPENDIX C. MICROPROCESSOR PROGRAMS

A. GENERAL

Sections B and C of this Appendix are the listing files for the two MPU programs written for the signal processor subsystems. The theory of operation of the two programs is identical and is most clearly described by Figure 31. The detailed operation of the Initialization , Mode Change, Blink, Output Display and Hysteresis Modify routines is described by the comments which accompany each of the programs. In addition to the detailed description provided by the program comments, the operation of the Count Routine is also explained in Chapter IV.

B. PAN

```

1          TTL          POSITION DETERMINING PROGRAM (AZIMUTH)
2          *            LATEST REVISION          9 MAY 89
3          *            FILE NAME                PAN.ASM
4          **
5          ** PROGRAM DESCRIPTION
6          **
7          **
8          **
9          ** I/O REGISTER ADDRESSES
10         **
11         0000          PORTA EQU $0000 I/O PORT A
12         0001          PORTB EQU $0001 I/O PORT B
13         0002          PORTC EQU $0002 I/O PORT C
14         0003          PORTD EQU $0003 INPUT PORT D
15         **
16         ** DATA DIRECTION REGISTER OFFSET
17         **
18         0004          DDR EQU 4 (eg. DDR FOR PORT A IS PORTA+DDR )
19         **
20         ** OTHERS
21         **
22         0008          TIMER EQU $0008 EIGHT BIT TIMER REGISTER.
23         0009          TCR EQU $0009 TIMER CONTROL REGISTER.
24         000A          MR EQU $000A MISCELLANEOUS REGISTER.
25         0010          RAM EQU $0010 START OF ON-CHIP RAM(112 - 31 FOR STACK)
26         0080          ZROM EQU $0080 PAGE ZERO OF ROM.
27         0100          ROM EQU $0100 START OF MAIN ROM.
28         0F38          MOR EQU $0F38 MASK OPTION REGISTER.
29         0FF8          INTRPT EQU $0FF8 LOCATION OF INTERRUPT VECTORS.
30         1000          MEMSIZ EQU $1000 MEMORY ADDRESS SIZE.
31         **
32         ** EQUATES
33         **
34         0001          BIT0 EQU 1
35         0002          BIT1 EQU 2
36         0004          BIT2 EQU 4
37         0008          BIT3 EQU 8
38         0010          BIT4 EQU 16
39         0020          BIT5 EQU 32
40         0040          BIT6 EQU 64
41         0080          BIT7 EQU 128
42         **
43         0000          B0 EQU 0
44         0001          B1 EQU 1
45         0002          B2 EQU 2
46         0003          B3 EQU 3
47         0004          B4 EQU 4
48         0005          B5 EQU 5
49         0006          B6 EQU 6
50         0007          B7 EQU 7
51         **
52         ** EQUATES FOR THE TIMER CONTROL REGISTER
53         **
54         ***
55         0007          TIR EQU 7 TIMER INTERRUPT REQUEST. 1 = REQUEST, 0 = NO REQ.
56         0006          TIM EQU 6 TIMER INTERRUPT MASK. 1 = DISABLED, 0 = ENABLED.
57         0005          TIN EQU 5 EXTERNAL OR INTERNAL CLOCK SOURCE. 1 = EXT, 0 = INT
58         0004          TEE EQU 4 EXTERNAL CLOCK ENABLE. NOT USED.
59         0003          PSC EQU 3 PRESCALER CLEAR. NOT USED.
60         0002          PS2 EQU 2 (PS2) --
61         0001          PS1 EQU 1 (PS1) |-- PRESCALER SELECT BITS.

```

```

62      0000      PS0      EQU      0      (PS0)  --
63      **
64      ** EQUATES FOR THE STATUS BYTE, 'STAT'.
65      ***
66      ***
67      **
68      0007      UD        EQU      7      COUNT DIRECTION? 1 = UP, 0 = DOWN.
69      0006      MOD_32    EQU      6      IS 'BINCT' MODULO 32? 1 = YES, 0 = NO.
70      0005      FLASH     EQU      5      BLINK THE DISPLAY? 1 = YES, 0 = NO.
71      0004      POSCT     EQU      4      DISPLAY POSITION OR COUNT? 1 = POS, 0 = COUNT.
72      0003      L_SET     EQU      3      VALUE OF 'MODE,PORTD' LAST TIME.
73      0002      NEGTV     EQU      2      IS 'BCDCT' NEGATIVE NUMBER? 1 = YES, 0 = NO.
74      ***          1      NOT USED.
75      ***          0      NOT USED.
76      ***
77      ***
78      ** I/O EQUATES AND DESCRIPTIONS.
79      ***
80      ***
81      ***      PORT A (I/O)
82      ***
83      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
84      ***      |          BCD DIGIT #4          |          BCD DIGIT #3          |
85      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
86      ***      | D4 | C4 | B4 | A4 | D3 | C3 | B3 | A3 |
87      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
88      *** BIT      7          6          5          4          3          2          1          0
89      ***
90      ***
91      ***      PORT B (I/O)
92      ***
93      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
94      ***      |          DISPLAY CONTROL          | BCD DIGIT #5 (MOST SIGNIFICANT) |
95      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
96      ***      | DECPT | POSTIV |          | BLANK | D5 | C5 | B5 | A5 |
97      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
98      *** BIT      7          6          5          4          3          2          1          0
99      ***
100     0007      DECPT     EQU      7      TO DISPLAY THE DECIMAL POINT...DECPT IS CLEARED
101     0006      POSTIV    EQU      6      USED TO DISPLAY NEGATIVE SIGN...CLEARED TO SHOW
102     ***                                          MINUS SIGN.
103     0004      BLANK     EQU      4      TO BLANK DIGITS 2 AND 3...CLEAR BLANK.
104     ***                                          DIGITS 4 AND 5 ARE ALWAYS BLANKED.
105     ***                                          DIGIT 1 IS NEVER BLANKED.
106     ***
107     ***      PORT C (I/O)
108     ***
109     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
110     ***      |          BCD DIGIT #2          | BCD DIGIT #1(LEAST SIGNIFICANT) |
111     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
112     ***      | D2 | C2 | B2 | A2 | D1 | C1 | B1 | A1 |
113     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
114     *** BIT      7          6          5          4          3          2          1          0
115     ***
116     ***
117     ***      PORT D (INPUT ONLY)
118     ***
119     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
120     ***      | CH_A | INT2 | CH_B | FUNCT | SET |          |          |          |
121     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
122     *** BIT      7          6          5          4          3          2          1          0
123     ***
124     0007      CH_A      EQU      7      INDICATES THE STATUS OF CHANNEL A.
125     0006      INT2      EQU      6      INTERRUPT #2. USED TO CHANGE DISPLAY MODES.
126     0005      CH_B      EQU      5      INDICATES THE STATUS OF CHANNEL B.
127     0004      FUNCT     EQU      4      USED TO PUT THE PROGRAM IN A MODE THAT WILL ALLOW

```



```

128      ***      'HYST' TO BE INCREMENTED.
129      0003      SET      EQU      3      INCREMENTS 'HYST' WHEN TOGGLED AND FUNCT IS LOW.
130      ***
131      ***
132      *****
133      **
134      **
135      **      RAM VARIABLES
136      *****
137      **
138      ** RESERVE MEMORY SPACE FOR THE PROGRAM VARIABLES.
139      **
140      0000      DATA
141      **
142      **
143      0000      ABSOLUTE (ABSOLUTE ADDRESSING USED HERE TO RELATIVE DIRECTIVE)
144      **
145      0010      ORG      RAM      START OF RAM.
146      **
147      *** BINARY COUNT.
148      0010      BINCT RMB      3
149      0010      HIBIN EQU      BINCT HI BYTE.
150      0011      MIDBIN EQU      BINCT+1 MIDDLE BYTE.
151      0012      LOBIN EQU      BINCT+2 LO BYTE.
152      **
153      *** POSITION POINTERS.
154      0013      PTR      RMB      4      EACH BYTE POINTS TO A POSITION IN THE
155      **      TABLE THAT CONTAINS ONE OR TWO DIGITS
156      **      OF THE BCD POSITION.
157      0013      PTR4 EQU      PTR      MOST SIGNIFICANT DIGITS.
158      0014      PTR3 EQU      PTR+1
159      0015      PTR2 EQU      PTR+2
160      0016      PTR1 EQU      PTR+3 LEAST SIGNIFICANT DIGIT.
161      **
162      *** COUNT POINTERS.
163      0017      CTPTR RMB      3      EACH BYTE POINTS TO A POSITION IN THE
164      **      TABLE THAT CONTAINS TWO OF THE DIGITS
165      **      IN THE BCD COUNT.
166      0017      CTPTR3 EQU      CTPTR      MOST SIGNIFICANT DIGITS.
167      0018      CTPTR2 EQU      CTPTR+1
168      0019      CTPTR1 EQU      CTPTR+2 LEAST SIGNIFICANT DIGITS.
169      **
170      *** BCD POSITION IN DEGREES.
171      001A      DEGRES RMB      4
172      001A      HUNDEG EQU      DEGRES      CONTENTS X 100.000
173      001B      ONEDEG EQU      DEGRES+1      CONTENTS X 1.000
174      001C      HUNDTH EQU      DEGRES+2      CONTENTS X 0.010
175      001D      THOUTH EQU      DEGRES+3      + CONTENTS X 0.001
176      ***
177      ***      POSITION IN DEGREES
178      **
179      *** BCD COUNT.
180      001E      BCDCT RMB      3
181      001E      TENTHO EQU      BCDCT      CONTENTS X 10,000
182      001F      HUNDRD EQU      BCDCT+1      CONTENTS X 100
183      0020      TENONE EQU      BCDCT+2      + CONTENTS X 1
184      ***
185      ***      NUMBER OF PULSES COUNTED
186      ***
187      *** HYSTERESIS COUNTER. POINTS TO A NUMBER IN THE TABLE THAT IS THE
188      *** AMOUNT OF HYSTERESIS PRESENT IN THE SYSTEM. INITIALIZED TO 7.
189      0021      HYSTPT RMB      1
190      **
191      *** POSITION INCREMENT. CONTAINS A NUMBER, THAT WHEN MULTIPLIED BY 0.001
192      *** IS THE NUMBER OF DEGREES THAT THE POSITION COUNTER (BCDPOS) IS
193      *** TO BE INCREMENTED OR DECREMENTED DURING PROGRAM EXECUTION.

```

```

194      *** THE VALUE OF 'POSINC', DETERMINED EXPERIMENTALLY, SHOULD BE
195      *** 7.0312. SINCE THE PROGRAM IS DESIGNED WORK WITH INTEGERS ONLY
196      *** THIS NUMBER IS ROUNDED TO 7. TO REDUCE THE CUMULATIVE EFFECT OF
197      *** THE ROUND OFF, EVERY 32 COUNTS 'POSINC' IS SET EQUAL TO 8. THIS
198      *** AGAIN LEADS TO SOME CUMULATIVE ERROR THAT IS ACCOUNTED FOR BY
199      *** SETTING 'POSINC' TO 7 INSTEAD OF 8 WHEN THE COUNT REACHES A
200      *** VALUE OF 16384 (2^14).
201      ***
202 0022      POSINC RMB 1
203      ***
204      *** HYSTERESIS VARIABLES. USED TO ELIMINATE THE EFFECTS OF BACKLASH ON
205      *** THE POSITION MEASUREMENTS.
206      ***
207 0023      HYST RMB 1 THE THRESHHOLD VALUE DETERMINED
208      *** EXPERIMENTALLY.
209 0024      HYSTCT RMB 1 CURRENT AMOUNT OF HYSTERESIS MEASURED.
210      ***
211      *** STATUS BYTE. USED TO KEEP TRACK OF WHAT IS GOING ON.
212      ***
213 0025      STAT RMB 1 CURRENT STATUS.
214 0026      LSTAT RMB 1 PREVIOUS/LAST STATUS. USED TO KEEP TRACK OF
215      *** L_SET ONLY.
216      ***
217      *** TIMER COUNTER. USED IN CONJUNCTION WITH THE TIMER PRESCALER AND THE
218      *** TDR TO KEEP TRACK OF ONE SEC. INTERVALS. USED IN BLINKING THE
219      *** DISPLAY. INITIALLY SET TO 31, WHEN THE 'FLASH' BIT OF 'STAT'
220      *** IS SET. TIMCT IS DECREMENTED EACH CLOCK INTERRUPT (APPROX. 31
221      *** TIMES PER SEC). RESET TO 31 WHEN CONTENTS GO TO ZERO.
222      *** WHEN (TIMCT)=0 THE DISPLAY WILL TOGGLE.
223      ***
224 0027      TIMCT RMB 1
225      **
226      ENDS
227      **
228      ***
229      *****
230      **
231      ** PAGE ZERO ROM
232      **
233      *****
234      **
235      ** INITIALIZATION ROUTINE.
236      **
237      **
238 0000      ** CODE
239      **
240 0080      ** ORG ZROM PAGE ZERO ROM.
241      **
242 0080      ** RELATIVE RELATIVE ADDRESSING MUST BE USED FOR THE BRANCH.
243      **
244 0080      RESTRT EQU $ THIS IS THE ENTRY POINT WHEN THE RESET
245      *** SWITCH IS PUSHED.
246      **
247      *****
248      **
249      *** INITIALIZE THE PC AND CLEAR RAM.
250      ***
251      ***
252 0080 9B SEI SET INTERRUPT TO AVOID INTERRUPTION AND
253 0081 9C RSP RESET THE STACK POINTER. JUST IN CASE!
254      ***
255 0082 AE 10 LDX #BINCT CLEAR ALL OF THE VARIABLES BETWEEN
256 0084 7F CLR ,X 'BINCT' AND 'TIMCT' (INCLUSIVE).NOTE
257 0085 5C INCX THAT THIS SETS THE COUNTER AND THE POS-
258 0086 A3 27 CPX #TIMCT ITION TO ZERO. THIS MEANS THAT ROTATION
259 0088 23 FA BLS CLRIT SHOULD START IN AN INCREASING (CW)

```

```

260                                     ***          DIRECTION FROM THE MOST CCW POSITION
261                                     ***          AFTER A RESET.
262                                     ***
263      008A      ABSOLUTE          BACK TO ABSOLUTE ADDRESSING.
264                                     ***
265      *****
266                                     ***
267                                     ***          ESTABLISH I/O PORTS.
268                                     ***
269      008A      A6 FF          LDA      #-1          PORTS A,B,C ARE CONFIGURED AS
270      008C      B7 04          STA      PORTA+DDR     ALL OUTPUT. PORT D IS ALL INPUT
271      008E      B7 05          STA      PORTB+DDR     SO THERE IS NO MASK TO SET.
272      0090      B7 06          STA      PORTC+DDR
273                                     ***
274                                     ***
275      0092      CD 03 4E      JSR      OUTCT          COUNT IS TO BE DISPLAYED INITIALLY.
276                                     ***
277      *****
278                                     ***          SET UP THE STATUS REGISTER.
279                                     ***
280      0095      A6 08          LDA      #%00001000    --
281      0097      B4 03          AND      PORTD          |--> SET UP 'L_SET' BIT OF 'STAT'.
282      0099      B7 25          STA      STAT          --
283                                     ***
284      009B      1C 25          BSET     MOD_32,STAT    0 IS MODULO 32.
285                                     **
286      *****
287                                     ***
288                                     ***          INITIALIZE HYSTCT.
289                                     ***
290      009D      A6 08          LDA      #08
291      009F      B7 23          STA      HYST
292      00A1      B7 21          STA      HYSTPT
293                                     ***
294      *****
295      **
296          SET UP THE TIMER FOR A 4 MHZ CRYSTAL / 4 = 1 MHZ CLOCK.
297      ***
298      NOTE: THE MASK OPTION REGISTER IS IN ROM. IT IS SET UP AT
299      THE END OF THE PROGRAM.
300      ***
301      *****          SET UP THE TCR.          *****
302      ***
303      00A3      A6 47          LDA      #BIT6+BIT2+BIT1+BIT0
304                                     (TIM)|(PS2)(PS1)(PS0)
305      ***          (DISABLE INTERRUPT)|(PRESCALE BY 128)
306      ***
307      00A5      B7 09          STA      TCR
308                                     ***
309                                     ***
310      ***          SET UP THE TIMER.
311      ***
312      00A7      A6 FF          LDA      #255          1 MHZ/(128*255) = 30.6 (APPROX. 31)
313      00A9      B7 08          STA      TIMER
314                                     ***
315      *****          INITIALIZE THE TIMER COUNTER.          *****
316      ***
317      00AB      A6 1F          LDA      #31          PROVIDES FOR 1 SEC. BLINK INTERVAL.
318      00AD      B7 27          STA      TIMCT        FOR 2 SEC. INTERVAL JUST USE TIMECT=62, etc.
319                                     ***
320                                     ***
321      *****
322      **
323          SET UP MISCELLANEOUS REGISTER.
324      **
325      00AF      1D 0A          BCLR     B6,MR          ENABLES THE SECOND INTERRUPT.

```

```

326
327
328 00B1 9A          CLI          CLEAR THE INTERRUPT MASK TO GET STARTED.
329
330 00B2             RELATIVE      RELATIVE ADDRESSING MUST BE USED FOR THE
331                               REMAINDER OF THE PROGRAM.
332
333 *****
334 **
335 ** WAIT LOOP.  EXECUTES, UNTIL AN INTERRUPT OCCURS.
336 **
337 00B2 09 03 0B    PAUSE  BRCLR  FUNCT,PORTD,CHHYST  WANT TO CHANGE HYST?
338 **                               YES...GO TO CHHYST.
339 00B5 06 03 04    BRSET  SET,PORTD,SBIT  NO... 'SET,PORTD' SET?
340 00B8 17 25       BCLR   L_SET,STAT      NO...CLEAR 'L_SET,STAT'
341 00BA 20 F6       BRA     PAUSE           AND LOOP.
342 00BC 16 25       SBIT   BSET  L_SET,STAT  YES...SET 'L_SET,STAT'
343 00BE 20 F2       BRA     PAUSE           AND...LOOP
344 **
345 *****
346 **
347 ** HYSTERESIS MODIFICATION ROUTINE.  PERMITS MODIFICATION OF THE
348 ** HYSTERESIS BUFFER WITHOUT REPROGRAMMING.
349 **
350 00C0 A6 40       CHHYST LDA    #BIT6      DISABLE TIMER INTERRUPT.
351 00C2 B7 09       STA    TCR
352
353             LDA    #%00001000      SAVE 'L_SET'
354             AND    STAT             INTO
355             STA    LSTAT            'LSTAT'.
356             LDA    #%00001000
357             AND    PORTD            'SET,PORTD' --> ACCUMULATOR
358             CMP    LSTAT            HAS THE SET SWITCH BEEN CHANGED?
359             BEQ    DISPLA
360
361             LDA    #%00001000      YES...
362             EOR    STAT             --
363             STA    STAT             |-->CHANGE 'L_SET,STAT',
364             INC    HYST             --
365             INC    HYSTPT           THEN INCREMENT THE HYSTERESIS
366                                     POINTER AND 'HYST'...
367             LDA    HYSTPT           --
368             CMP    #25              --
369             BLS    DISPLA           --
370
371             CLRA                    -- BUT NOT ABOVE 25.
372             STA    HYST             -- THEN-->
373             STA    HYSTPT           --
374
375             DISPLA LDA    #%00000000  NO... JUST----->
376             STA    PORTA             --
377             LDA    #%11000000        --
378             STA    PORTB             --
379
380             LDX    HYSTPT           --
381             LDA    TABLE,X          --
382             STA    PORTC             --
383
384             BRCLR  FUNCT,PORTD,CHHYST  IS 'HYST' SETTING COMPLETE?
385             BRSET  POSCT,STAT,SHOPOS  NO... KEEP CHECKING 'SET'.
386             JSR    OUTCT              YES... RESET THE DISPLAY.
387             BRA    DUNCHG
388
389 0101 CD 03 68    SHOPOS JSR    OUTPOS
390
391 0104 0B 25 04    DUNCHG BRCLR  FLASH,STAT,NO_INT  IF THE DISPLAY IS TO BLINK...

```


392	0107	A6 07	LDA	#BIT2+BIT1+BIT0	ENABLE TIMER INTERRUPT AND RESET
393	0109	B7 09	STA	TCR	TIMER PRESCALER
394	010B	20 A5	NO_INT BRA	PAUSE	PRIOR TO RETURNING.
395			***		
396			**		
397			*****		
398			**	MAXIMUM EXECUTION TIME FOR THE REMAINDER OF THE PROGRAM OCCURS	
399			**	IF THE COUNTER ROTATES THROUGH ZERO AS THE DISPLAY MODE IS CHANGED	
400			**	FROM THE BLINKING MODE TO THE COUNT MODE AT THE SAME TIME THAT THE	
401			**	BLINKING ROUTINE IS CAUSING THE DISPLAY TO TOGGLE TO SHOW THE	
402			**	POSITION IN DEGREES.	
403			**	MAXIMUM EXECUTION TIME = 140 + 184 + 708 = 1032 CLOCK CYCLES.	
404			*****		
405			**		
406			**	MODE CHANGE ROUTINE. CHANGES THE DISPLAY MODE FROM	
407			**	COUNT -> POSITION -> BLINKING -> COUNT ->....(ETC.)	
408			**	MAXIMUM EXECUTION TIME OF 181 CLOCK CYCLES OCCURS WHEN THE	
409			**	DISPLAY MODE IS CHANGED FROM DISPLAYING THE COUNT TO DISPLAYING	
410			**	THE POSITION (IN DEGREES).	
411			**	IF THE DISPLAY IS CHANGED FROM BLINKING TO A COUNT DISPLAY	
412			**	EXECUTION TIME IS 140 CLOCK CYCLES.	
413			**		
414	010D	1F 0A	CHMODE BCLR	B7,MR	AVOID REPEATED INTERRUPTS.
415			**		
416	010F	0A 25 10	BRSET	FLASH,STAT,DIS_CT	IF FLASHING, DISPLAY COUNT...
417	0112	09 25 07	BRCLR	POSCT,STAT,DISPOS	IF SHOWING COUNT, DISPLAY POSITION...
418	0115	1A 25	BSET	FLASH,STAT	ELSE, BLINK.
419			**		
420	0117	A6 07	LDA	#BIT2+BIT1+BIT0	ENABLE TIMER INTERRUPT AND RESET
421	0119	B7 09	STA	TCR	TIMER PRESCALER.
422	011B	80	RTI		
423			**		
424	011C	18 25	DISPOS BSET	POSCT,STAT	--
425	011E	CD 03 68	JSR	OUTPOS	-- DISPLAY CURRENT POSITION, AND WAIT.
426	0121	80	RTI		--
427			**		
428	0122	A6 47	DIS_CT LDA	#BIT6+BIT2+BIT1+BIT0	DISABLE TIMER INTERRUPT AND RESET
429	0124	B7 09	STA	TCR	TIMER PRESCALER.
430	0126	19 25	BCLR	POSCT,STAT	--
431	0128	1B 25	BCLR	FLASH,STAT	
432			**		-- DISPLAY CURRENT COUNT, AND WAIT.
433	012A	CD 03 4E	JSR	OUTCT	
434	012D	80	RTI		--
435			**		
436			*****		
437			**		
438			**	BLINK ROUTINE. INTERRUPT ROUTINE TO CHANGE THE DISPLAY FROM POSITION	
439			**	TO COUNT OR VICE VERSA EVERY 31 ST TIMER INTERRUPT IF THE	
440			**	'FLASH' BIT OF 'STAT' IS SET.	
441			**	MAXIMUM EXECUTION TIME OF 184 CLOCK CYCLES OCCURS WHEN THE	
442			**	DISPLAY IS TOGGLED FROM A COUNT DISPLAY TO A POSITION DISPLAY.	
443			**		
444		012E	BLINK EQU	\$	
445	012E	0F 09 DC	BRCLR	TIR,TCR,CHMODE	IF THE INTERRUPT WAS NOT A TIMER
446			**		INTERRUPT IT MUST BE FROM INT2.
447			**		
448	0131	1F 09	BCLR	TIR,TCR	AVOID REPEATED TIMER INTERRUPTS.
449			**		
450	0133	3A 27	DEC	TIMCT	IF THERE HAVE BEEN 31 TIMER
451	0135	27 01	BEQ	CHGDIS	INTERRUPTS (1 SEC), IT'S TIME TO
452			**		CHANGE THE DISPLAY.
453	0137	80	RTI		OTHERWISE, IT'S BACK TO WORK.
454			**		
455	0138	A6 1F	CHGDIS LDA	#31	RESET TIMCT TO 31 (1 SEC. INTERVAL).
456	013A	B7 27	STA	TIMCT	
457			**		


```

458 013C B6 25 LDA STAT --
459 013E A8 10 EOR #%00010000 |-- CHANGE 'POSCT' BIT OF 'STAT'.
460 0140 B7 25 STA STAT --
461
462 0142 08 25 04 BRSET POSCT,STAT,POSOUT DECIDE ON CORRECT DISPLAY.
463
464 ***** CHANGE THE DISPLAY TO SHOW THE COUNT..... *****
465
466 0145 CD 03 4E JSR OUTCT
467 0148 80 RTI
468
469 ***** OR HAVE THE DISPLAY SHOW THE POSITION. *****
470
471 0149 CD 03 68 POSOUT JSR OUTPOS
472 014C 80 RTI
473
474 *****
475
476 COUNT ROUTINE.
477
478 WHEN A COUNT IS RECEIVED THIS IS THE ENTRY POINT .
479 MAXIMUM EXECUTION TIME OF 708 CLOCK CYCLES OCCURS WHEN THE
480 COUNTER ROTATES CCW THROUGH ZERO AND THE POSITION (IN DEGREES)
481 IS BEING DISPLAYED.
482
483
484 ** CURRENT DIRECTION OF ROTATION IS DETERMINED BY INSPECTING THE STATUS
485 ** OF 'CH_A' AND 'CH_B'. THE FOUR POSSIBILITIES AND THE ASSOCIATED
486 ** DIRECTION OF ROTATION ARE AS SHOWN BELOW. NOTE THAT THIS SCHEME
487 ** PREVENTS MULTIPLE OSCILLATIONS ABOUT A SINGLE POINT FROM
488 ** REPEATEDLY INCREMENTING OR DECREMENTING THE COUNTER.
489
490
491 +-----+-----+-----+-----+
492 | CH_A | CH_B | DIRECTION | COUNT THE PULSE? |
493 |-----|-----|-----|-----|
494 | LO | LO | CW | NO |
495 | LO | HI | CCW | YES |
496 | HI | LO | CCW | NO |
497 | HI | HI | CW | YES |
498 +-----+-----+-----+-----+
499
500 ***** FIRST SEE IF WE ARE SUPPOSED TO COUNT THIS INTERRUPT. *****
501
502 014D 0A 03 01 COUNT EQU $
503 0150 80 BRSET CH_B,PORTD,OKCT IF CH_B IS LO WE DON'T COUNT THE
504 RTI INTERRUPT.
505
506 ***** IF THE INTERRUPT IS VALID UPDATE 'STAT'. *****
507
508 0151 A6 7F OKCT LDA #%01111111
509 0153 B4 25 AND STAT
510 0155 B7 25 STA STAT
511 0157 A6 80 LDA #%10000000
512 0159 B4 03 AND PORTD
513
514 015B BA 25 ORA STAT
515 015D B7 25 STA STAT
516
517
518 015F 0E 25 09 BRSET UD,STAT,HYSTCK IF ROTATING CW SEE BELOW.
519 0162 B6 24 LDA HYSTCT ELSE, SEE IF WE DECREMENT THIS TIME.
520 0164 27 60 BEQ CCW IF HYSTCT=0, GO TO THE COUNT DOWN
521
522 0166 A0 01 SUB #1 ROUTINE.
523 0168 B7 24 STA HYSTCT ELSE, DECREMENT THE HYSTERESIS COUNTER,

```

```

524 016A 80          RTI          AND WAIT FOR THE NEXT INTERRUPT.
525
526 016B B6 23      HYSTCK LDA    HYST          IF ROTATING CW....
527 016D B1 24      CMP     HYSTCT        AND HYST = HYSTCT ....
528 016F 27 03      BEQ     CW           COUNT THE PULSE .
529 0171 3C 24      INC     HYSTCT        ELSE, INCREMENT THE HYSTERESIS COUNTER,
530 0173 80          RTI          AND WAIT FOR ANOTHER PULSE.
531
532
533 *****
534
535
536
537          0174      CW      EQU      $
538
539
540 ***** INCREMENT THE BINARY COUNTER (BINCT). *****
541
542 0174 B6 12          LDA    LOBIN      BEGIN AT THE LSB OF THE BINARY COUNTER.
543 0176 AB 01          ADD     #1        LOBIN = LOBIN + 1 ; CARRY -> C,CCR
544 0178 B7 12          STA    LOBIN
545
546 017A B6 11          LDA    MIDBIN
547 017C A9 00          ADC     #0        ADD THE CARRY TO THE MIDDLE BYTE.
548 017E B7 11          STA    MIDBIN
549
550 0180 B6 10          LDA    HIBIN
551 0182 A9 00          ADC     #0        ADD THE CARRY TO THE HIGH BYTE.
552 0184 B7 10          STA    HIBIN
553
554
555 ***** CLR/SET MOD_32 APPROPRIATELY. *****
556
557
558 THE FOLLOWING SEVERAL LINES OF CODE ARE PRETTY MESSY. ALL THAT
559 IS BEING DONE IS TO ENSURE THAT THE SCALE FACTOR IS SET PROPERLY.
560 FOR THE PAN AXIS THE SCALE FACTOR IS;
561
562          1 PULSE => 0.007097 DEGREES
563
564 0186 B6 12          LDA    LOBIN      IF THE LOW FIVE BITS OF 'LOBIN' ARE NOT
565 0188 A4 1F          AND     #%00011111 ZERO THEN THE NUMBER ISN'T A MODULO 32 NUMBER.
566 018A 26 0F          BNE     NOT_32
567 018C B6 11          LDA    MIDBIN      IF THE LOW SIX BITS OF 'MIDBIN' ARE ZERO
568 018E 27 07          BEQ     MOD        AND 'HIBIN' .NE. ZERO
569 0190 A4 3F          AND     #%00111111 THEN THE NUMBER IS MODULO 16,384, AND WE
570 0192 26 03          BNE     MOD        DON'T WANT TO SET 'MOD_32,STAT', UNLESS
571 0194 0D 11 04      BRCLR   B6,MIDBIN,NOT_32 THE NUMBER IS ALSO MODULO 32,768.
572
573 0197 1C 25      MOD    BSET     MOD_32,STAT
574 0199 20 02      BRA     DIRCHK
575
576 019B 1D 25      NOT_32 BCLR     MOD_32,STAT
577
578 019D B6 10      DIRCHK LDA    HIBIN
579 019F 2B 1D      BMI     CWNEG          IF HIBIN < 0 , WE'RE ROTATING CCW TOWARD
580
581
582          BNE     CWPOS          ELSE IF BINCT .NE. 0
583 01A3 B6 11      LDA    MIDBIN        WE'RE ROTATING CW
584 01A5 26 10      BNE     CWPOS        AWAY FROM THE ORIGIN.
585 01A7 B6 12      LDA    LOBIN
586 01A9 26 0C      BNE     CWPOS
587
588
589 01AB 15 25      BCLR     NEGTV,STAT    ELSE, WE'VE ROTATED CW THROUGH THE ORIGIN.
                                           CLR NEGATIVE SIGN.

```

```

590 01AD AE 13          LDX  #PTR4  --
591 01AF 7F          CLRIT2 CLR  ,X    --
592 01B0 5C          INCX             --RESET ALL COUNTERS AND DEGRES TO ZERO.
593 01B1 A3 1D          CPX  #THOUTH --
594 01B3 23 FA          BLS  CLRIT2 --
595 01B5 20 68          BRA  UPOUT    UPDATE OUTPUT.
596
597 01B7 AD 74          CWPOS BSR  ADDBCD
598 01B9 CD 02 6A        JSR  INCPOS
599 01BC 20 64          BRA  UPOUT
600
601 01BE CD 02 CA        CWNEG JSR  SUBBCD
602 01C1 CD 02 6A        JSR  INCPOS
603 01C4 20 5C          BRA  UPOUT
604
605
606
607
608
609
610          01C6        CCW  EQU  $
611
612
613 ***** CLR/SET MOD_32 APPROPRIATELY. *****
614
615          AGAIN SET THE SCALE FACTOR TO;
616
617          1 PULSE => 0.007097 DEGREES
618
619 01C6 B6 12          LDA  LOBIN      IF THE LOW FIVE BITS OF 'LOBIN' ARE NOT
620 01C8 A4 1F          AND  #%00011111 ZERO THEN THE NUMBER ISN'T A MODULO 32 NUMBER.
621 01CA 26 0F          BNE  NO_32
622 01CC B6 11          LDA  MIDBIN     IF THE LOW SIX BITS OF 'MIDBIN' ARE ZERO
623 01CE 27 07          BEQ  MODLO      AND 'HIBIN' .NE. ZERO
624 01D0 A4 3F          AND  #%00111111 THEN THE NUMBER IS MODULO 16,384, AND WE
625 01D2 26 03          BNE  MODLO      DON'T WANT TO SET 'MOD_32,STAT', UNLESS
626 01D4 0D 11 04        BRCLR B6,MIDBIN,NO_32 THE NUMBER IS ALSO MODULO 32,768.
627
628 01D7 1C 25          MODLO BSET  MOD_32,STAT
629 01D9 20 02          BRA  DECBIN
630
631 01DB 1D 25          NO_32 BCLR  MOD_32,STAT
632
633
634 ***** DECREMENT THE BINARY COUNTER (BINCT). *****
635
636 01DD B6 12          DECBIN LDA  LOBIN  BEGIN AT THE LSB OF THE BINARY COUNTER.
637 01DF A0 01          SUB  #1          LOBIN = LOBIN - 1 ; BORROW -> C,CCR
638 01E1 B7 12          STA  LOBIN
639
640 01E3 B6 11          LDA  MIDBIN
641 01E5 A2 00          SBC  #0          SUBTRACT THE CARRY FROM THE MIDDLE BYTE.
642 01E7 B7 11          STA  MIDBIN
643
644 01E9 B6 10          LDA  HIBIN
645 01EB A2 00          SBC  #0          SUBTRACT THE CARRY FROM THE HIGH BYTE.
646 01ED B7 10          STA  HIBIN
647
648 01EF B6 10          LDA  HIBIN
649 01F1 2A 29          BPL  CCWPOS     IF HIBIN .GE. 0 , WE'RE ROTATING CCW TOWARD
650
651          LDA  # -1  --
652 01F5 B1 10          CMP  HIBIN      --
653 01F7 26 1C          BNE  CCWNEG     -- ELSE IF BINCT .NE. -1 ,
654 01F9 B1 11          CMP  MIDBIN     -- WE'RE ROTATING CCW AWAY
655 01FB 26 18          BNE  CCWNEG     -- FROM THE ORIGIN.

```

```

656 01FD B1 12          CMP     LOBIN    --
657 01FF 26 14          BNE     CCWNEG   --
658                                     ***
659 0201 14 25          BSET     NEGTV,STAT  ELSE, WE'VE GONE THROUGH ORIGIN IN CCW
660                                     ***      DIRECTION. SET NEGATIVE SIGN.
661                                     ***      AND SET ALL COUNTERS APPROPRIATELY.
662 0203 A6 03          LDA     #03      --
663 0205 B7 13          STA     PTR4     --
664 0207 B7 1A          STA     HUNDEG   -- DEGES = 360.00
665 0209 A6 3C          LDA     #60     --
666 020B B7 14          STA     PTR3     --
667 020D AE 15          LDX     #PTR2    --
668 020F 7F             CLREM    CLR     ,X      --
669 0210 5C             INCX     --          -- EVERYTHING ELSE IS ZERO BEFORE CHANGE.
670 0211 A3 19          CPX     #CTPTR1  --
671 0213 23 FA          BLS     CLREM    --
672                                     ***
673 0215 AD 16          CCWNEG  BSR     ADDBCD
674 0217 CD 02 FD       JSR     DECPOS
675 021A 20 06          BRA     UPOUT
676                                     ***
677 021C CD 02 CA       CCWPOS  JSR     SUBBCD
678 021F CD 02 FD       JSR     DECPOS
679                                     ***
680                                     ***
681                                     **
682 *****
683 **
684 ** OUTPUT ROUTINE. ROUTINE TO PRINT DATA TO THE OUTPUT PORTS. BY
685 ** CALLING THE APPROPRIATE SUBROUTINE.('OUTCT' TO OUTPUT THE
686 ** THE COUNT AND 'OUTPOS' TO OUTPUT THE POSITION).
687 **
688 0222          UPOUT EQU     $
689 **
690 0222 09 25 04          BRCLR   POSCT,STAT,PUTCT
691 **
692 0225 CD 03 68          JSR     OUTPOS
693 0228 80               RTI
694 **
695 0229 CD 03 4E          PUTCT  JSR     OUTCT
696 022C 80               RTI
697 **
698 *****
699 ***** SUBROUTINE TO INCREMENT THE BCD COUNTER (BCDCT). *****
700 *****
701 022D B6 19          ADDBCD  LDA     CTPTR1
702 022F AB 01          ADD     #1
703 0231 A1 63          CMP     #99      CTPTR > 99 ?
704 0233 23 05          BLS     OK1      NO, WE'RE OK HERE. LOOK UP THE FIRST TWO DIGITS.
705 0235 A0 64          SUB     #100     YES... MODIFY THE CTPTR,
706 0237 99             SEC             SET THE CARRY, AND
707 0238 20 01          BRA     OK1A     USE TABLE LOOK UP.
708                                     ***
709 023A 98             OK1      CLC             NO CARRY EXISTS IF WE ENTER AT THIS POINT.
710 023B B7 19          OK1A     STA     CTPTR1  --
711 023D 97             TAX             --
712                                     ***      -- LOOK UP THE TWO LEAST SIGNIFICANT DIGITS.
713 023E D6 03 BE       LDA     TABLE,X  --
714 0241 B7 20          STA     TENONE  --
715 0243 24 24          BCC     NOMO      AND CONTINUE ONLY IF THERE WAS A CARRY.
716                                     ***
717                                     ***
718 0245 B6 18          LDA     CTPTR2
719 0247 A9 00          ADC     #0        ADD THE CARRY.
720 0249 A1 63          CMP     #99      CTPTR > 99 ?
721 024B 23 05          BLS     OK2      NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.

```



```

722 024D A0 64 SUB #100 YES... MODIFY THE CTPTR,
723 024F 99 SEC SET THE CARRY, AND
724 0250 20 01 BRA OK2A USE TABLE LOOK UP.
725 ***
726 0252 98 OK2 CLC NO CARRY EXISTS IF WE ENTER AT THIS POINT.
727 0253 87 18 OK2A STA CTPTR2 --
728 0255 97 TAX --
729 *** -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
730 0256 D6 03 BE LDA TABLE,X --
731 0259 87 1F STA HUNDRD --
732 0258 24 0C BCC NOMO AND CONTINUE ONLY IF THERE WAS A CARRY.
733 ***
734 025D B6 17 LDA CTPTR3
735 025F A9 00 ADC #0 ADD THE CARRY.
736 0261 87 17 STA CTPTR3 --
737 0263 97 TAX --
738 *** -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
739 0264 D6 03 BE LDA TABLE,X --
740 0267 87 1E STA TENTHO --
741 ***
742 0269 81 NOMO RTS
743 ***
744 *****
745 ***** SUBROUTINE TO INCREMENT THE POSITION COUNTER (DEGRES). *****
746 ***
747 ***** FIRST CHECK TO SEE IF THE BINARY COUNTER HAS REACHED A MODULO 32
748 ***** NUMBER.
749 *****
750 026A 0D 25 04 INCPOS BRCLR MOD_32,STAT,INC7 'MOD_32,STAT' SET ?
751 *****
752 026D A6 08 LDA #8 YES ...
753 026F 20 02 BRA INC INCREMENT THE POSITION BY 0.008 DEGREES.
754 *****
755 0271 A6 07 INC7 LDA #7 NO ....
756 0273 87 22 INC STA POSINC INCREMENT THE POSITION BY 0.007 DEGREES.
757 *****
758 ***** ROUTINE TO INCREMENT THE POSITION COUNTER , 'DEGRES', BY A
759 ***** PREDETERMINED AMOUNT, 'POSINC'.
760 *****
761 0275 B6 16 LDA PTR1
762 0277 8B 22 ADD POSINC
763 0279 A1 09 CMP #9 PTR1 > 9 ?
764 027B 23 05 BLS OK3 NO, WE'RE OK HERE. LOOK UP THE FIRST DIGIT.
765 027D A0 0A SUB #10 YES... MODIFY THE CTPTR,
766 027F 99 SEC SET THE CARRY, AND
767 0280 20 01 BRA OK3A USE TABLE LOOK UP.
768 *****
769 0282 98 OK3 CLC NO CARRY EXISTS IF WE ENTER AT THIS POINT.
770 0283 87 16 OK3A STA PTR1 --
771 0285 97 TAX --
772 ***** -- LOOK UP THE LEAST SIGNIFICANT DIGIT.
773 0286 D6 03 BE LDA TABLE,X --
774 0289 87 1D STA THOUTH --
775 0288 24 3C BCC DONE AND CONTINUE ONLY IF THERE WAS A CARRY.
776 *****
777 *****
778 028D B6 15 LDA PTR2
779 028F A9 00 ADC #0 ADD THE CARRY.
780 0291 A1 63 CMP #99 PTR2 > 99 ?
781 0293 23 05 BLS OK4 NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.
782 0295 A0 64 SUB #100 YES...MODIFY THE CTPTR,
783 0297 99 SEC SET THE CARRY,
784 0298 20 01 BRA OK4A AND USE TABLE LOOK UP.
785 *****
786 029A 98 OK4 CLC NO CARRY EXISTS IF WE ENTER AT THIS POINT.
787 029B 87 15 OK4A STA PTR2 --

```



```

788 029D 97          TAX          --
789          *****          -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
790 029E D6 03 BE    LDA          TABLE,X  --
791 02A1 B7 1C        STA          HUNDTH  --
792 02A3 24 24        BCC          DONE          AND CONTINUE ONLY IF THERE WAS A CARRY.
793          *****
794          *****
795 02A5 B6 14        LDA          PTR3
796 02A7 A9 00        ADC          #0          ADD THE CARRY.
797 02A9 A1 63        CMP          #99        PTR3 > 99 ?
798 02AB 23 05        BLS          OK5        NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.
799 02AD A0 64        SUB          #100       YES... MODIFY THE CTPTR,
800 02AF 99           SEC          SET THE CARRY, AND
801 02B0 20 01        BRA          OK5A       USE TABLE LOOK UP.
802          *****
803 02B2 98           OK5         CLC          NO CARRY EXISTS IF WE ENTER AT THIS POINT.
804 02B3 B7 14        OK5A        STA          PTR3  --
805 02B5 97           TAX          --
806          *****          -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
807 02B6 D6 03 BE    LDA          TABLE,X  --
808 02B9 B7 18        STA          ONEDEG  --
809 02BB 24 0C        BCC          DONE          AND CONTINUE ONLY IF THERE WAS A CARRY.
810          *****
811 02BD B6 13        LDA          PTR4
812 02BF A9 00        ADC          #0          ADD THE CARRY.
813 02C1 B7 13        STA          PTR4  --
814 02C3 97           TAX          --
815          *****          -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
816 02C4 D6 03 BE    LDA          TABLE,X  --
817 02C7 B7 1A        STA          HUNDEG  --
818          *****
819 02C9 81           DONE         RTS
820          ***
821          **
822          *****
823          ***** SUBROUTINE TO DECREMENT THE BCD COUNTER (BCDCT). *****
824          ***
825 02CA B6 19        SUBBCD      LDA          CTPTR1
826 02CC A0 01        SUB          #1          CTPTR > 99 ?
827 02CE 24 03        BCC          OK6        NO, WE'RE OK HERE. LOOK UP THE FIRST TWO DIGITS.
828 02D0 AB 64        ADD          #100       YES, MODIFY THE CTPTR, AND
829 02D2 99           SEC          GENERATE A BORROW.
830          ***
831 02D3 B7 19        OK6         STA          CTPTR1  --
832 02D5 97           TAX          --
833          ***          -- LOOK UP THE TWO LEAST SIGNIFICANT DIGITS.
834 02D6 D6 03 BE    LDA          TABLE,X  --
835 02D9 B7 20        STA          TENONE  --
836 02DB 24 1F        BCC          COMPLT     AND CONTINUE ONLY IF THERE WAS A BORROW.
837          ***
838          ***
839 02DD B6 18        LDA          CTPTR2
840 02DF A2 00        SBC          #0          SUBTRACT THE CARRY. CTPTR > 99 ?
841 02E1 24 03        BCC          OK7        NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.
842 02E3 AB 64        ADD          #100       YES, MODIFY THE CTPTR, AND
843 02E5 99           SEC          GENERATE A BORROW.
844          ***
845 02E6 B7 18        OK7         STA          CTPTR2  --
846 02E8 97           TAX          --
847          ***          -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
848 02E9 D6 03 BE    LDA          TABLE,X  --
849 02EC B7 1F        STA          HUNDRD  --
850 02EE 24 0C        BCC          COMPLT     AND CONTINUE ONLY IF THERE WAS A CARRY.
851          ***
852 02F0 B6 17        LDA          CTPTR3
853 02F2 A2 00        SBC          #0          SUBTRACT THE BORROW.

```

```

854 02F4 B7 17          STA  CTPTR3  --
855 02F6 97            TAX              --
856                                     ***
857 02F7 D6 03 BE      LDA  TABLE,X  --
858 02FA B7 1E          STA  TENTHO  --
859                                     ***
860 02FC 81            COMPLT  RTS
861                                     ***
862                                     *****
863                                     ***** SUBROUTINE TO DECREMENT THE POSITION COUNTER (DEGRES). *****
864                                     ***
865                                     **** FIRST CHECK TO SEE IF THE BINARY COUNTER HAS REACHED A MODULO 32
866                                     **** NUMBER.
867                                     ****
868 02FD 00 25 04      DECPOS  BRCLR  MOD_32,STAT,DEC7      'MOD_32,STAT' SET ?
869                                     ****
870 0300 A6 08          LDA  #8              YES...
871 0302 20 02          BRA  DEC              DECREMENT THE POSITION BY 0.008 DEGREES.
872                                     ****
873 0304 A6 07          DEC7  LDA  #7              NO ....
874 0306 B7 22          DEC  STA  POSINC         DECREMENT THE POSITION BY 0.007 DEGREES.
875                                     ****
876                                     **** ROUTINE TO DECREMENT THE POSITION COUNTER , 'DEGREES', BY A
877                                     **** PREDETERMINED AMOUNT, 'POSINC'.
878                                     ****
879 0308 B6 16          LDA  PTR1
880 030A B0 22          SUB  POSINC  PTR1 < 0 ?
881 030C 24 03          BCC  OK8      NO, WE'RE OK HERE. LOOK UP THE FIRST DIGIT.
882 030E AB 0A          ADD  #10      YES, MODIFY THE CTPTR, AND
883 0310 99            SEC              GENERATE A BORROW.
884                                     ****
885 0311 B7 16          OK8  STA  PTR1  --
886 0313 97            TAX              --
887                                     ****
888 0314 D6 03 BE      LDA  TABLE,X  --
889 0317 B7 1D          STA  THOUTH  --
890 0319 24 32          BCC  DUNSUB      AND CONTINUE ONLY IF THERE WAS A BORROW.
891                                     ***
892                                     ***
893 031B B6 15          LDA  PTR2
894 031D A2 00          SBC  #0      SUBTRACT THE BORROW. PTR2 < 0 ?
895 031F 24 03          BCC  OK9      NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.
896 0321 AB 64          ADD  #100     YES, MODIFY THE CTPTR, AND
897 0323 99            SEC              GENERATE A BORROW.
898                                     ***
899 0324 B7 15          OK9  STA  PTR2  --
900 0326 97            TAX              --
901                                     ***
902 0327 D6 03 BE      LDA  TABLE,X  --
903 032A B7 1C          STA  HUNDTH  --
904 032C 24 1F          BCC  DUNSUB      AND CONTINUE ONLY IF THERE WAS A CARRY.
905                                     ***
906                                     ***
907 032E B6 14          LDA  PTR3
908 0330 A2 00          SBC  #0      SUBTRACT THE BORROW. PTR3 < 0 ?
909 0332 24 03          BCC  OK10     NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.
910 0334 AB 64          ADD  #100     YES, MODIFY THE CTPTR, AND
911 0336 99            SEC              GENERATE A BORROW.
912                                     ****
913 0337 B7 14          OK10 STA  PTR3  --
914 0339 97            TAX              --
915                                     ****
916 033A D6 03 BE      LDA  TABLE,X  --
917 033D B7 1B          STA  ONEDEG  --
918 033F 24 0C          BCC  DUNSUB      AND CONTINUE ONLY IF THERE WAS A CARRY.
919                                     ****

```

```

920 0341 B6 13          LDA    PTR4
921 0343 A2 00          SBC    #0      SUBTRACT THE BORROW.
922 0345 B7 13          STA    PTR4    --
923 0347 97             TAX          --
924                      ****      -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
925 0348 D6 03 BE       LDA    TABLE,X  --
926 034B B7 1A          STA    HUNDEG  --
927                      ****
928 034D 81             DUNSUB RTS
929                      ***
930                      **
931                      **
932                      *****
933                      **
934                      ** OUTPUT COUNT (OUTCT). SUBROUTINE TO MOVE THE CURRENT COUNT (BCDCT)
935                      ** TO THE OUTPUT PORTS. REMOVES THE DECIMAL POINT FROM THE
936                      ** DISPLAY AND BLANKS ALL BUT THE LEAST SIGNIFICANT DIGIT. ALSO
937                      ** SETS THE MINUS SIGN IF APPROPRIATE.
938                      **
939                      034E      OUTCT EQU    $
940                      **
941 034E B6 20          LDA    TENONE
942 0350 B7 02          STA    PORTC
943                      **
944 0352 B6 1F          LDA    HUNDRD
945 0354 B7 00          STA    PORTA
946                      **
947 0356 B6 1E          LDA    TENTHO
948 0358 B7 01          STA    PORTB
949                      **
950 035A 1E 01          BSET    DECPT,PORTB
951 035C 19 01          BCLR    BLANK,PORTB
952                      **
953 035E 04 25 04       BRSET    NEGTV,STAT,MINUS
954 0361 1C 01          BSET    POSTIV,PORTB
955 0363 20 02          BRA     ALLDUN
956                      **
957 0365 1D 01          MINUS BCLR    POSTIV,PORTB
958                      **
959 0367 81             ALLDUN RTS
960                      **
961                      **
962                      ** OUTPUT POSITION (OUTPOS). SUBROUTINE TO MOVE THE CURRENT POSITION
963                      ** COUNT (BCDCT) TO THE OUTPUT PORTS. THE DECIMAL POINT IS
964                      ** DISPLAYED , AND ONLY THE MOST SIGNIFICANT DIGIT IS BLANKED.
965                      **
966                      0368      OUTPOS EQU    $
967                      **
968 0368 B6 1D          LDA    THOUTH  --
969 036A A1 05          CMP    #5      --
970 036C 25 38          BLO    TRUNC   -- IF 5 > 'THOUTH' SIMPLY TRUNCATE THE
971 036E B6 1C          LDA    HUNDTH  -- DISPLAY. OTHERWISE...
972 0370 A4 09          AND    #9      -- IF THE LAST DIGIT ISN'T A NINE IT IS
973 0372 A1 09          CMP    #9      -- EASY TO ROUND UP. JUST ADD A ONE.
974 0374 26 28          BNE    DECIMAL --
975 0376 B6 1C          LDA    HUNDTH  -- BUT IF THE LAST DIGIT IS A NINE CHECK TO
976 0378 A1 99          CMP    #$99    -- SEE IF IT'S 99. IF SO IT GETS GRIM.
977 037A 27 04          BEQ    UGLY    --
978 037C AB 07          ADD    #7      -- IF THE NUMBER IS X9 AND X.NE. 9, THEN
979 037E 20 28          BRA     PCOUT   -- JUST ADD SEVEN TO ROUND UP. DUE TO
980                      **      -- HEXIDECIMAL.
981                      **      -- IF THE LOW TWO DIGITS ARE BOTH NINES
982 0380 A6 00          UGLY   LDA    #00  -- AND WE NEED TO ROUND UP....
983 0382 B7 02          STA    PORTC   -- MAKE THE LOW TWO DIGITS BOTH ZEROS
984 0384 99             SEC          -- AND SET THE CARRY.
985                      **

```

```

986 0385 B6 18 LDA ONEDEG -- CHECK THE LAST DIGIT AS BEFORE.
987 0387 A4 09 AND #9 -- IF USING THIS PORTION OF THE CODE
988 0389 A1 09 CMP #9 -- THERE HAD TO BE A CARRY.
989 0388 26 1E BNE NEXT -- IF THE LAST DIGIT IS NOT A NINE USE THE
990 038D B6 18 LDA ONEDEG -- ADC INSTRUCTION BELOW.
991 038F A1 99 CMP #999 -- IF IT IS A NINE, IS THE NEXT ONE A NINE
992 0391 27 04 BEQ RLUGLY -- ALSO?
993 0393 AB 07 ADD #7 -- IF NOT JUST ADD SEVEN,
994 0395 20 18 BRA PAOUT -- AND DISPLAY THE OUTPUT.
995
**
996 0397 A6 00 RLUGLY LDA #00 --
997 0399 B7 00 STA PORTA -- IF SO ROUND UP THE MOST SIGNIFICANT
998 0398 99 SEC -- DIGIT AND SET EVERYTHING ELSE TO ZERO.
999 039C 20 13 BRA NEXT1 --
1000
**
1001 039E B6 1C DECIMAL LDA HUNDTH --
1002 03A0 AB 01 ADD #1 --
1003
**
1004 03A2 B7 02 STA PORTC -- THIS IS ALL THAT NEEDS TO BE DONE IF
1005 03A4 20 05 BRA NEXT -- THE LAST DIGIT IS NOT A NINE.
1006
**
1007 03A6 B6 1C TRUNC LDA HUNDTH --
1008 03A8 B7 02 PCOUT STA PORTC -- AND IF THERE IS NO CARRY IT'S EVEN EASIER.
1009 03AA 98 CLC --
1010
**
1011 03AB B6 18 NEXT LDA ONEDEG
1012 03AD A9 00 ADC #0
1013 03AF B7 00 PAOUT STA PORTA
1014
**
1015 03B1 B6 1A NEXT1 LDA HUNDEG
1016 03B3 A9 00 ADC #0
1017 03B5 B7 01 STA PORTB
1018
**
1019 03B7 1C 01 BSET POSTIV,PORTB
1020 03B9 18 01 BSET BLANK,PORTB
1021 03BB 1F 01 BCLR DECP,PORTB
1022
**
1023 03BD 81 RTS
1024
**
1025
**
1026 *****
1027
**
1028 ** SET UP THE TABLE TO BE USED WITH BCD INCREMENT/DECREMENT ROUTINES.
1029
**
1030 * ENDS
1031 * DATA
1032 03BE 00 01 02 03 04 TABLE FCB $00,$01,$02,$03,$04,$05,$06,$07,$08,$09
03C3 05 06 07 08 09
1033 03C8 10 11 12 13 14 FCB $10,$11,$12,$13,$14,$15,$16,$17,$18,$19
03CD 15 16 17 18 19
1034 03D2 20 21 22 23 24 FCB $20,$21,$22,$23,$24,$25,$26,$27,$28,$29
03D7 25 26 27 28 29
1035 03DC 30 31 32 33 34 FCB $30,$31,$32,$33,$34,$35,$36,$37,$38,$39
03E1 35 36 37 38 39
1036 03E6 40 41 42 43 44 FCB $40,$41,$42,$43,$44,$45,$46,$47,$48,$49
03EB 45 46 47 48 49
1037 03F0 50 51 52 53 54 FCB $50,$51,$52,$53,$54,$55,$56,$57,$58,$59
03F5 55 56 57 58 59
1038 03FA 60 61 62 63 64 FCB $60,$61,$62,$63,$64,$65,$66,$67,$68,$69
03FF 65 66 67 68 69
1039 0404 70 71 72 73 74 FCB $70,$71,$72,$73,$74,$75,$76,$77,$78,$79
0409 75 76 77 78 79
1040 040E 80 81 82 83 84 FCB $80,$81,$82,$83,$84,$85,$86,$87,$88,$89
0413 85 86 87 88 89
1041 0418 90 91 92 93 94 FCB $90,$91,$92,$93,$94,$95,$96,$97,$98,$99
041D 95 96 97 98 99

```



```

1042      *      ENDS
1043      *      CODE
1044      ****
1045      **
1046      **          SET UP MASK OPTION REGISTER.
1047      **
1048      0422      ABSOLUTE
1049      **
1050      **
1051      0F38      ORG      MOR
1052      0F38      07      FCB      #BIT2+BIT1+BIT0
1053      **
1054      **      COMMENTS:
1055      **      BIT 7      CLOCK SOURCE 0 = CRYSTAL.
1056      **      BIT 6      TIMER OPTION 0 = INTERNAL.
1057      **      BIT 5      TIMER/CLOCK SOURCE 0 = INTERNAL.
1058      **      BIT 4      NOT USED.
1059      **      BIT 3      NOT USED.
1060      **      BIT 2      SET -
1061      **      BIT 1      SET -  PRESCALE SELECT 111 => 128
1062      **      BIT 0      SET -
1063      **
1064      **
1065      ****
1066      **
1067      **          ASSIGN INTERRUPT VECTORS.
1068      **
1069      0FF8      ORG      INTRPT
1070      **
1071      0FF8      012E      FDB      BLINK      TIMER/INT2 INTERRUPT VECTOR.
1072      0FFA      014D      FDB      COUNT      EXTERNAL INTERRUPT VECTOR.
1073      0FFC      014D      FDB      COUNT      SOFTWARE INTERRUPT VECTOR, NOT USED.
1074      0FFE      0080      FDB      RESTRT     RESET VECTOR.
1075      **
1076      **
1077      **
1078      ENDS
1079      1000      END

```

Lines Assembled : 1079

Assembly Errors : 0

C. TILT

```

1          TTL                                POSITION DETERMINING PROGRAM (ELEVATION)
2          *                                LATEST REVISION          9 MAY 89
3          *                                FILE NAME              TILT.ASM
4          **
5          ** PROGRAM DESCRIPTION
6          **
7          **
8          **
9          ** I/O REGISTER ADDRESSES
10         **
11         0000    PORTA    EQU    $0000    I/O PORT A
12         0001    PORTB    EQU    $0001    I/O PORT B
13         0002    PORTC    EQU    $0002    I/O PORT C
14         0003    PORTD    EQU    $0003    INPUT PORT D
15         **
16         ** DATA DIRECTION REGISTER OFFSET
17         **
18         0004    DDR      EQU    4        (eg. DDR FOR PORT A IS PORTA+DDR )
19         **
20         ** OTHERS
21         **
22         0008    TIMER    EQU    $0008    EIGHT BIT TIMER REGISTER.
23         0009    TCR      EQU    $0009    TIMER CONTROL REGISTER.
24         000A    MR       EQU    $000A    MISCELLANEOUS REGISTER.
25         0010    RAM      EQU    $0010    START OF ON-CHIP RAM(112 - 31 FOR STACK)
26         0080    ZROM     EQU    $0080    PAGE ZERO OF ROM.
27         0100    ROM      EQU    $0100    START OF MAIN ROM.
28         0F38    MOR      EQU    $0F38    MASK OPTION REGISTER.
29         0FF8    INTRPT   EQU    $0FF8    LOCATION OF INTERRUPT VECTORS.
30         1000    MEMSIZ   EQU    $1000    MEMORY ADDRESS SIZE.
31         **
32         ** EQUATES
33         **
34         0001    BIT0     EQU    1
35         0002    BIT1     EQU    2
36         0004    BIT2     EQU    4
37         0008    BIT3     EQU    8
38         0010    BIT4     EQU    16
39         0020    BIT5     EQU    32
40         0040    BIT6     EQU    64
41         0080    BIT7     EQU    128
42         **
43         0000    B0       EQU    0
44         0001    B1       EQU    1
45         0002    B2       EQU    2
46         0003    B3       EQU    3
47         0004    B4       EQU    4
48         0005    B5       EQU    5
49         0006    B6       EQU    6
50         0007    B7       EQU    7
51         **
52         ** EQUATES FOR THE TIMER CONTROL REGISTER
53         **
54         ***
55         0007    TIR      EQU    7        TIMER INTERRUPT REQUEST. 1 = REQUEST, 0 = NO REQ.
56         0006    TIM      EQU    6        TIMER INTERRUPT MASK. 1 = DISABLED, 0 = ENABLED.
57         0005    TIN      EQU    5        EXTERNAL OR INTERNAL CLOCK SOURCE. 1 = EXT, 0 = INT.
58         0004    TEE      EQU    4        EXTERNAL CLOCK ENABLE. NOT USED.
59         0003    PSC      EQU    3        PRESCALER CLEAR. NOT USED.
60         0002    PS2      EQU    2        (PS2)  --
61         0001    PS1      EQU    1        (PS1)  |-- PRESCALER SELECT BITS.

```

```

62      0000      PS0      EQU      0      (PS0)  --
63      **
64      ** EQUATES FOR THE STATUS BYTE, 'STAT'.
65      ***
66      ***
67      **
68      0007      UD      EQU      7      COUNT DIRECTION? 1 = UP, 0 = DOWN.
69      0006      MOD_32 EQU      6      IS 'BINCT' MODULO 32? 1 = YES, 0 = NO.
70      0005      FLASH EQU      5      BLINK THE DISPLAY? 1 = YES, 0 = NO.
71      0004      POSCT EQU      4      DISPLAY POSITION OR COUNT? 1 = POS, 0 = COUNT.
72      0003      L_SET EQU      3      VALUE OF 'MODE,PORTD' LAST TIME.
73      0002      NEGTV EQU      2      IS 'BCDCT' NEGATIVE NUMBER? 1 = YES, 0 = NO.
74      ***      1      NOT USED.
75      ***      0      NOT USED.
76      ***
77      ***
78      ** I/O EQUATES AND DESCRIPTIONS.
79      ***
80      ***
81      ***      PORT A (I/O)
82      ***
83      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
84      ***      |          BCD DIGIT #4          |          BCD DIGIT #3          |
85      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
86      ***      | D4 | C4 | B4 | A4 | D3 | C3 | B3 | A3 |
87      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
88      *** BIT      7      6      5      4      3      2      1      0
89      ***
90      ***
91      ***      PORT B (I/O)
92      ***
93      ***
94      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
95      ***      |          DISPLAY CONTROL          |          NOT USED          |
96      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
97      ***      | DECPT | POSTIV |          BLANK          |          |          |          |
98      ***      +-----+-----+-----+-----+-----+-----+-----+-----+
99      *** BIT      7      6      5      4      3      2      1      0
100     ***
101     0007      DECPT EQU      7      TO DISPLAY THE DECIMAL POINT...DECPT IS CLEARED
102     0006      POSTIV EQU      6      USED TO DISPLAY NEGATIVE SIGN...CLEARED TO SHOW
103     0004      BLANK EQU      4      MINUS SIGN.
104     ***      TO BLANK DIGITS 2 AND 3...CLEAR BLANK.
105     ***      DIGITS 4 AND 5 ARE ALWAYS BLANKED.
106     ***      DIGIT 1 IS NEVER BLANKED.
107     ***
108     ***      PORT C (I/O)
109     ***
110     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
111     ***      |          BCD DIGIT #2          | BCD DIGIT #1(LEAST SIGNIFICANT) |
112     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
113     ***      | D2 | C2 | B2 | A2 | D1 | C1 | B1 | A1 |
114     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
115     *** BIT      7      6      5      4      3      2      1      0
116     ***
117     ***
118     ***      PORT D (INPUT ONLY)
119     ***
120     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
121     ***      | CH_A | INT2 | CH_B | FUNCT | SET |          |          |          |
122     ***      +-----+-----+-----+-----+-----+-----+-----+-----+
123     *** BIT      7      6      5      4      3      2      1      0
124     0007      CH_A EQU      7      INDICATES THE STATUS OF CHANNEL A.
125     0006      INT2 EQU      6      INTERRUPT #2. USED TO CHANGE DISPLAY MODES.
126     0005      CH_B EQU      5      INDICATES THE STATUS OF CHANNEL B.
127     0004      FUNCT EQU      4      USED TO PUT THE PROGRAM IN A MODE THAT WILL ALLOW

```

```

128          0003      ***          'HYST' TO BE INCREMENTED.
129          SET      EQU      3          INCREMENTS 'HYST' WHEN TOGGLED AND FUNCT IS LOW.
130          ***
131          ***
132          ****
133          **
134          **          RAM VARIABLES
135          **
136          ****
137          **
138          ** RESERVE MEMORY SPACE FOR THE PROGRAM VARIABLES.
139          **
140          0000      DATA
141          **
142          **
143          0000      ABSOLUTE (ABSOLUTE ADDRESSING USED HERE TO RELATIVE DIRECTIVE)
144          **
145          0010      ORG      RAM      START OF RAM.
146          **
147          *** BINARY COUNT.
148          0010      BINCT RMB      2
149          0010      HIBIN EQU      BINCT      HI BYTE.
150          0011      LOBIN EQU      BINCT+1    LO BYTE.
151          **
152          *** POSITION POINTERS.
153          0012      PTR      RMB      3          EACH BYTE POINTS TO A POSITION IN THE
154          **          TABLE THAT CONTAINS ONE OR TWO DIGITS
155          **          OF THE BCD POSITION.
156          0012      PTR3     EQU      PTR      MOST SIGNIFICANT DIGITS.
157          0013      PTR2     EQU      PTR+1
158          0014      PTR1     EQU      PTR+2    LEAST SIGNIFICANT DIGIT.
159          **
160          *** COUNT POINTERS.
161          0015      CTPTR    RMB      2          EACH BYTE POINTS TO A POSITION IN THE
162          **          TABLE THAT CONTAINS TWO OF THE DIGITS
163          **          IN THE BCD COUNT.
164          0015      CTPTR2   EQU      CTPTR    MOST SIGNIFICANT DIGITS.
165          0016      CTPTR1   EQU      CTPTR+1  LEAST SIGNIFICANT DIGITS.
166          **
167          *** BCD POSITION IN DEGREES.
168          0017      DEGRES   RMB      3
169          0017      ONEDEG   EQU      DEGRES      CONTENTS X      1.000
170          0018      HUNDTH   EQU      DEGRES+1    CONTENTS X      0.010
171          0019      THOUTH   EQU      DEGRES+2    + CONTENTS X      0.001
172          ***          -----
173          ***          POSITION IN DEGREES
174          **
175          *** BCD COUNT.
176          001A      BCDCT    RMB      2
177          001A      HUNDRD   EQU      BCDCT      CONTENTS X      100
178          001B      TENONE   EQU      BCDCT+1    + CONTENTS X      1
179          ***          -----
180          ***          NUMBER OF PULSES COUNTED
181          ***
182          *** HYSTERESIS COUNTER. POINTS TO A NUMBER IN THE TABLE THAT IS THE
183          *** AMOUNT OF HYSTERESIS PRESENT IN THE SYSTEM. INITIALIZED TO 6.
184          001C      HYSTPT   RMB      1
185          **
186          *** POSITION INCREMENT. CONTAINS A NUMBER, THAT WHEN MULTIPLIED BY 0.001
187          *** IS THE NUMBER OF DEGREES THAT THE POSITION COUNTER (BCDPOS) IS
188          *** TO BE INCREMENTED OR DECREMENTED DURING PROGRAM EXECUTION.
189          *** THE VALUE OF 'POSINC', DETERMINED EXPERIMENTALLY, SHOULD BE
190          *** 7.0452. SINCE THE PROGRAM IS DESIGNED WORK WITH INTEGERS ONLY
191          *** THIS NUMBER IS ROUNDED TO 7. TO REDUCE THE CUMULATIVE EFFECT OF
192          *** THE ROUND OFF, EVERY 32 COUNTS 'POSINC' IS SET EQUAL TO 8. THIS
193          *** AGAIN LEADS TO SOME CUMULATIVE ERROR, BUT THE SMALL ANGULAR RANGE

```

```

194      ***      OF THE TILT ANGLE (10.5 DEGREES) ALLOWS US TO NEGLECT ANY FURTHER
195      ***      MODIFICATIONS.
196      ***
197 001D    POSINC  RMB      1
198      ***
199      *** HYSTERESIS VARIABLES. USED TO ELIMINATE THE EFFECTS OF BACKLASH ON
200      ***      THE POSITION MEASUREMENTS.
201      ***
202 001E    HYST     RMB      1      THE THRESHOLD VALUE DETERMINED
203      ***      EXPERIMENTALLY.
204 001F    HYSTCT   RMB      1      CURRENT AMOUNT OF HYSTERESIS MEASURED.
205      ***
206      *** STATUS BYTE. USED TO KEEP TRACK OF WHAT IS GOING ON.
207      ***
208 0020    STAT     RMB      1      CURRENT STATUS.
209 0021    LSTAT    RMB      1      PREVIOUS/LAST STATUS. USED TO KEEP TRACK OF
210      ***      L_SET ONLY.
211      ***
212      *** TIMER COUNTER. USED IN CONJUNCTION WITH THE TIMER PRESCALER AND THE
213      ***      TDR TO KEEP TRACK OF ONE SEC. INTERVALS. USED IN BLINKING THE
214      ***      DISPLAY. INITIALLY SET TO 31, WHEN THE 'FLASH' BIT OF 'STAT'
215      ***      IS SET. TIMCT IS DECREMENTED EACH CLOCK INTERRUPT (APPROX. 31
216      ***      TIMES PER SEC). RESET TO 31 WHEN CONTENTS GO TO ZERO.
217      ***      WHEN (TIMCT)=0 THE DISPLAY WILL TOGGLE.
218      ***
219 0022    TIMCT    RMB      1
220      **
221      ENDS
222      **
223      ***
224      *****
225      **
226      **      PAGE ZERO ROM
227      **
228      *****
229      **
230      **      INITIALIZATION ROUTINE.
231      **
232      **
233 0000      CODE
234      **
235 0080      ORG      ZROM      PAGE ZERO ROM.
236      **
237 0080      RELATIVE      RELATIVE ADDRESSING MUST BE USED FOR THE BRANCH.
238      **
239      0080    RESTRT  EQU      $      THIS IS THE ENTRY POINT WHEN AN EXTERNAL
240      ***      INTTERRUPT OCCURS.
241      **
242      *****
243      **
244      ***      INITIALIZE THE PC AND CLEAR RAM.
245      ***
246      ***
247 0080  9B      SEI      SET INTERUPT TO AVOID INTERUPTION AND
248 0081  9C      RSP      RESET THE STACK POINTER. JUST IN CASE!
249      ***
250 0082  AE 10    LDX      #BINCT CLEAR ALL OF THE VARIABLES BETWEEN
251 0084  7F      CLRIT    CLR      ,X 'BINCT' AND 'TIMCT' (INCLUSIVE).NOTE
252 0085  5C      INCX     THAT THIS SETS THE COUNTER AND THE POS-
253 0086  A3 22    CPX      #TIMCT ITION TO ZERO. THIS MEANS THAT ROTATION
254 0088  23 FA    BLS      CLRIT SHOULD START IN AN INCREASING (CW)
255      ***      DIRECTION FROM THE MOST CCW POSITION
256      ***      AFTER A RESET.
257      ***
258 008A      ABSOLUTE    BACK TO ABSOLUTE ADDRESSING.
259      ***

```


260			*****
261			***
262			***
263			***
264	008A	A6 FF	LDA # -1 PORTS A,B,C ARE CONFIGURED AS
265	008C	B7 04	STA PORTA+DDR ALL OUTPUT. PORT D IS ALL INPUT
266	008E	B7 05	STA PORTB+DDR SO THERE IS NO MASK TO SET.
267	0090	B7 06	STA PORTC+DDR
268			***
269			*****
270			***
271			***
272	0092	A6 08	LDA #X00001000 --
273	0094	B4 03	AND PORTD --> SET UP 'L_SET' BIT OF 'STAT'.
274	0096	B7 20	STA STAT --
275			***
276	0098	1C 20	BSET MOD_32,STAT 0 IS MODULO 32.
277			**
278			*****
279			***
280			***
281			***
282	009A	A6 06	LDA #06
283	009C	B7 1E	STA HYST
284	009E	B7 1C	STA HYSTPT
285			***
286			*****
287			**
288			**
289			SET UP THE TIMER FOR A 4 MHZ CRYSTAL / 4 = 1 MHZ CLOCK.
290			***
291			NOTE: THE MASK OPTION REGISTER IS IN ROM. IT IS SET UP AT
292			THE END OF THE PROGRAM.
293			*****
294			***
295	00A0	A6 47	LDA #BIT6+BIT2+BIT1+BIT0
296			(TIM) (PS2)(PS1)(PS0)
297			*** (DISABLE INTERRUPT) (PRESCALE BY 128)
298			***
299	00A2	B7 09	STA TCR
300			***
301			***
302			*** SET UP THE TIMER.
303			***
304	00A4	A6 FF	LDA #255 1 MHZ/(128*255) = 30.6 (APPROX. 31)
305	00A6	B7 08	STA TIMER
306			***
307			*****
308			***
309	00A8	A6 1F	LDA #31 PROVIDES FOR 1 SEC. BLINK INTERVAL.
310	00AA	B7 22	STA TIMCT FOR 2 SEC. INTERVAL JUST USE TIMECT=62, etc.
311			***
312			***
313			*****
314			**
315			**
316			SET UP MISCELLANEOUS REGISTER.
317	00AC	1D 0A	BCLR B6,MR ENABLES THE SECOND INTERRUPT.
318			**
319			*****
320			**
321			**
322			COUNT = 0 IS DISPLAYED INITIALLY.
323	00AE	CD 02 D8	JSR OUTCT
324	00B1	1C 01	BSET POSTIV,PORTB
325			**


```

326
327 00B3 9A
328
329 00B4
330
331
332
333
334
335
336 00B4 09 03 0B
337
338 00B7 06 03 04
339 00BA 17 20
340 00BC 20 F6
341 00BE 16 20
342 00C0 20 F2
343
344
345
346
347
348
349 00C2 A6 40
350 00C4 B7 09
351
352 00C6 A6 08
353 00C8 B4 20
354 00CA B7 21
355 00CC A6 08
356 00CE B4 03
357 00D0 B1 21
358 00D2 27 15
359
360 00D4 A6 08
361 00D6 B8 20
362 00D8 B7 20
363 00DA 3C 1E
364 00DC 3C 1C
365
366 00DE B6 1C
367 00E0 A1 19
368 00E2 23 05
369
370 00E4 4F
371 00E5 B7 1E
372 00E7 B7 1C
373
374 00E9 A6 00
375 00EB B7 00
376 00ED A6 C0
377 00EF B7 01
378
379 00F1 BE 1C
380 00F3 D6 03 28
381 00F6 B7 02
382
383 00F8 09 03 C7
384 00FB 04 20 04
385 00FE 1C 01
386 0100 20 02
387 0102 1D 01
388 0104 08 20 05
389
390 0107 CD 02 D8
391 010A 20 03

**
**
*** CLI CLEAR THE INTERRUPT MASK TO GET STARTED.
**
***
*** RELATIVE RELATIVE ADDRESSING MUST BE USED FOR THE
*** REMAINDER OF THE PROGRAM.
*****
**
** ** WAIT LOOP. EXECUTES, UNTIL AN INTERRUPT OCCURS.
**
PAUSE BRCLR FUNCT,PORTD,CHYST WANT TO CHANGE HYST?
** YES...GO TO CHYST.
BRSET SET,PORTD,SBIT NO...'SET,PORTD' SET?
BCLR L_SET,STAT NO...CLEAR 'L_SET,STAT'
BRA PAUSE AND LOOP.
SBIT BSET L_SET,STAT YES...SET 'L_SET,STAT'
BRA PAUSE AND LOOP.
*****
**
** ** HYSTERESIS MODIFICATION ROUTINE. PERMITS MODIFICATION OF THE
** HYSTERESIS BUFFER WITHOUT REPROGRAMMING.
** YES...
CHYST LDA #BIT6 DISABLE TIMER INTERRUPT.
STA TCR
***
LDA #X00001000 SAVE 'L_SET'
AND STAT INTO
STA LSTAT 'LSTAT'.
LDA #X00001000
AND PORTD 'SET,PORTD' --> ACCUMULATOR
CMP LSTAT HAS THE SET SWITCH BEEN CHANGED?
BEQ DISPLA
***
YES...
LDA #X00001000 --
EOR STAT |--->CHANGE 'L_SET,STAT',
STA STAT --
INC HYST THEN INCREMENT THE HYSTERESIS
INC HYSTPT POINTER AND 'HYST'...
***
LDA HYSTPT --
CMP #25 --
BLS DISPLA --
***
-- BUT NOT ABOVE 25.
-- THEN--->
CLRA --
STA HYST --
STA HYSTPT --
***
DISPLA LDA #X00000000 NO... JUST----->
STA PORTA --
LDA #X11000000 --
STA PORTB --
***
-- DISPLAY CURRENT 'HYST'.
LDX HYSTPT --
LDA TABLE,X --
STA PORTC --
***
IS 'HYST' SETTING COMPLETE?
BRCLR FUNCT,PORTD,CHYST NO... KEEP CHECKING 'SET'.
BRSET NEGTV,STAT,SIGN YES... RESET THE DISPLAY.
BSET POSTIV,PORTB
BRA DIR
SIGN BCLR POSTIV,PORTB
DIR BRSET POSCT,STAT,SHOPOS
**
JSR OUTCT
BRA DUNCHG

```

```

392
393 010C CD 02 E5
394
395 010F 08 20 04
396 0112 A6 07
397 0114 B7 09
398 0116 20 9C
399
400
401
402
403
404
405
406
407
408
409
410
411
412
413
414
415
416
417
418
419 0118 1F 0A
420
421 011A 0A 20 10
422 011D 09 20 07
423 0120 1A 20
424
425 0122 A6 07
426 0124 B7 09
427 0126 80
428
429 0127 18 20
430 0129 CD 02 E5
431 012C 80
432
433 012D A6 47
434 012F B7 09
435 0131 19 20
436 0133 1B 20
437
438 0135 CD 02 D8
439 0138 80
440
441
442
443
444
445
446
447
448
449 0139
450 0139 0F 09 DC
451
452
453 013C 1F 09
454
455 013E 3A 22
456 0140 27 01
457

***
SHOPOS JSR OUTPOS
***
DUNCHG BRCLR FLASH,STAT,NO_INT IF THE DISPLAY IS TO BLINK...
LDA #BIT2+BIT1+BIT0 ENABLE TIMER INTERRUPT AND RESET
STA TCR TIMER PRESCALER
NO_INT BRA PAUSE PRIOR TO RETURNING.
***
**
*****
** MAXIMUM EXECUTION TIME FOR THE REMAINDER OF THE PROGRAM OCCURS
** IF THE COUNTER ROTATES THROUGH ZERO AS THE DISPLAY MODE IS CHANGED
** FROM THE BLINKING MODE TO THE COUNT MODE AT THE SAME TIME THAT THE
** BLINKING ROUTINE IS CAUSING THE DISPLAY TO TOGGLE TO SHOW THE
** POSITION IN DEGREES.
** MAXIMUM EXECUTION TIME = 67 + 140 + 618 = 825 CLOCK CYCLES.
**
*****
**
**MODE CHANGE ROUTINE. CHANGES THE DISPLAY MODE FROM
** COUNT -> POSITION -> BLINKING -> COUNT ->....(ETC.)
** MAXIMUM EXECUTION TIME OF 127 CLOCK CYCLES OCCURS WHEN THE
** DISPLAY MODE IS CHANGED FROM DISPLAYING THE COUNT TO DISPLAYING
** THE POSITION (IN DEGREES).
** IF THE DISPLAY IS CHANGED FROM BLINKING TO A COUNT DISPLAY
** EXECUTION TIME IS 67 CLOCK CYCLES.
**
CHMODE BCLR B7,MR AVOID REPEATED INTERRUPTS.
**
BRSET FLASH,STAT,DIS_CT IF FLASHING, DISPLAY COUNT...
BRCLR POSCT,STAT,DISPOS IF SHOWING COUNT, DISPLAY POSITION...
BSET FLASH,STAT ELSE, BLINK.
**
LDA #BIT2+BIT1+BIT0 ENABLE TIMER INTERRUPT AND RESET
STA TCR TIMER PRESCALER.
RTI
**
DISPOS BSET POSCT,STAT --
JSR OUTPOS |-- DISPLAY CURRENT POSITION, AND WAIT.
RTI --
**
DIS_CT LDA #BIT6+BIT2+BIT1+BIT0 DISABLE TIMER INTERRUPT AND RESET
STA TCR TIMER PRESCALER.
BCLR POSCT,STAT --
BCLR FLASH,STAT --
**
JSR OUTCT |-- DISPLAY CURRENT COUNT, AND WAIT.
RTI --
**
*****
**
** BLINK ROUTINE. INTERRUPT ROUTINE TO CHANGE THE DISPLAY FROM POSITION
** TO COUNT OR VICE VERSA EVERY 31 ST TIMER INTERRUPT IF THE
** 'FLASH' BIT OF 'STAT' IS SET.
** MAXIMUM EXECUTION TIME OF 140 CLOCK CYCLES OCCURS WHEN THE
** DISPLAY IS TOGGLED FROM A COUNT DISPLAY TO A POSITION DISPLAY.
**
BLINK EQU $
BRCLR TIR,TCR,CHMODE IF THE INTERRUPT WAS NOT A TIMER
INTERRUPT IT MUST BE FROM INT2.
**
**
BCLR TIR,TCR AVOID REPEATED TIMER INTERRUPTS.
**
DEC TIMCT IF THERE HAVE BEEN 31 TIMER
BEQ CHGDIS INTERRUPTS (1 SEC), IT'S TIME TO
CHANGE THE DISPLAY.
**

```

```

458 0142 80 RTI OTHERWISE, IT'S BACK TO WORK.
459
460 0143 A6 1F CHGDIS LDA #31 RESET TIMCT TO 31 (1 SEC. INTERVAL).
461 0145 B7 22 STA TIMCT
462
463 0147 B6 20 LDA STAT --
464 0149 A8 10 EOR #X00010000 |-- CHANGE 'POSCT' BIT OF 'STAT'.
465 0148 B7 20 STA STAT --
466
467 014D 08 20 04 BRSET POSCT,STAT,POSOUT DECIDE ON CORRECT DISPLAY.
468
469 ***** CHANGE THE DISPLAY TO SHOW THE COUNT.... *****
470
471 0150 CD 02 D8 JSR OUTCT
472 0153 80 RTI
473
474 ***** OR HAVE THE DISPLAY SHOW THE POSITION. *****
475
476 0154 CD 02 E5 POSOUT JSR OUTPOS
477 0157 80 RTI
478
479 *****
480
481 COUNT ROUTINE.
482 WHEN A COUNT IS RECEIVED THIS IS THE ENTRY POINT .
483 MAXIMUM EXECUTION TIME OF 618 CLOCK CYCLES OCCURS WHEN THE
484 COUNTER ROTATES CCW THROUGH ZERO AND THE POSITION (IN DEGREES)
485 IS BEING DISPLAYED.
486
487
488
489 ** CURRENT DIRECTION OF ROTATION IS DETERMINED BY INSPECTING THE STATUS
490 ** OF 'CH_A' AND 'CH_B'. THE FOUR POSSIBILITIES AND THE ASSOCIATED
491 ** DIRECTION OF ROTATION ARE AS SHOWN BELOW. NOTE THAT THIS SCHEME
492 ** PREVENTS MULTIPLE OSCILLATIONS ABOUT A SINGLE POINT FROM
493 ** REPEATEDLY INCREMENTING OR DECREMENTING THE COUNTER.
494
495 **
496 ** +-----+-----+-----+-----+
497 ** | CH_A | CH_B | DIRECTION | COUNT THE PULSE? |
498 ** |-----+-----+-----+-----+
499 ** | LO | LO | CW | NO |
500 ** | LO | HI | CCW | YES |
501 ** | HI | LO | CCW | NO |
502 ** | HI | HI | CW | YES |
503 ** +-----+-----+-----+-----+
504
505 ***** FIRST SEE IF WE ARE SUPPOSED TO COUNT THIS INTERRUPT. *****
506
507 0158 0158 COUNT EQU $
508 015B 0A 03 01 BRSET CH_B,PORTD,OKCT IF CH_B IS LO WE DON'T COUNT THE
509 015B 80 RTI INTERRUPT.
510
511 ***** IF THE INTERRUPT IS VALID UPDATE 'STAT'. *****
512
513 015C A6 7F OKCT LDA #X01111111
514 015E B4 20 AND STAT SAVE ALL OF THE OLD 'STAT' EXCEPT THE
515 0160 B7 20 STA STAT DIRECTION OF ROTATION.
516 0162 A6 80 LDA #X10000000
517 0164 B4 03 AND PORTD 'CH_A,PORTD' INDICATES THE DIRECTION
518 0166 BA 20 * OF ROTATION AND BECOMES 'UD,STAT'.
519 0168 B7 20 ORA STAT ADD THE RESULTS TO GET
520 STA STAT THE NEW 'STAT'.
521
522 ** DECIDE IF THE "SLACK" DUE TO BACKLASH/HYSTERESIS HAS BEEN TAKEN OUT.
523
524 016A 0E 20 09 BRSET UD,STAT,HYSTCK IF ROTATING CW SEE BELOW.

```

```

524 0160 B6 1F          LDA    HYSTCT      ELSE, SEE IF WE DECREMENT THIS TIME.
525 016F 27 4B          BEQ    CCW          IF HYSTCT=0, GO TO THE COUNT DOWN
526                                     **      ROUTINE.
527 0171 A0 01          SUB    #1          ELSE, DECREMENT THE HYSTERESIS COUNTER,
528 0173 B7 1F          STA    HYSTCT
529 0175 80             RTI              AND WAIT FOR THE NEXT INTERRUPT.
530                                     **
531 0176 B6 1E          HYSTCK LDA    HYST      IF ROTATING CW....
532 0178 B1 1F          CMP    HYSTCT      AND HYST = HYSTCT ....
533 017A 27 03          BEQ    CW          COUNT THE PULSE .
534 017C 3C 1F          INC    HYSTCT      ELSE, INCREMENT THE HYSTERESIS COUNTER,
535 017E 80             RTI              AND WAIT FOR ANOTHER PULSE.
536                                     **
537                                     **
538 *****
539                                     **
540                                     **
541                                     **      CLOCKWISE ROUTINE.
542 017F          CW      EQU    $
543                                     **
544                                     ***
545 ***** INCREMENT THE BINARY COUNTER (BINCT). *****
546                                     ***
547 017F B6 11          LDA    LOBIN      BEGIN AT THE LSB OF THE BINARY COUNTER.
548 0181 AB 01          ADD    #1        LOBIN = LOBIN + 1 ; CARRY -> C,CCR
549 0183 B7 11          STA    LOBIN
550                                     ***
551 0185 B6 10          LDA    HIBIN
552 0187 A9 00          ADC    #0        ADD THE CARRY TO THE HIGH BYTE.
553 0189 B7 10          STA    HIBIN
554                                     ***
555                                     ***
556 ***** CLR/SET MOD_32 APPROPRIATELY. *****
557                                     ***
558 018B B6 11          LDA    LOBIN      IF THE LOW FIVE BITS OF 'LOBIN' ARE NOT
559 018D A4 1F          AND    #%00011111 NOT THEN THE NUMBER ISN'T A MODULO 32 NUMBER.
560 018F 26 04          BNE    NOT_32
561                                     ***
562 0191 1C 20          BSET    MOD_32,STAT
563 0193 20 02          BRA    DIRCHK
564                                     ***
565 0195 1D 20          NOT_32 BCLR    MOD_32,STAT
566                                     ***
567                                     ***
568 0197 B6 10          DIRCHK LDA    HIBIN
569 0199 28 19          BMI    CWNEG      IF HIBIN < 0 , WE'RE ROTATING CW TOWARD
570                                     ***      THE ORIGIN.
571                                     ***
572 019B 26 10          BNE    CWPOS      ELSE IF BINCT .NE. 0 ,
573 019D B6 11          LDA    LOBIN      WE'RE ROTATING CW
574 019F 26 0C          BNE    CWPOS      AWAY FROM THE ORIGIN.
575                                     ***
576 01A1 15 20          BCLR    NEGTV,STAT ELSE, WE'VE GONE THROUGH ORIGIN IN CW
577                                     ***      DIRECTION. CLR NEGATIVE SIGN.
578 01A3 AE 12          LDX    #PTR3    --
579 01A5 7F            CLRIT2 CLR    ,X    --
580 01A6 5C            INCX           --RESET ALL COUNTERS AND DEGRES TO ZERO.
581 01A7 A3 19          CPX    #THOUTH --
582 01A9 23 FA          BLS    CLRIT2 --
583 01AB 20 4C          BRA    UPOUT      UPDATE OUTPUT.
584                                     ***
585 01AD AD 5E          CWPOS  BSR    ADDBCD
586 01AF CD 02 32       JSR    INCPOS
587 01B2 20 45          BRA    UPOUT
588                                     ***
589 01B4 CD 02 7A       CWNEG  JSR    SUBBCD

```



```

590 01B7 CD 02 9A      JSR   DECPOS
591 01BA 20 3D      BRA   UPOUT
592      ***
593      **
594      *****
595      **
596      **          COUNTER-CLOCKWISE ROUTINE.
597      **
598      01BC      CCW   EQU   $
599      ***
600      ***
601      ***** CLR/SET MOD_32 APPROPRIATELY. *****
602      ***
603 01BC B6 11      LDA   LOBIN   IF THE LOW FIVE BITS OF 'LOBIN' ARE NOT
604 01BE A4 1F      AND   #X00011111 ZERO THEN THE NUMBER ISN'T A MODULO 32 NUMBER.
605 01C0 26 04      BNE   NO_32
606      ***
607 01C2 1C 20      BSET  MOD_32,STAT
608 01C4 20 02      BRA   DECBIN
609      ***
610 01C6 1D 20      NO_32 BCLR  MOD_32,STAT
611      ***
612      ***
613      ***** DECREMENT THE BINARY COUNTER (BINCT). *****
614      ***
615 01C8 B6 11      DECBIN LDA  LOBIN   BEGIN AT THE LSB OF THE BINARY COUNTER.
616 01CA A0 01      SUB   #1     LOBIN = LOBIN - 1 ; BORROW -> C,CCR
617 01CC B7 11      STA   LOBIN
618      ***
619 01CE B6 10      LDA   HIBIN
620 01D0 A2 00      SBC   #0     SUBTRACT THE CARRY FROM THE HIGH BYTE.
621 01D2 B7 10      STA   HIBIN
622      ***
623 01D4 B6 10      LDA   HIBIN
624 01D6 2A 1B      BPL   CCWPOS   IF HIBIN .GE. 0 , WE'RE ROTATING CCW TOWARD
625      ***                               THE ORIGIN.
626 01D8 A1 FF      CMP   #-1    --
627 01DA 26 10      BNE   CCWNEG   -- ELSE IF BINCT .NE. -1 ,
628 01DC B6 11      LDA   LOBIN   --WE'RE ROTATING CCW AWAY
629 01DE A1 FF      CMP   #-1    -- FROM THE ORIGIN.
630 01E0 26 0A      BNE   CCWNEG   --
631 01E2 14 20      BSET  NEGTV,STAT ELSE, WE'VE GONE THROUGH ORIGIN IN CCW
632      ***                               DIRECTION. SET NEGATIVE SIGN.
633      ***                               AND SET ALL COUNTERS APPROPRIATELY.
634 01E4 AE 12      LDX   #PTR3   --
635 01E6 7F          CLREM CLR   ,X    --
636 01E7 5C          INCX          -- RESET ALL COUNTERS AND DEGRES TO ZERO.
637 01E8 A3 19      CPX   #THOUTH --
638 01EA 23 FA      BLS   CLREM   --
639      ***
640 01EC AD 1F      CCWNEG BSR   ADDBCD
641 01EE CD 02 32   JSR   INCPOS
642 01F1 20 06      BRA   UPOUT
643      ***
644 01F3 CD 02 7A   CCWPOS JSR   SUBBCD
645 01F6 CD 02 9A   JSR   DECPOS
646      ***
647      ***
648      **
649      *****
650      **
651      ** OUTPUT ROUTINE. ROUTINE TO PRINT DATA TO THE OUTPUT PORTS. BY
652      ** CALLING THE APPROPRIATE SUBROUTINE.('OUTCT' TO OUTPUT THE
653      ** THE COUNT AND 'OUTPOS' TO OUTPUT THE POSITION).
654      **
655      01F9      UPOUT EQU   $

```



```

656
657 01F9 04 20 04
658 01FC 1C 01
659 01FE 20 02
660
661 0200 1D 01
662
663 0202 09 20 04
664
665 0205 CD 02 E5
666 0208 80
667
668 0209 CD 02 D8
669 020C 80
670
671
672
673
674 020D B6 16
675 020F AB 01
676 0211 A1 63
677 0213 23 05
678 0215 A0 64
679 0217 99
680 0218 20 01
681
682 021A 98
683 021B B7 16
684 021D 97
685
686 021E D6 03 28
687 0221 B7 1B
688 0223 24 0C
689
690
691 0225 B6 15
692 0227 A9 00
693 0229 B7 15
694 022B 97
695
696 022C D6 03 28
697 022F B7 1A
698
699 0231 81
700
701
702
703
704
705
706
707 0232 00 20 04
708
709 0235 A6 08
710 0237 20 02
711
712 0239 A6 07
713 023B B7 1D
714
715
716
717
718 023D B6 14
719 023F BB 1D
720 0241 A1 09
721 0243 23 05

**
BRSET NEGTV,STAT,MINUS --
BSET POSTIV,PORTB --
BRA DISCHK --
**
MINUS BCLR POSTIV,PORTB -- SET THE NEGATIVE SIGN
** APPROPRIATELY.
DISCHK BRCLR POSCT,STAT,PUTCT
**
JSR OUTPOS
RTI
**
PUTCT JSR OUTCT
RTI
**
*****
***** SUBROUTINE TO INCREMENT THE BCD COUNTER (BCDCT). *****
***
ADDBCD LDA CTPTR1
ADD #1
CMP #99 CTPTR > 99 ?
BLS OK1 NO, WE'RE OK HERE. LOOK UP THE FIRST TWO DIGITS.
SUB #100 YES... MODIFY THE CTPTR,
SEC SET THE CARRY, AND
BRA OK1A USE TABLE LOOK UP.
***
OK1 CLC NO CARRY EXISTS IF WE ENTER AT THIS POINT.
OK1A STA CTPTR1 --
TAX --
***
-- LOOK UP THE TWO LEAST SIGNIFICANT DIGITS.
LDA TABLE,X --
STA TENONE --
BCC NOMO AND CONTINUE ONLY IF THERE WAS A CARRY.
***
***
LDA CTPTR2
ADC #0 ADD THE CARRY.
STA CTPTR2 --
TAX --
***
-- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
LDA TABLE,X --
STA HUNDRD --
***
NOMO RTS
***
*****
***** SUBROUTINE TO INCREMENT THE POSITION COUNTER (DEGRES). *****
***
**** FIRST CHECK TO SEE IF THE BINARY COUNTER HAS REACHED A MODULO 32
**** NUMBER.
****
INCPOS BRCLR MOD_32,STAT,INC7 'MOD_32,STAT' SET ?
****
LDA #8 YES ...
BRA INC INCREMENT THE POSITION BY 0.008 DEGREES.
****
INC7 LDA #7 NO ....
INC STA POSINC INCREMENT THE POSITION BY 0.007 DEGREES.
****
**** ROUTINE TO INCREMENT THE POSITION COUNTER ,'DEGRES',BY A
**** PREDETERMINED AMOUNT, 'POSINC'.
****
LDA PTR1
ADD POSINC
CMP #9 PTR1 > 9 ?
BLS OK3 NO, WE'RE OK HERE. LOOK UP THE FIRST DIGIT.

```

722	0245	A0 0A	SUB	#10	YES... MODIFY THE CTPTR,
723	0247	99	SEC		SET THE CARRY, AND
724	0248	20 01	BRA	OK3A	USE TABLE LOOK UP.
725			****		
726	024A	98	OK3	CLC	NO CARRY EXISTS IF WE ENTER AT THIS POINT.
727	024B	B7 14	OK3A	STA	PTR1 --
728	024D	97		TAX	--
729			****		-- LOOK UP THE LEAST SIGNIFICANT DIGIT.
730	024E	D6 03 28		LDA	TABLE,X --
731	0251	B7 19		STA	THOUTH --
732	0253	24 24		BCC	DONE AND CONTINUE ONLY IF THERE WAS A CARRY.
733			****		
734			****		
735	0255	B6 13		LDA	PTR2
736	0257	A9 00		ADC	#0 ADD THE CARRY.
737	0259	A1 63		CMP	#99 PTR2 > 99 ?
738	025B	23 05		BLS	OK4 NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.
739	025D	A0 64		SUB	#100 YES...MODIFY THE CTPTR,
740	025F	99		SEC	SET THE CARRY,
741	0260	20 01		BRA	OK4A AND USE TABLE LOOK UP.
742			****		
743	0262	98	OK4	CLC	NO CARRY EXISTS IF WE ENTER AT THIS POINT.
744	0263	B7 13	OK4A	STA	PTR2 --
745	0265	97		TAX	--
746			****		-- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
747	0266	D6 03 28		LDA	TABLE,X --
748	0269	B7 18		STA	HUNDTH --
749	026B	24 0C		BCC	DONE AND CONTINUE ONLY IF THERE WAS A CARRY.
750			****		
751			****		
752	026D	B6 12		LDA	PTR3
753	026F	A9 00		ADC	#0 ADD THE CARRY.
754	0271	B7 12		STA	PTR3 --
755	0273	97		TAX	--
756			****		-- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
757	0274	D6 03 28		LDA	TABLE,X --
758	0277	B7 17		STA	ONEDEG --
759			****		
760	0279	81	DONE	RTS	
761			***		
762			*		
763			*****		*****
764			*****		SUBROUTINE TO DECREMENT THE BCD COUNTER (BCDCT). *****
765			***		
766	027A	B6 16	SUBBCD	LDA	CTPTR1
767	027C	A0 01		SUB	#1 CTPTR > 99 ?
768	027E	24 03		BCC	OK6 NO, WE'RE OK HERE. LOOK UP THE FIRST TWO DIGITS.
769	0280	AB 64		ADD	#100 YES, MODIFY THE CTPTR, AND
770	0282	99		SEC	GENERATE A BORROW.
771			***		
772	0283	B7 16	OK6	STA	CTPTR1 --
773	0285	97		TAX	--
774			***		-- LOOK UP THE TWO LEAST SIGNIFICANT DIGITS.
775	0286	D6 03 28		LDA	TABLE,X --
776	0289	B7 18		STA	TENONE --
777	028B	24 0C		BCC	COMPLT AND CONTINUE ONLY IF THERE WAS A BORROW.
778			***		
779			***		
780	028D	B6 15		LDA	CTPTR2
781	028F	A2 00		SBC	#0 SUBTRACT THE CARRY. CTPTR > 99 ?
782	0291	B7 15		STA	CTPTR2 --
783	0293	97		TAX	--
784			***		-- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
785	0294	D6 03 28		LDA	TABLE,X --
786	0297	B7 1A		STA	HUNDRD --
787			***		

```

788 0299 81          COMPLT RTS
789                ***
790                *****
791                ***** SUBROUTINE TO DECREMENT THE POSITION COUNTER (DEGRES). *****
792                ***
793                **** FIRST CHECK TO SEE IF THE BINARY COUNTER HAS REACHED A MODULO 32
794                **** NUMBER.
795                ****
796 029A 00 20 04     DECPOS BRCLR MOD_32,STAT,DEC7      'MOD_32,STAT' SET ?
797                ****
798 029D A6 08         LDA #8                               YES...
799 029F 20 02         BRA DEC                             DECREMENT THE POSITION BY 0.008 DEGREES.
800
801 02A1 A6 07         DEC7 LDA #7                           NO ....
802 02A3 B7 1D         DEC STA POSINC                       DECREMENT THE POSITION BY 0.007 DEGREES.
803                ****
804                **** ROUTINE TO DECREMENT THE POSITION COUNTER ,'DEGREES',BY A
805                **** PREDETERMINED AMOUNT, 'POSINC'.
806                ****
807 02A5 B6 14         LDA PTR1
808 02A7 B0 1D         SUB POSINC PTR1 < 0 ?
809 02A9 24 03         BCC OK8                               NO, WE'RE OK HERE. LOOK UP THE FIRST DIGIT.
810 02AB AB 0A         ADD #10                               YES, MODIFY THE CTPTR, AND
811 02AD 99            SEC                                   GENERATE A BORROW.
812                ****
813 02AE B7 14         OK8 STA PTR1 --
814 02B0 97            TAX --
815                **** -- LOOK UP THE LEAST SIGNIFICANT DIGIT.
816 02B1 D6 03 28     LDA TABLE,X --
817 02B4 B7 19         STA THOUTH --
818 02B6 24 1F         BCC DUNSUB                            AND CONTINUE ONLY IF THERE WAS A BORROW.
819                ***
820                ***
821 02B8 B6 13         LDA PTR2
822 02BA A2 00         SBC #0                                SUBTRACT THE BORROW. PTR2 < 0 ?
823 02BC 24 03         BCC OK9                               NO, WE'RE OK HERE. LOOK UP THE NEXT TWO DIGITS.
824 02BE AB 64         ADD #100                              YES, MODIFY THE CTPTR, AND
825 02C0 99            SEC                                   GENERATE A BORROW.
826                ***
827 02C1 B7 13         OK9 STA PTR2 --
828 02C3 97            TAX --
829                *** -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
830 02C4 D6 03 28     LDA TABLE,X --
831 02C7 B7 18         STA HUNDTH --
832 02C9 24 0C         BCC DUNSUB                            AND CONTINUE ONLY IF THERE WAS A CARRY.
833                ***
834                ***
835 02CB B6 12         LDA PTR3
836 02CD A2 00         SBC #0                                SUBTRACT THE BORROW.
837 02CF B7 12         STA PTR3 --
838 02D1 97            TAX --
839                **** -- LOOK UP THE NEXT TWO DIGITS IN THE TABLE.
840 02D2 D6 03 28     LDA TABLE,X --
841 02D5 B7 17         STA ONEDEG --
842                ****
843 02D7 81          DUNSUB RTS
844                ***
845                **
846                **
847                *****
848                **
849                ** OUTPUT COUNT (OUTCT). SUBROUTINE TO MOVE THE CURRENT COUNT (BCDCT)
850                ** TO THE OUTPUT PORTS. REMOVES THE DECIMAL POINT FROM THE
851                ** DISPLAY AND BLANKS ALL BUT THE LEAST SIGNIFICANT DIGIT. ALSO
852                ** SETS THE MINUS SIGN IF APPROPRIATE.
853                **

```

```

854          02D8          OUTCT EQU $
855          **
856 02D8 B6 18          LDA TENONE
857 02DA B7 02          STA PORTC
858          **
859 02DC B6 1A          LDA HUNDRD
860 02DE B7 00          STA PORTA
861          **
862 02E0 1E 01          BSET DECPT,PORTB
863 02E2 19 01          BCLR BLANK,PORTB
864          **
865 02E4 81          RTS
866          **
867          *****
868          **
869          ** OUTPUT POSITION (OUTPOS). SUBROUTINE TO MOVE THE CURRENT POSITION
870          ** COUNT (BCDCT) TO THE OUTPUT PORTS. THE DECIMAL POINT IS
871          ** DISPLAYED , AND ONLY THE MOST SIGNIFICANT DIGIT IS BLANKED.
872          **
873          02E5          OUTPOS EQU $
874          **
875 02E5 B6 19          LDA THOUTH --
876 02E7 A1 05          CMP #5 --
877 02E9 25 2D          BLO TRUNC -- IF 5 > 'THOUTH' SIMPLY TRUNCATE THE
878 02EB B6 18          LDA HUNDTH -- DISPLAY. OTHERWISE...
879 02ED A4 09          AND #9 -- IF THE LAST DIGIT ISN'T A NINE IT IS
880 02EF A1 09          CMP #9 -- EASY TO ROUND UP. JUST ADD A ONE.
881 02F1 26 1D          BNE DECIMAL --
882 02F3 B6 18          LDA HUNDTH -- BUT IF THE LAST DIGIT IS A NINE CHECK TO
883 02F5 A1 99          CMP #$99 -- SEE IF IT'S 99. IF SO IT GETS GRIM.
884 02F7 27 04          BEQ UGLY --
885 02F9 AB 07          ADD #7 -- IF THE NUMBER IS X9 AND X .NE. 9, THEN
886 02FB 20 1D          BRA PCOUT -- JUST ADD SEVEN TO ROUND UP. DUE TO
887          ** -- HEXIDECIMAL.
888          ** -- IF THE LOW TWO DIGITS ARE BOTH NINES
889 02FD A6 00          UGLY LDA #00 -- AND WE NEED TO ROUND UP....
890 02FF B7 02          STA PORTC -- MAKE THE LOW TWO DIGITS BOTH ZEROS
891 0301 99          SEC -- AND SET THE CARRY.
892          **
893 0302 B6 17          LDA ONEDEG -- CHECK THE LAST DIGIT AS BEFORE.
894 0304 A4 09          AND #9 -- IF USING THIS PORTION OF THE CODE
895 0306 A1 09          CMP #9 -- THERE HAD TO BE A CARRY.
896 0308 26 13          BNE NEXT -- IF THE LAST DIGIT IS A NINE DO THE
897 030A B6 17          LDA ONEDEG -- CARRY HERE. IF NOT USE THE ADC
898 030C AB 07          ADD #7 -- INSTRUCTION TO TAKE CARE OF IT
899 030E 20 11          BRA PAOUT -- BELOW.
900 0310 B6 18          DECIMAL LDA HUNDTH --
901 0312 AB 01          ADD #1 --
902          ** -- THIS IS ALL THAT NEEDS TO BE DONE IF
903 0314 B7 02          STA PORTC -- THE LAST DIGIT IS NOT A NINE.
904 0316 20 05          BRA NEXT --
905          **
906 0318 B6 18          TRUNC LDA HUNDTH --
907 031A B7 02          PCOUT STA PORTC -- AND IF THERE IS NO CARRY IT'S EVEN EASIER.
908 031C 98          CLC --
909          **
910 031D B6 17          NEXT LDA ONEDEG
911 031F A9 00          ADC #0
912 0321 B7 00          PAOUT STA PORTA
913          **
914 0323 18 01          BSET BLANK,PORTB
915 0325 1F 01          BCLR DECPT,PORTB
916          **
917 0327 81          RTS
918          **
919          *****

```



```

920
921
922
923
924
925 0328 00 01 02 03 04
032D 05 06 07 08 09
926 0332 10 11 12 13 14
0337 15 16 17 18 19
927 033C 20 21 22 23 24
0341 25 26 27 28 29
928 0346 30 31 32 33 34
034B 35 36 37 38 39
929 0350 40 41 42 43 44
0355 45 46 47 48 49
930 035A 50 51 52 53 54
035F 55 56 57 58 59
931 0364 60 61 62 63 64
0369 65 66 67 68 69
932 036E 70 71 72 73 74
0373 75 76 77 78 79
933 0378 80 81 82 83 84
037D 85 86 87 88 89
934 0382 90 91 92 93 94
0387 95 96 97 98 99

935
936
937
938
939
940
941 038C
942
943
944
945 0F38
946 0F38 07
947
948
949
950
951
952
953
954
955
956
957
958
959
960
961
962
963 0FF8
964
965 0FF8 0139
966 0FFA 0158
967 0FFC 0158
968 0FFE 0080
969
970
971
972
973 1000

**
** SET UP THE TABLE TO BE USED WITH BCD INCREMENT/DECREMENT ROUTINES.
**
*      ENDS
*      DATA
TABLE  FCB  $00,$01,$02,$03,$04,$05,$06,$07,$08,$09
FCB  $10,$11,$12,$13,$14,$15,$16,$17,$18,$19
FCB  $20,$21,$22,$23,$24,$25,$26,$27,$28,$29
FCB  $30,$31,$32,$33,$34,$35,$36,$37,$38,$39
FCB  $40,$41,$42,$43,$44,$45,$46,$47,$48,$49
FCB  $50,$51,$52,$53,$54,$55,$56,$57,$58,$59
FCB  $60,$61,$62,$63,$64,$65,$66,$67,$68,$69
FCB  $70,$71,$72,$73,$74,$75,$76,$77,$78,$79
FCB  $80,$81,$82,$83,$84,$85,$86,$87,$88,$89
FCB  $90,$91,$92,$93,$94,$95,$96,$97,$98,$99

*      ENDS
*      CODE
*****
**
**          SET UP MASK OPTION REGISTER.
**
**          ABSOLUTE      JUST TO ENSURE THAT THE INTERRUPT VECTORS
**                          ARE CORECTLY LOCATED.
**
**
**          ORG      MOR
**          FCB      #BIT2+BIT1+BIT0
**
**          COMMENTS:
**          BIT 7    CLOCK SOURCE 0 = CRYSTAL.
**          BIT 6    TIMER OPTION 0 = INTERNAL.
**          BIT 5    TIMER/CLOCK SOURCE 0 = INTERNAL.
**          BIT 4    NOT USED.
**          BIT 3    NOT USED.
**          BIT 2    SET -
**          BIT 1    SET - PRESCALE SELECT 111 => 128
**          BIT 0    SET -
**
*****
**
**          ASSIGN INTERRUPT VECTORS.
**
**          ORG      INTRPT
**
**          FDB      BLINK    TIMER/INT2 INTERRUPT VECTOR.
**          FDB      COUNT    EXTERNAL INTERRUPT VECTOR.
**          FDB      COUNT    SOFTWARE INTERRUPT VECTOR, NOT USED.
**          FDB      RESTRT    RESET VECTOR.
**
**
**          ENDS
**          END

```

Lines Assembled : 973

Assembly Errors : 0

LIST OF REFERENCES

1. Ayers, Gary Robert, *Calibration and Initialization of the NPS Modified Infrared Search and Target Designation (IRSTD) System*, Master's Thesis, Naval Postgraduate School, Monterey, CA, December 1987.
2. Norton, Harry N., *Sensor and Analyzer Handbook*, Prentice Hall Inc., 1982.
3. Herceg, Edward E., *Handbook of Measurement and Control*, Schaevitz Engineering, 1972.
4. Lenk, John D., *Handbook of Controls and Instrumentation*, Prentice Hall Inc., 1980.
5. Farrand Controls, *INDUCTOSYN Precision Linear and Rotary Position Transducers*, pp. 2-6, undated.
6. Doebelin, Ernest O., *Measurement Systems, Application and Design*, Mc Graw-Hill Book Co., 1976.
7. Hewlett Packard, *Application Note 1011, Design and Operational Considerations for the HEDS-5000 and HEDS-6000 Incremental Optical Shaft Encoders*, undated.
8. *Installation and Operation Manual, PT1250DC Heavy Duty Pan/Tilt*, p. 12, PELCO Sales Co., 1988.
9. Hewlett Packard, *56 mm Diameter Two and Three Channel Incremental Optical Encoder Kit*, Technical Data, January 1984.
10. Motorola Semiconductors, *MC68705U3 Advance Information*, Motorola Inc., 1981.
11. National Semiconductor Corporation, *Logic Databook*, Vol. 2, 1984.

12. Terman, F.W., *Latches and Flip Flops*, Lab Notes for EC2820 (Digital Circuits), pp. 3,4, Naval Postgraduate School, undated.
13. Taub, Herbert, *Digital Circuits and Microprocessors*, pp. 130-135, McGraw-Hill Book Co., 1982.
14. Motorola, *M6805 HMOS, M146805 CMOS Family, Microcomputer/Microprocessor User's Manual*, 2nd ed., Prentice-Hall Inc., 1983.
15. *Installation and Operation Manual, Motorized Zoom Lenses*, p. 6, PELCO Sales Co., undated.
16. National Semiconductor Corporation, *Linear Databook*, pp. (1-181)-(1-183), 1982.
17. 2500 A.D. Software, *6805 Macro Assembler*, Version 4.02, pp. (1-1)-(2-38), undated.
18. Motorola, *M68705EVM Evaluation Module User's Manual (M68705EVM/AD4)*, 4th ed., Motorola Inc., 1987.
19. Houghton, P.S., *Gears; Spur, Helical, Bevel, Internal, Epicyclic, and Worm*, 3rd ed., pp. 1.4,1.5, Technical Press, 1970.
20. Peebles, Peyton Z., Jr., *Probability, Random Variables, and Random Signals*, pp. 121-122, 2nd ed., McGraw-Hill Book Co., 1987.
21. Lloyd, Scot D., *An Autopilot Design for the United States Marine Corps' Airborne Remotely Operated Device*, Master's Thesis, Naval Postgraduate School, Monterey, CA, September 1987.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Technical Information Center Cameron Station Alexandria, VA 22304-6145	2
2. Library, Code 0142 Naval Postgraduate School Monterey, CA 93943-5002	2
3. Commandant of the Marine Corps Code TE 06 Headquarters, U.S. Marine Corps Washington, D.C. 20380-0001	1
4. Professor A. W. Cooper, Code 61Cr Department of Physics Naval Postgraduate School Monterey, CA 93943	10
5. Department Chairman, Code 62 Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, CA 93943	1
6. Professor H. A. Titus, Code 62Ts Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, CA 93943	2
7. Professor G. J. Thaler, Code 62Tr Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, CA 93943	1
8. Captain Peter D. Lloyd 3719 Frostwood Rd. Knoxville, TN 37921	5

Thesis

L767 Lloyd

c.1 The design and implementation of a position measuring system for a remotely controlled video camera.

Thesis

L767 Lloyd

c.1 The design and implementation of a position measuring system for a remotely controlled video camera.



thesL767

The design and implementation of a posit



3 2768 000 90780 2

DUDLEY KNOX LIBRARY